

state of
california

business &
transportation
agency

department
of
transportation



division of
structures

NOTE: PROGRAM USES

$$E_s = 28,000,000 \text{ PSI}$$

FRAME SYSTEM

Final Report

June 1975

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16. Abstract This report presents the results of a four-year project to provide bridge designers with a unified structural analysis tool for plane rectangular frames made up of prismatic and/or non-prismatic members. The program developed will calculate and report section, member and frame properties, fixed end moments, distributed moment and shear ordinates, and deflections for each member. Sidesway can be considered in single story frames. The program accepts prestressed cable information and produces cable path ordinates, cable path eccentricities, force coefficients, moment coefficients, shortening fixed end moments, prestress force, concrete strength, prestress moments and stresses, combined moments and stresses, and prestress deflections. Moment and shear plots may be obtained as optional output. Provision for describing railroad loadings or special overload truck loadings for live load analysis is also available with this program. A separate program provides input data retention and editing capabilities for this system.					
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INTRODUCTION

This project was prompted by a recognition of the opportunities for work improvement in the Division of Structures by means of electronic data processing (EDP). Electronic computer-based problem solving services are an important tool in the bridge design function. These services were developed individually over a period of years, each with characteristics appropriate to the known needs and then available processing facilities. Frame System was conceived as an integrated system that could tie together the frame analysis problems into a single system. This approach would eliminate the need to transfer data between the various services. With the implementation of Frame System, it became apparent that additional features added to the basic system could reduce processing costs, improve turnaround, analyze prestressed frames and provide easier to use input/output features. These modifications to the initial system were thought to be a cost effective solution to plane frame analysis capabilities in view of today's performance requirements and the current state-of-the-art in computer hardware and software.

THE PROJECT

6.1 Organization

The project was organized as a closed system with specific processing goals to be achieved. Work was divided into subtasks and designated as features to be added to the mainline frame analysis system. The features were named:

- . Prestressed Frame Analysis
- . Input data Retention
- . Input/output features
- . Railroad Loading
- . Live Load Deflections

The original approach for project completion was a single person operation with each feature completed in a sequential fashion. Subsequent personnel turnover problems prompted a new approach to project development. The final approach adopted used multiple analyst/programmers to work on individual features of the program under the direction of a project leader. This approach has provided some benefits to ongoing maintenance efforts but has caused difficulties when integration of features were accomplished. Multiple programmer/analyst provide various points of view to the development process and prevent one person from dominating the final product. Maintenance of the program is expected to be less difficult because less time will be needed to understand system operation.

Progress on this project was reported quarterly to the Federal Highway Administration. Funding was originally estimated at \$90,000 and later increased to a total of \$135,000. Cost overruns were attributed to three major factors. The factors were identified as:

- . Inflation of salaries
- . Personnel turnover
- . Computer System Changes

Processing equipment available to the project evolved from IBM S/360-65 at the outset, to an S/370-168 at termination. A Calcomp drum plotter and 3270 cathode ray tube remote terminals were available for systems development work.

6.2 Performance

Project performance required a mixture of engineering analysis and EDP technology. Interaction between the eventual users of the system and project developers created a constantly changing environment for the project. The primary steps to achieve the goals of the system were:

- . Problem definition
- . Evaluation of Alternatives
- . Translation to flow charts
- . Coding
- . Testing
- . Documentation
- . Implementation

The project performance was adversely affected by turnover of personnel. The original author of the system and his chief assistant programmer left for greener pastures during the first third of the project. Subsequent replacement personnel were trained engineers but required a period of additional training prior to becoming significant contributors to the project. As a result of the turnover problem, a multiple programmer/analyst approach to program development was attempted. Spin off from this technique has been to increase the interaction between members of the development team and to yield an improved product. Improved maintenance capabilities is expected to be a benefit in this approach because checks and balances

occur before the program code becomes complex or locked in. Negative factors that distract from program development by this method are perceived to be the following:

- . Coordination difficult
- . Unproductive discussion time
- . Coding errors from two or more sources difficult to diagnose
- . Communication difficult

It is felt, overall, that for a large system development project the concept of a programming team approach will yield a good final product.

6.3 Implementation

The original Frame System program was in routine production status at the beginning of this project. Each feature of the project was programmed and tested by the programmer/analyst prior to a trial implementation period. The trial period involved the selection of EDP oriented bridge designers to be initial users of the feature to be implemented. Checking of the newly created feature was accomplished in a quasi-production environment so that the systems operation could be monitored in its final configuration. Parallel operation of the existing program allowed comparisons of output values and system performance. User participation in system implementation was instrumental in removing many unforeseen program bugs that were not uncovered in the program testing period. Implementation in the production environment followed the user test period with a simultaneous removal of the previous program modules. Modules removed from the

production libraries were not destroyed for approximately three months in order to provide backup protection. Implementation of new features ultimately results in a reevaluation of the product itself. For this system new improvements have been suggested by developments in bridge design, bridge maintenance, and computer software and hardware capabilities.

6.4 Benefits

Frame System benefits the bridge design function in several ways. First the lengthy, repetitive type calculations for a bridge structure are reduced to an easier description of the physical constraints of the design problem. Analysis of the loads and load combinations are automatically generated with the resulting output usable in the next step of the design procedure. Second, the previous time constraint for analysis of bridge designs is improved. The resulting additional time in the design process allows the exploration of many structural alternatives as opposed to the previous method of selecting one design and completing it within the time constraint. Aesthetics of bridge structures are also improved due to the ease of analysis of structures with varying shapes. Previous hand analysis techniques were designed to be used with bridges whose superstructure and substructure members were of constant dimensions throughout the length of the member. The addition of nonprismatic members added significantly to the rigors of manual analysis calculations with a resultant lack of commitment by designers to a complex design for the benefit of aesthetics. The

computer program provides an alternative to manual analysis that encourages the considerations of aesthetics.

In addition to the benefits derived from providing a service for design, the system was modified to incorporate cost savings in computer processing. The existing system operated in what is known as a "batch environment." This technique consisted of a cycle of input forms, keypunching, machine processing and printed output. The usual outcome of one cycle of operation was an error in input data. The error condition was then identified, corrected and resubmitted for machine processing. A substantial amount of the reprocessing costs involved the rekeypunching of data that had no errors with the resultant increased probability of new errors developing in previously correct data. Analysis of operation costs also indicated that a substantial amount of the cost of operations was due to keypunch charges. The system solution to this problem consisted of two ideas. The primary system objective was to reduce the keypunch effort for problem data that was correct. The secondary objective was to reduce the time from input submission to receipt of printed output.

To achieve the first objective a preprocessing program was designed to store data in computer readable form regardless of the correctness of the data. Subsequent processing determined if the data could be processed and provided the necessary information for correction if errors were encountered. The second submittal of data was then processed on an exception

basis in that only the data in error was repunched. The resultant benefit was a drastic reduction in keypunch costs.

Time delay in processing was also attributable to system float time that occurred during the processing cycle.

An attempt to shorten the path was inserted into the system to provide a parallel processing path. The additional path removed the need for keypunching by placing the engineer in direct contact with the computer via a computer terminal with a video display. Correction data, if the volume was small, was keyed directly to computer storage and resubmission initiated from the terminal.

DESCRIPTION OF PROGRAM

7.1 Nature of Program

Frame System was designed to provide orthogonal plane frame analysis capability for prismatic or nonprismatic bridge frames with or without intermediate hinges. The main purpose of the system is to provide a low cost frame analysis program for a majority of the bridges designed in California. The program uses the method of integration to produce member properties and fixed end moments. Distributed end moments are produced using the Hardy-Cross method of moment distribution. This analysis method has proven to be sufficient for a majority of the framed structures designed in California. This method of analysis as implemented in Frame System has limitations with respect to the following factors:

- . Curvature
- . Torsion
- . Axial deformations
- . Shear deformations
- . Skew
- . Transverse distribution
- . Partial fixity of supports
- . Sloping members

Structural frames with the above constraints will require other analysis techniques. Programs such as "The Structural Design Language," known by the acronym STRUDL, developed at the M.I.T. Civil Engineering Systems Laboratory, may

be used when the bridge designer has determined that the limitations of Frame System have been exceeded.

To provide a low cost alternative to the large multipurpose programs such as STRUDL required features to both minimize processing costs and features to minimize user costs. Program optimization was accomplished using the H level IBM FORTRAN IV compiler for efficient core usage and loop structure in machine language. Processing costs were reduced with respect to resubmittals by providing a data update facility within the system. Resubmittal costs are reduced because the volume of keyed data is significantly reduced using the update capability. Only those records with changes need be keyed for subsequent submittals of Frame System. Keying of input data records was determined to be the major source of generated costs from computer operations in our environment.

Minimization of costs from the user point of view involves ease of input submittal and interpretation of results. Input submittal is performed with preprinted input forms with descriptive column headings to guide the users input preparation. Where input values are repetitive or standard shapes are involved, provision is made to either recall previously coded input data or use standard shapes stored in the program. Variations of the standard member shapes can be accomplished by adding or subtracting parts at a cross section. For live loading input effort is limited to a description of the number of lanes of the standard AASHTO truck to be applied to the structure.

Output results are arranged in a logical order. The philosophy adopted for frame system was an automatic print of the input values followed by the results calculated by the program. Program output formats were designed to fit into the subsequent design steps. For example a summary sheet provides moments and axial load results for the controlling conditions in column design.

7.2 Coordinate System and Sign Convention

The coordinate system used by Frame System is two dimensional with the X and Y axis arranged in the usual order encountered in structural engineering (see Fig. 1).

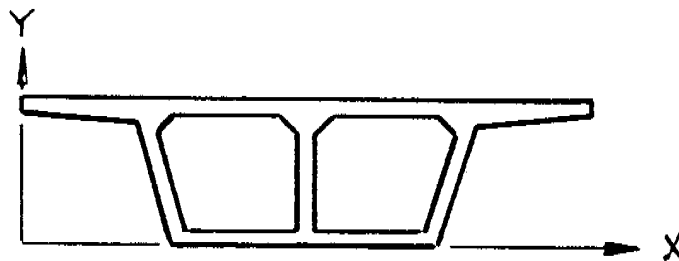


Fig. 1

The axis of bending for the cross section is considered to be located at the center of gravity of the section and parallel to the X axis. For a vertical member, the axis system is rotated ninety degrees so that the X and Y axis are parallel to the cross section plane of the column (see Fig. 2).

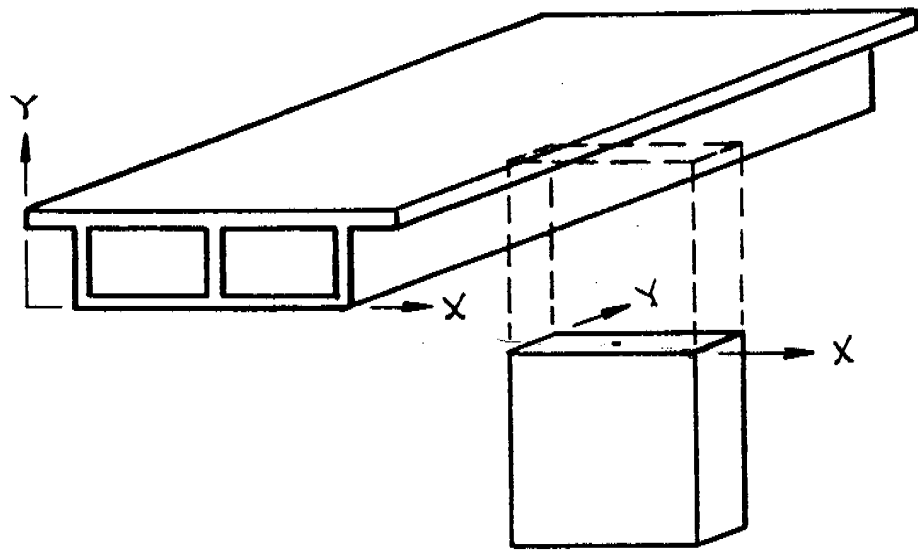


Fig. 2

The sign convention for Frame System is beam convention. For example, a positive moment reported on output for a horizontal member indicates the member has positive curvature at that point. Text books often mention that positive curvature is the shape a horizontal member would assume to hold water (see Fig. 3).

i.e.

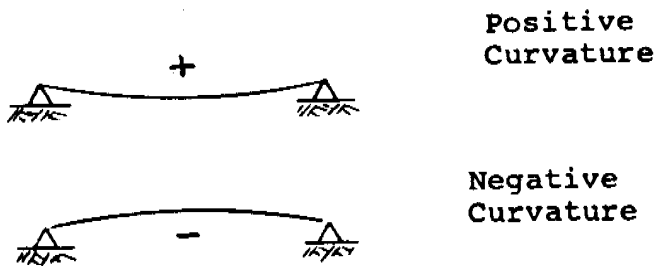


Fig. 3

For vertical members a positive moment would indicate the member is bending with positive curvature viewed with the bottom as the left end of the member (see Fig. 4).

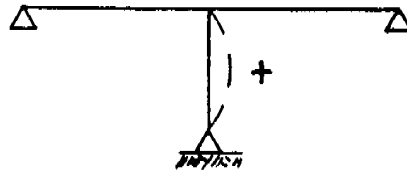


Fig. 4

Deflections and rotations are measured from the unloaded position of the frame. Clockwise rotations are positive and downward deflections are positive. For vertical members a positive deflection indicates the member has deflected to the right.

7.3 Analysis Assumptions

The Hardy-Cross analysis technique considers the frame members to be linearly elastic. Analysis of bending and shear by the method implies knowledge from three sources. First and foremost are the laws of Statics. Second are the facts of geometry which relate how the structure is connected. Third, the properties of materials is involved in the problem with Hooke's law assumed and moduli of elasticity of the component parts of a structure known. The final moments are obtained by successive numerical approximations. The method in general involves the calculation of moments at the ends of all beams in a frame under certain artificial conditions of restraint, then

a redistribution of unbalanced moments by arithmetical proportion when the artificial restraints are removed. For Frame System the balancing procedure is performed five times for structures with distribution factors on all members within the range $.1 \leq x \leq .9$. For all other distribution factors not within the above limitations, ten cycles of moment distribution are performed. For frames that require sidesway correction a one inch horizontal deflection is introduced and the resulting moments distributed throughout the frame. If a loading condition is specified to be sideswayed, the base shear equations are solved to obtain the required amount of sidesway moments needed to adjust the distributed moments.

The method of moment distribution has been considered the major method of moment and shear calculation in California bridge design for many years with adequate results obtained from this method. Methods to account for the affects of axial deformation and shear deformation have existed for many years. It is felt by this author that frame system should be modified to utilize these additional analysis techniques to optionally consider the additional deformations that physically occur in a bridge structure.

8. Summary

The project to modify Frame System has produced a computer program that provides for the analysis of a significant portion of the bridges designed for the California Department of Transportation. The features implemented have

reduced significantly the computational load for the bridge designer. The prestress, and update features of the project have contributed to the design effort and will most likely provide for more economical bridge designs. The Railroad Loading feature of the project was implemented as Live Load Generator option to the program. This feature was thought to be a solution for railroad multi-axle loadings. Upon reflection of the capability as implemented, it has been found that the system is inadequate for AREA loadings and partially adequate for loadings such as BART trains. The major use has been in the area of special overload permit vehicle analysis. When the Department becomes involved in mass transit design work or extensive railroad bridge design it will become necessary to rework this area of the program. The Live Load deflection feature was determined not necessary at the present time. As a result the live load deflection may be obtained from the existing program by simulating the critical Live Load situation with a loading trial.

APPENDIX A

FRAME SYSTEM UPDATE
(BDEØ38)

PROGRAM DOCUMENTATION

CONTENTS

Instructions to Users. A-2
Systems Documentation. A-11

FRAME SYSTEM UPDATE

The purpose of the Frame System Update program is to provide a means of storing Frame System input data in a readily accessible file for periods of 30 days or more.

All of the above features are made available via line number, a special code on the input forms, and the BRIDGE JOB CONTROL FORM.

CREATING A NEW FILE

New files may be created only by using the BRIDGE JOB CONTROL FORM (FORM H BD D 147) and a full set of Frame System input data for a problem.

The following is an example of the BRIDGE JOB CONTROL FORM that must be used to store a data file for Frame System Update

BRIDGE JOB CONTROL BDEJCL. A grid form with columns for PROGRAM NAME, PRIORITY, SOURCE, CHARGE, EXPEND AUTH, SPECIAL DESIGNATION, IDENT, FILE ADDRESS, RETPD, CORE, REGION, TIME, COMMENTS, and S C NO.

USER INSTRUCTIONS

THIS FORM MUST BE USED FOR THE FOLLOWING BRIDGE DEPARTMENT COMPUTER APPLICATIONS

- FRAME SYSTEM UPDATE TIME SHEET SUMMARY
BRIDGE DECK GEOMETRICS MAN HOUR SUMMARY
ICES BRIDGE STRUDL
ICES BRIDGE COGO
ICES BRIDGE LIST

EXAMPLES OF EACH OF THE ABOVE APPLICATIONS ARE AVAILABLE ON SEPARATE SHEETS.

KEY PUNCH INSTRUCTIONS

USE BLUE CARD PUNCH AS SHOWN (RIGHT CC) USE PRINTER PUNCH. PUNCH DATA CARDS AND PLACE BEHIND BLUE CARD.

PROCESSING INSTRUCTIONS

JOB NAME BDEJCL PLACE BLUE CARD AND DATA BEHIND 'JCL' CARDS. MANY DECKS. BLUE CARD & DATA, MAY BE SUBMITTED TOGETHER.

INPUT. CARDS

OUTPUT. PRINTER (SYSOUT = D)

BRIDGE CLERK

RETURN INPUT CARDS AND OUTPUT TO SUBMITTER EXT. DATE

ALPHABETIC BATCH IDENTIFICATION

Table with 4 columns: Letter (A-J), Range (0-4 to 45-49), Letter (K-U), Range (50-54 to 95-99)

The BRIDGE JOB CONTROL FORM must be filled out in the following manner for Frame System Update. Under program name, write FRAM. Start the word in Column 1. Under priority, place a number from 00 to 07 or 11. For applications where overnight turnaround is acceptable use a priority 00.

Fill in appropriate cost information under source, charge, expenditure authorization and special designation, if applicable. Fill in District, Group, Batch and Problem Number. The parameters 'RETPD', 'CORE', and 'TIME', are not used in this application and can be ignored and left blank.

'FILE STATUS' refers to the condition of the file. If it is a new file write the word 'NEW' in the space provided. If the file already exists and some manipulation of the data is to take place write the word 'OLD' under file status. If the file is to be deleted write the word 'DEL' under file status. No additional forms are required to delete a file. If the file is of no further use, please delete the file as space in the storage facilities is limited.

The file address is a six digit name composed of alpha and numeric characters. The file name must be left adjusted and must not contain any blanks. Each job must have a unique name so it would be to the users advantage to use your 'DIST-GROUP-BATCH-PROBLEM NO' identification (i.e., 14T101).

The 'PARM' parameter must be either 1, 2 or left blank. Instructions for the different parm parameters are given in the table below.

PARM PARAMETER ON JOB CONTROL FORM

LIST/RUN CODE	FILE STATUS	UPDATE DATA ATTACHED	NO UPDATE DATA
Blank	New	File will be created and run	
	Old	File will be updated and run	Old File will be run
1	New	File will be created	
	Old	File will be updated, and listed	Old File will be listed
2	New	File will be created and run	
	Old	File will be updated listed and run	Old fill will be listed and run

The following is an example of a completed BRIDGE JOB CONTROL FORM for storing a file for Frame System.

BRIDGE JOB CONTROL

BDEJCL

PROGRAM NAME	PRIORITY	SOURCE		CHARGE		EXPEND AUTH				SPECIAL DESIGNATION (USE WHEN APPLICABLE)	IDENT			FILE STATUS	FILE ADDRESS	REYPD	PARM	CORE REGION	TIME	COMMENTS (NAME)	S C NO	
		DIST	UNIT	DIST	UNIT	10	11	12	13		14	15	16									17
FRAM	00	1	093	4303	3910002						INT	1001	2060	14716							MC-SARE	7275

USER INSTRUCTIONS

THIS FORM MUST BE USED FOR THE FOLLOWING BRIDGE DEPARTMENT COMPUTER APPLICATIONS.

- FRAME SYSTEM UPDATE
- BRIDGE DECK GEOMETRICS
- ICES BRIDGE STRUDL
- ICES BRIDGE COGO
- ICES BRIDGE LIST
- TIME SHEET SUMMARY
- MAN HOUR SUMMARY

EXAMPLES OF EACH OF THE ABOVE APPLICATIONS ARE AVAILABLE ON SEPARATE SHEETS.

KEY PUNCH INSTRUCTIONS

USE BLUE CARD PUNCH AS SHOWN (RIGHT CC) USE PRINTER PUNCH.
PUNCH DATA CARDS AND PLACE BEHIND BLUE CARD.

PROCESSING INSTRUCTIONS

JOB NAME BDEJCL PLACE BLUE CARD AND DATA BEHIND 'JCL' CARDS.
MANY DECKS. BLUE CARD & DATA, MAY BE SUBMITTED TOGETHER.

ALPHABETIC BATCH IDENTIFICATION

A	0-4	K	90-94
B	5-9	L	55-59
C	10-14	N	60-64
D	15-19	O	65-69
E	20-24	P	70-74
F	25-29	Q	75-79
G	30-34	R	80-84
H	35-39	S	85-89
I	40-44	T	90-94
J	45-49	U	95-99

INPUT: CARDS

OUTPUT: PRINTER (SYSOUT = D)

BRIDGE CLERK

RETURN INPUT CARDS AND OUTPUT TO SUBMITTER _____ EXT. _____ DATE _____

DM OS D147 (Rev. 10-73)

Each problem submitted must be a separate and distinct problem. Do not submit multiple problems with one BRIDGE JOB CONTROL FORM. Each job must have one BRIDGE JOB CONTROL FORM followed by the Frame System Forms. If you wish to store two problems you must submit each problem separately with its own BRIDGE JOB CONTROL FORM and file address. The next version of the program will allow for multiple problems in a single file. This new version will be released about February 1, 1974.

UPDATE

All existing input sheets for Frame System have 4 columns added to the left of the data sections: the CODE column and LINE No. column.

Update	
CODE	Line No.

Both of these columns should be left blank when creating a new file, but are used when updating an old file.

LINE NO.

When creating a new file (FILE STATUS is NEW), the line numbers are automatically assigned by the program and are printed on the Frame System Update output.

When updating an existing file (FILE STATUS is OLD) the Line No. of the new or modified record must always be included. If the Line No. of the new record is not found in the file it will be inserted in the file. If the Line No. exists in the file the program will replace the entire old line of data with the new line.

CODE

This column can either be left blank or filled with a code letter of D, R, or S.

If the Code is left blank, the line of data will be inserted in the file, or replace the existing line of data in the file.

If D is used, the Line No. given will be searched for in the existing file and, if found, will be deleted from the file. If not found, an error message will be output to the user.

If S is used, the Line No. given will be skipped by the program on all future runs.

To reuse the skipped record, place an R in the Code column and provide the Line No. of the record. It will then be used in all future runs of the file.

Each time a new record is read or acted on by Frame System Update it will print a message of the action taken on that record. Either it was modified, added, or deleted from the data set. Also it will tell if the record will be skipped or returned to the job stream of the Frame System Program.

The List program will give a formatted list of all the records stored in the data set. It will also list if a record was to be skipped or returned to the job stream on the current run of 'Frame System'.

A number of examples follow that will illustrate the various features of the program.

- 1) Insert or modify Line No. 0025.

C O D E	Update		Member No.	End Joint No.		End Condition Direction	Length
	Line No.			Lt.	Rt.		
				lt.	rt.		
	25	2	2	3	H	750	

The entire line will be replaced so all data must be entered.

- 2) Delete record 0040.

C O D E	Update		Member No.	End Joint No.		End Condition Direction	Length
	Line No.			Lt.	Rt.		
				lt.	rt.		
D	40						

- 3) Skip record 0050

C O D E	Update		Member No.	End Joint No.		End Condition Direction	Length
	Line No.			Lt.	Rt.		
				lt.	rt.		
S	50						

4) Return record 0060 to problem job stream.

C O D E	Update	Member No.	End Joint No.		End Condition Direction		Length
	Line No.		Lt.	Rt.	lt.	rt.	
R	60						

The following is an example of input and output for Frame System Update.

Figures 1 and 2 are the input forms that created the file. Figure 3 is the output from the program showing line numbers and formats.

BDEJCL

PROGRAM NAME	PRIORITY	SOURCE		CHARGE		EXPEND AUTH	SPECIAL DESIGNATION (USE WHEN APPLICABLE)	IDENT			FILE ADDRESS	REPOD	REVAL	TYPE	SECTION	TIME	COMMENTS (NAME)	S E NO
		DIST	UNIT	DIST	UNIT			OUT	DRUP	BATCH								
FRAM	00	14033	14033	14033	14033			14T	1001		14033						McGARR	7275

USER INSTRUCTIONS
THIS FORM MUST BE USED FOR THE FOLLOWING BRIDGE DEPARTMENT COMPUTER APPLICATIONS.

FRAME SYSTEM UPDATE	TIME SHEET SUMMARY
BRIDGE DECK GEOMETRICS	MAN HOUR SUMMARY
ICES BRIDGE STRUDL	
ICES BRIDGE COGO	
ICES BRIDGE LIST	

EXAMPLES OF EACH OF THE ABOVE APPLICATIONS ARE AVAILABLE ON SEPARATE SHEETS

KEY PUNCH INSTRUCTIONS
USE BLUE CARD PUNCH AS SHOWN (RIGHT CC) USE PRINTER PUNCH PUNCH DATA CARDS AND PLACE BEHIND BLUE CARD.

PROCESSING INSTRUCTIONS
JOB NAME BDEJCL PLACE BLUE CARD AND DATA BEHIND 'JCL' CARDS. MANY DECKS, BLUE CARD & DATA, MAY BE SUBMITTED TOGETHER.

INPUT CARDS
OUTPUT PRINTER (SYSOUT = D)

BRIDGE CLERK
RETURN INPUT CARDS AND OUTPUT TO SUBMITTER *P. McCabe* EXT *6579* DATE *10-1-73*

04 05 D47 (Rev 10-73)

A	0-4	K	50-54
B	5-9	L	55-59
C	10-14	N	60-64
D	15-19	O	65-69
E	20-24	P	70-74
F	25-29	Q	75-79
G	30-34	R	80-84
H	35-39	S	85-89
I	40-44	T	90-94
J	45-49	U	95-99

Figure 1
FRAME SYSTEM
Superstructure Sections

BDE044

Page 1 of 1
Name McCabe
Phone 5-6579

UPDATE	LINE NO	CROSS SECTION LOCATION	REF COORD		SS DATA		SLAB DATA		INT GIRDERS		EXTERIOR GIRDERS		OVERHANGS		STORE	
			X	Y	WIDTH	DEPTH	TOP THICK	BOTTOM THICK	NUMBER	TYPE	LEFT	RIGHT	LEFT	RIGHT		
	1. 00.		00	00	340	325	725	700	3/2	1/2	1/2	1/2	1/2	1/2	1/2	01
	1. 200.				370											
	1. 500.				450											
	2. 0001															
	2. 500.		00	00	450	350	750	725	4/2	1/2	1/2	1/2	1/2	1/2	1/2	
	2. 1000.				500											

BASIC SECTION

EXTERIOR GIRDERS

Form H-80 D12 (REV 4/73)

Figure 2
A-8

SUPERSTRUCTURE SECTIONS

LINE NO.	MEM NO	X-SEC NO	LOCAT	REF	REF. PT. COORD.		S.S. DATA		SLAB DATA		INT. GDRS		EXTERIOR GIRDERS		OVERHANGS										
					X	Y	WIDTH	DEPTH	TOP	BOT	NO	WB	LEFT T	RIGHT T	WB	FACT	LEFT LEN	EX IN	RIGHT LEN	EX IN	ST				
ADDED																									
0010	1	0.0			0.0	0.0	34.0	3.25	7.25	7.00	3	12	1	12	1.50	1	12	1.50	3.0	7	11	3.0	7	11	
ADDED																									
0020	1	20.0			0.0	0.0	37.0	3.25	7.25	7.00	3	12	1	12	1.50	1	12	1.50	3.0	7	11	3.0	7	11	
ADDED																									
0030	1	50.0			0.0	0.0	45.0	3.25	7.25	7.00	3	12	1	12	1.50	1	12	1.50	3.0	7	11	3.0	7	11	01
ADDED																									
0040	2	0.0	01		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0.0	0	0.0	0	0.0	0.0	0	0	0.0	0	0	0
ADDED																									
0050	2	50.0			0.0	0.0	45.0	3.50	7.50	7.25	4	12	1	12	1.50	1	12	1.50	3.0	7	11	3.0	7	11	
ADDED																									
0060	2	100.0			0.0	0.0	50.0	3.50	7.50	7.25	4	12	1	12	1.50	1	12	1.50	3.0	7	11	3.0	7	11	

THE NEW FILE WITH IDENTIFICATION NOA.FRAM.B0147166 WILL EXPIRE ON
WEDNESDAY OCTOBER 31, 1973

BATCH CHARGE UNITS= 7 APPROXIMATE MACHINE TIME 4.20 SECS APPROXIMATE MACHINE CHARGE \$ 0.84

Figure 3

Figure 4 is the input form showing the corrections that are to be made to the file.

Figure 5 is the output showing the changes that were made to the file.

FRAME SYSTEM
Superstructure Sections

B0E0AA

Page 1 of 1
Name MCCABE
Phone 6519

UPDATE	LINE NO	X-SEC NO	LOCAT	REF	REF. PT. COORD.		S.S. DATA		SLAB DATA		INT. GIRDERS		EXTERIOR GIRDERS		OVERHANGS									
					X	Y	WIDTH	DEPTH	TOP	BOTTOM	NO	WB	LEFT T	RIGHT T	WB	FACT	LEFT LEN	EX IN	RIGHT LEN	EX IN	ST			
	20	1	200		00	00	400	325	725	700	3	12	1	12	150	1	12	150	3	7	11	3	7	11
S	25	1	400				440																	
D	50																							
D	60																							

BASK SECTION

Form H-80 D12 (REV 6/73)

EXTERIOR GIRDERS

TYPE 0 TYPE 1 TYPE 2 TYPE 3

Figure 4

SUPERSTRUCTURE SECTIONS

LINE NO.	MEM NO	X-SEC NO	LOCAT	REF	REF. PT. COORD.		S.S. DATA		SLAB DATA		INT. GDRS		EXTERIOR GIRDERS		OVERHANGS									
					X	Y	WIDTH	DEPTH	TOP	BOT	NO	WB	LEFT T	RIGHT T	WB	FACT	LEFT LEN	EX IN	RIGHT LEN	EX IN	ST			
MODIFIED																								
0020	1	20.0			0.0	0.0	40.0	3.25	7.25	7.00	3	12	1	12	1.50	1	12	1.50	3.0	7	11	3.0	7	11
ADDED																								
0025	1	40.0			0.0	0.0	44.0	3.25	7.25	7.00	3	12	1	12	1.50	1	12	1.50	3.0	7	11	3.0	7	11
SKIPPED																								
0050	2	50.0			0.0	0.0	45.0	3.50	7.50	7.25	4	12	1	12	1.50	1	12	1.50	3.0	7	11	3.0	7	11
DELETED																								
0060	2	100.0			0.0	0.0	50.0	3.50	7.50	7.25	4	12	1	12	1.50	1	12	1.50	3.0	7	11	3.0	7	11

Figure 5

Figures 6 and 7 are formatted lists of all the records in the file after updating.

IDENT		FRAME SYSTEM LIST										OCTOBER 02, 1973		PAGE 1	
SUPERSTRUCTURE SECTION PROPERTIES															
C LINE MEM	LOC	RECALL	X	Y	SUPERS STRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE				
0	10	1	0.0		WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB				0	
					34.0	3.25	7.25	7.00	3	12.					
			LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG			
			TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.	
			1	12.	1.50	1	12.	1.50	3.0	7.	11.	3.0	7.	11.	
C LINE MEM	LOC	RECALL	X	Y	SUPERS STRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE				
0	20	1	20.0		WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB				0	
					40.0	3.25	7.25	7.00	3	12.					
			LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG			
			TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.	
			1	12.	1.50	1	12.	1.50	3.0	7.	11.	3.0	7.	11.	
C LINE MEM	LOC	RECALL	X	Y	SUPERS STRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE				
0	25	1	40.0		WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB				0	
					44.0	3.25	7.25	7.00	3	12.					
			LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG			
			TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.	
			1	12.	1.50	1	12.	1.50	3.0	7.	11.	3.0	7.	11.	
C LINE MEM	LOC	RECALL	X	Y	SUPERS STRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE				
0	30	1	50.0		WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB				1	
					45.0	3.25	7.25	7.00	3	12.					
			LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG			
			TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.	
			1	12.	1.50	1	12.	1.50	3.0	7.	11.	3.0	7.	11.	

Figure 6

IDENT		FRAME SYSTEM LIST										OCTOBER 02, 1973		PAGE 2	
SUPERSTRUCTURE SECTION PROPERTIES															
C LINE MEM	LOC	RECALL	X	Y	SUPERS STRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE				
0	40	2	0.0	01	0.0	0.0	0.0	0.0	0	0.				0	
			LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG			
			TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.	
			0	0.	0.0	0	0.	0.0	0.0	0.	0.	0.0	0.	0.	
C LINE MEM	LOC	RECALL	X	Y	SUPERS STRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE				
0	50	2	50.0		WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB				0	
					44.0	3.50	7.50	7.25	4	12.					
			LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG			
			TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.	
			1	12.	1.50	1	12.	1.50	3.0	7.	11.	3.0	7.	11.	
COST DISTRIBUTION															
SOURCE	CHARGE	EXP. AUTHOR.	SPECIAL DESIGNATION												
14033	14033	910002													

Figure 7

SYSTEM DOCUMENTATION

A complete package of system documentation may be obtained for the Frame System Update program by sending a request and a 9-track magnetic tape to:

California Department of Transportation
Division of Structures
Bridge Computer Services
Box 1499
Sacramento, California 95807

APPENDIX B

FRAME SYSTEM
(BDEØ35)

PROGRAM DOCUMENTATION

VERSION 6.1 MOD Ø

CONTENTS

Instructions to Users.	B-2
Systems Documentation.	B-127

DEPARTMENT OF TRANSPORTATION
OFFICE OF STRUCTURES
COMPUTER SERVICE

FRAME SYSTEM

INSTRUCTIONS FOR USERS

This service is a general plane frame analysis and design program with a large degree of flexibility and several specialized input features. The following list is a summary of some of the program's capabilities:

1. The frame members may be prismatic or non-prismatic.
2. Intermediate member hinges and cantilevers are accommodated.
3. Sidesway may be included.
4. Members must be orthogonal - girders are horizontal and columns are vertical.
5. Reduction of the negative moment due to support width may be obtained.
6. Moment and Shear diagrams can be produced in plotted form.
7. Loads may be given as applied forces or as fixed-end-moments.
8. Live Loads for a standard HS truck or any 3-axle load will be automatically generated.
9. Influence lines may be generated, and plots produced.
10. Live Loads for a 13-axle truck may be automatically generated.
11. Bent live loading may be generated. (Future release)
12. The frame can be designed or analyzed for prestress from a given cable path.

Since this program is for plane frames only, the user must be aware of the limitations of the analysis method. Factors such as curvature, torsion, axial and shear deformations,

skew, transverse distribution, and partial fixity are not considered in the program. Considerable judgement is required in deciding if a structure such as a skewed, curved box girder bridge with intermediate diaphragms should be analyzed as a plane frame. For this type of structure, programs such as STRUDL, CELL, CURVBRG, MUPDI or FINPLA may be better.

DATA PREPARATION

Data may be given directly from input forms, or via an existing input file. To create or modify a file for a frame system problem see the user instructions titled "Frame System Update."

The following input forms may be used to define a problem:

FRAME DESCRIPTION describes the frame. By itself, this data would produce a dead load analysis.

SUPERSTRUCTURE SECTIONS describes cross-section geometry. By itself this form will produce section properties. This data is normally used to supplement the frame description data. The section described by this form may be modified by submitting Section Properties by Parts with the same member no. and cross-section location.

SECTION PROPERTIES BY PARTS describes a section of a prismatic member or multiple sections of a non-prismatic member. By itself this form will produce section properties. This data is normally used to supplement the frame description data or the superstructures sections data.

LOAD DATA describes the loading conditions applied to the frame. It can only be used as a supplement to the frame description.

SUPERSTRUCTURE LIVE LOAD describes the live load condition to be applied to the frame. A multiple of the standard HS20-16 truck or a user designed 3-axle truck may be specified as the live load.

LIVE LOAD GENERATOR describes the multi-axle live load to be applied to the frame. Variations of the axle load and spacing may be obtained, or the program will default to a standard P-13 truck.

PRESTRESSED DATA describes the prestressing cable paths to be incorporated in the frame to resist the input loads.

COMMON INPUT

IDENT and accounting data are standard. See General Instructions 1-1. Problem may be any number, but it must be the same number for all data pertaining to the problem.

IDENT.				SOURCE		CHARGE		EXPENDITURE	SPECIAL DESIGNATION
DIST.	GR.	BATCH	PROB.	DIST	UNIT	DIST	UNIT	AUTHORIZATION	WHEN APPLICABLE
S/C	2091.	7310		S/C	2091				

UPDATE CODE AND LIVE NO. are input required by the "Frame System Update" program. This information is not needed by the Frame System program.

FRAME DESCRIPTION

Member No. must start with 1 and increase consecutively. Horizontal members must be numbered first. Up to 50 members may be analyzed for dead load. If the live load input form is used only 25 horizontal members are allowed. If prestress data is used only 15 horizontal members are allowed.

Update CODE	Line No.	Member No.	End Joint No.		End Condition Direction	Length ft.	Min. I ft ⁴	Hinge Location or Support Width ft.	E ksi
			Lt.	Rt.					
			Lt.	Rt.					
Dead Load		Member Properties				Recall		D.L.	
Uniform	Unit Wt.	-K-		-C-		Member	Reverse	Deflections	Sideway
k/ft.	pcf	Lt.	Rt.	Lt.	Rt.	R			S

END JOINT NUMBERS define the structural topology or connectivity. Each member is connected to two of the joints in the structure. For vertical members, the left end is assumed to be the bottom and the right end is

assumed to be the top. Joints must be numbered consecutively starting with 1. Up to nine members may meet at one joint except if Live Load data or Prestressed Data are included. Then only three members may meet at one joint.

END CONDITIONS describe the degree of freedom of the member at the joint.

C = Cantilevered (unsupported)

P = Pinned (Moment is released. Horizontal and vertical forces are continuous.)

(R) = Roller (Moment and Horizontal force is released.)

Please note that vertical forces, including uplift, can be transmitted thru both a pin and a roller. A roller at the end of a vertical member causes the member to act as a cantilever. (See Sideways Restrictions). If no entry is made, the end condition is assumed to be fixed.

DIRECTION is assumed to be vertical unless a "G" or "H" is entered to indicate a girder or horizontal member.

LENGTH is the span length of the member from centerline of support to centerline of support.

MIN. I is the minimum moment of inertia. If the moment of inertia is entered here, then certain output features are not provided. If this entry is left blank, the required section properties must be provided by the "Superstructure Section" or "Section Properties by Parts" input forms.

HINGE LOCATIONS OR SUPPORT WIDTH define the hinge location or support width, depending on the entry in the "Direction" field. If a "G" or "H" is entered for direction, then a hinge location is defined, otherwise, a support width is defined. Hinge location is given as the distance in feet from the left support to the hinge centerline. The support is usually the bent cap width in feet or the column width in feet. This information is needed to obtain the moment reduction.

E, the modulus of elasticity, may be input or the user may accept the built-in defaults. Once an entry is made, E remains constant for all subsequent members until another entry is made. If no value is given, E defaults to two values. An E of 750 KSI is used for stiffness, deflections,

and prestress elastic shortening calculations. An E of 3000 KSI is used for sidesway calculations.

DEAD LOAD can be applied to the input frame by two methods.

UNIFORM describes a uniform load in kips/foot.

UNIT WT. describes the weight of the material to be used in calculating dead load. To use unit weight, the member must be described with Section Properties input. If no unit weight is given a value of zero is used. A separate value is required for each member described. Both a uniform load and a unit weight may be applied simultaneously. Dead loads applied to vertical members are assumed to act parallel to the longitudinal axis of the member. Supplemental loads may be added to the dead load analysis by giving "Load Data" with the trial no. 00. Supplemental loads such as barrier railings, sidewalks, and wearing surfaces may be applied as "Added Dead Load" by submitting "Load Data" input with the trial no. 01.

STIFFNESS AND CARRY OVER factors have to be given only when the member is non-prismatic and has not been defined by section properties input data. The factors may be given adjusted for pinned end conditions, if desired. The drawback of giving stiffness and carry over factors is that fixed end moments must be given for any loads applied to these members. Also, deflections cannot be calculated for these members.

MEMBER RECALL is available for members which have identical properties. These properties include Length, I, end condition, area, unit weight, and dead load. The only data required for the repetitive member is the member number, the end joint numbers, and the member number from which the data is to be obtained. If the member is to be flipped end for end enter "R" in the REVERSE column. Any other data given for the repetitive member, including section properties, is ignored. Data may not be recalled from a member which was generated by member recall.

DEFLECTIONS at the quarter points of all members will automatically be calculated for Dead Load (trial no. 00). If they are desired at some evenly spaced points other than the quarter points, enter the number of equal spaces under DEFLECTIONS. The entry needs to be made only once and may be made in the data for any member. Repeating the same entry in the data for several members is harmless, but two or more different entries will result in the last entry being

used for all members. In addition to the above, deflections will always be calculated at hinges and at the quarter points of the longer portion of a hinged member.

If correction for SIDESWAY is desired in the Dead Load analysis (trial no. 00), enter 'S' on the Frame Description input. The entry needs to be made only once and may be made in the data for any member. If correction for SIDESWAY is desired for any other trial, the entry must be made on Load Data input for that trial. This entry needs to be made only once per trial and may be made in the data for any line of the trial.

SIDESWAY DIAGNOSTICS, if any, are reported following the Fixed End Moments of the trial in which SIDESWAY was first requested.

If Sidesway Diagnostics are not present, the result of swaying the frame one inch to the right is reported in the form of Vertical member shears and end moments. If the structure contains hinges, these results are obtained by deflecting each frame separately. (The whole structure is not deflected simultaneously.)

Page headings will indicate whether sidesway was considered. If Sidesway Diagnostics are present, the heading will indicate that diagnostics are present and sidesway was not considered in analysis.

Sidesway Assumptions:

1. Hinges transfer vertical, but not horizontal forces.
2. Rollers resist vertical forces.

Sidesway Restrictions:

1. The structure must be a single story, plane, rectangular frame.
2. Ends of intermediate horizontal members may not be a roller or cantilever.
3. An end horizontal member which has a roller or cantilever, must be the only member at that joint.
4. Vertical members cannot be cantilevered.
5. Rollers are permitted at the right (top) end of vertical members, but not at the left (bottom) end.

SUPERSTRUCTURE SECTIONS

Normally this input option is used to supplement the frame description data, producing section and member properties. It may also be used as a stand alone submittal, producing just section properties. In either case, the section described may be modified by inputting section properties by parts data with the same member no. and cross section location.

UPDATE		MEMBER NO.	CROSS SECTION LOCATION (FT)	REF. PT. COORD.	S.S. DATA		SLAB DATA	
C O O D E	LINE NO.				X	Y	WIDTH E.D.-E.D.	DEPTH
			(FT)	(FT)	(FT)	(FT)	(IN.)	(IN.)

The MEMBER NO. and CROSS SECTION LOCATION identify and locate the section from the left end of the member. Both must be repeated on each line used to describe the section.

Generally, the MEMBER NO. will correspond to that of a Frame Description member. The exception is that if the member number is zero (and an arbitrary Location given), section properties alone are calculated, which allows building sections initially, storing the results, and recalling them when building members.

If the member is prismatic, only one section need be described. Its CROSS SECTION LOCATION may be zero if the member length is defined in the Frame Description. Otherwise, the location of this section must define the member length.

When describing a non-prismatic member, the resulting I diagram is one which varies as a straight line between the sections given. Therefore, the number of sections needed to describe the member depends on how the moment of inertia varies. The CROSS SECTION LOCATION of the first section would be zero. The last section location would equal the member length used in calculating the stiffness and carryover factors. A maximum of 50 sections per member is allowed.

For both prismatic and non-prismatic members, if the member length given in the frame description does not agree with the length defined by the last cross section location, the difference is resolved as follows. The length defined by the last cross section location is used to calculate member properties. The length given by the frame description is used to calculate fixed-end-moments.

The section properties that have been calculated for a given member no. and cross section location may be saved for future use. This is done by entering a number from 1 to 99 under STORE. Only one entry under STORE is needed for each cross section location even when using both the superstructure sections form and the section properties by parts form.

RECALL data for use in subsequent sections by entering the number which was assigned to store the data. Section properties are calculated in order of member no. and cross section location. Recall is only available on a stored value from a member no. and cross section location whose section properties have already been calculated. More than one recall may be made per section. The recalled data may be modified by adding or subtracting parts, provided that the X-Y coordinate system is on the same reference datum for both sections. The SIGN field cannot be applied to the data recalled. Sections may be recalled within and between problems, but not between batches.

WIDTH and DEPTH of the superstructure must be given. The width is measured from edge of deck to edge of deck and the depth is measured from top of deck to bottom of soffit. The depth must also be measured from the reference point.

TOP and BOTTOM SLAB THICKNESS must be given, except for T-beam sections, in which case the bottom slab is omitted.

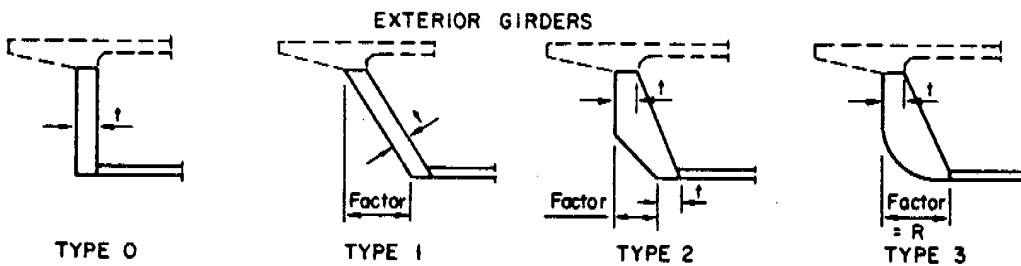
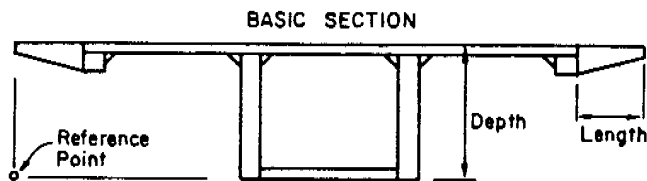
INT. GIRDERS			EXTERIOR GIRDERS						OVERHANGS						
			LEFT			RIGHT			LEFT			RIGHT			
NUMBER (INT. ONLY)	WEB THICK. (IN.)	TYPE	WEB THICK. (IN.)	FACTOR (FT.)	TYPE	WEB THICK. (IN.)	FACTOR (FT.)	LENGTH (FT.)	EXT. THICK. (IN.)	INT. THICK. (IN.)	LENGTH (FT.)	EXT. THICK. (IN.)	INT. THICK. (IN.)	STORE	

INT. GIRDERS NUMBER and WEB THICKNESS is optional input. Omit both entries if the section consists of exterior girders only.

EXTERIOR GIRDERS TYPE is shown on a sketch on the input form. The exterior girder may be omitted by entering it as a Type 9. Type 0 is assumed if no type is given.

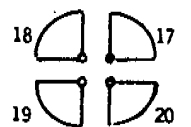
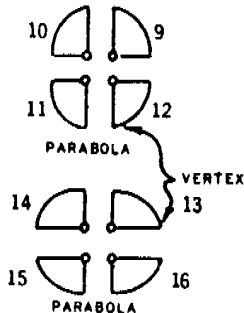
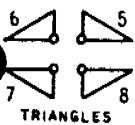
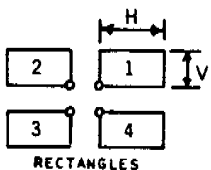
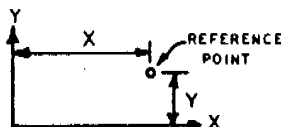
WEB THICKNESS is measured perpendicular to the girder face and is assumed to be equal to the interior girder thickness if omitted. The exterior girder FACTOR must be given for types 1, 2 and 3 to the nearest .01 foot.

Standard 4" fillets are assumed as shown.

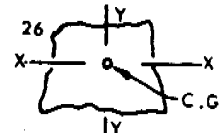
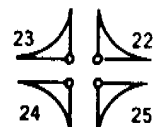
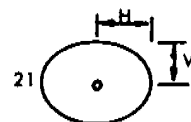


TYPE 9 MEANS NO EXTERIOR GIRDER

PART CODES



CIRCLES if $V = H$ or ELLIPSES if $V \neq H$



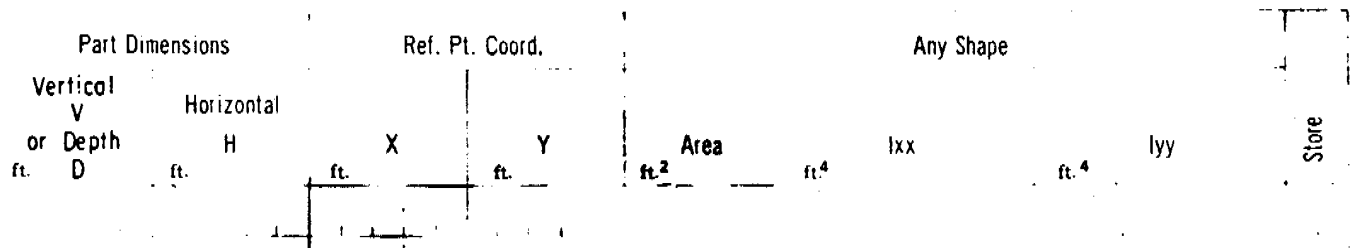
ANY SHAPE

SECTION PROPERTIES BY PARTS

Normally, this input option is used to supplement the frame description data, and/or the superstructure sections data, to produce section and member properties. It may also be used as a stand alone submittal, producing just section properties.

MEMBER NO., CROSS SECTION LOCATION, STORE and RECALL are described in the SUPERSTRUCTURE SECTIONS part of these instructions.

Sections are built by adding or subtracting the parts shown. PART CODE identifies the shape of the figure being defined. If no part code is given, but ANY SHAPE data is input, the part code is assumed to be 26. Part code 27 is used to give a depth to the cross section. The depth is used to calculate stresses.



SIGN is used to subtract a given part from a gross section or to build a section with negative properties.

VERTICAL and HORIZONTAL dimensions are required input if part codes 1 thru 25 are used. Area, Ixx and Iyy are not used for these part types. Part Code 26 may be used to define any shape with known properties. Area, Ixx, Iyy, and the reference points X and Y should be given.

The moment of inertia about the Y-Y axis is not used in the analysis of the frame, therefore, it is not necessary to give x or Iyy for any part. Note that omitting this data will produce false answers for Iyy.

LOAD DATA

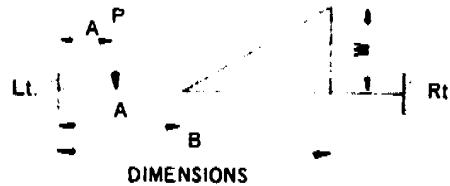
TRIAL NO represent different loading conditions submitted for a single problem. Trial no. 00 is taken to be dead load which supplements the dead load given in the frame description. Bent Caps and diaphragms would be examples

of trial no. 00 loads. Trial no. 1 is assumed to be added dead loads, i.e., barrier railing, wearing surface, signs. Added dead load is any loading which is placed on a frame in its final condition. This condition usually has an effect only on prestressed frames.

MEMBER NO. refer to the member to which the load is applied. Any or all members may be loaded in a given trial.

* CODE

- L=Max. W on left
- R=Max. W on right
- U=Uniform Load
- P=Point Load



Trial No.	Member No.	Loads		Code*	A ft.	B ft.	FEMs*		Deflections Sidesway S	Comments
		W or P k/ft or k					Left ft-k	Right ft-k		

If the dimensions "A" and "B" happen to be greater than the member length, the member length is used and a warning message is printed.

Enter an 'S' in the sidesway column to obtain sideswayed results for all loads of a given trial. Only one entry per trial is required.

Up to 17 characters of COMMENTS may be made per line on which other data (trial no., etc.) are given. If a single comment covers more than one line, the comment lines may not print in order.

SUPERSTRUCTURE LIVE LOAD

This feature uses two types of input data, MEMBER DATA and LIVE LOAD DATA. Combinations of both or either by itself may be used to produce horizontal member moment and shear envelopes, and the maximum vertical member moments and reactions due to a HS20-44 AASHTO or a multi-axle live loading as well as alternative, standard construction, and sidewalk live loadings. Upon request, influence line ordinates will also be produced.

Plotted results may be obtained for the dead load and live load moment and shear diagrams and for the influence line diagram. All plots must start with the first member in the frame and will continue to the last member.

INFLUENCE LINES, both ordinates and plots, may be obtained by entering a check mark (✓) in the proper box on the input form. Member No. 1 and Number of Live Load Lanes must also be given.

Separate plots will be produced for each horizontal member. Each plot frame will contain the influence lines for the .2L, .4L, .5L, .6L, .8L and 1.0L positions along a particular member. Each influence line is delineated by a separate line code shown on the plot.

MOMENT and SHEAR plotted results may be obtained by entering a code shown in the table below. To obtain dead load plots only enter Member No. 1 and the plot code, but leave the Number of Live Loads blank. To obtain plots with live loads, the Number of Live Load Lanes as well as Member No. 1 and the plot code must be input.

RESISTING MOMENT OF UNIT STEEL values may be given and will cause tick marks to appear on the moment diagrams.

Entry Code	Program Response
Blank or Ø	No plot
1	Plot Moment & Shear Diagram for DL+LL and DL.
2	Plot Moment diagram for DL+LL and DL.
3	Plot Shear diagram for DL+LL and DL.
4	Plot Moment & Shear diagram for DL only.
5	Plot Moment diagram for DL only.
6	Plot shear diagram for DL only.
7	Plot Moment & Shear diagram for LL only.
8	Plot Moment diagram for LL only.
9	Plot Shear diagram for LL only.

The minimum input data required to produce results due to a HS20-44 AASHTO or multi-axle live loading is the NUMBER of LIVE LOAD LANES applied to the horizontal members of the frame. Although this data may be given as MEMBER and/or LIVE LOAD DATA, it will normally be given as MEMBER DATA. Reduction in the number of substructure lanes due to improbable coincident maximum loading is not performed by this feature, but the reduced data may be given by the user.

Unless otherwise specified, AASHTO IMPACT FACTORS will be included in the calculations and therefore, should not be included in the NUMBER of LIVE LOAD LANES.

Superstructure Live Load input data must be accompanied by Frame Description input data. Superstructure Sections, Section Properties by Parts, and the Load Data input options may also be used, producing results as described in earlier instructions.

When the Superstructure Live Load feature is used, the frame is subject to the following limitations:

1. The structure must be a rectangular single story plane frame.
2. Horizontal members must be numbered consecutively starting with 01, up to a maximum of 25.
3. Cantilevered members are not allowed.

MEMBER DATA

Member No.	Number of Live Load Lanes				Plot Data		Moment & Shear	Influence Lines P-13	COMMENTS
	Superstructure		Substructure		Resisting Moment of Unit Steel				
	Lt. End	Rt. End	Lt.	Rt.	Positive	Negative			

When using this input option, enter the horizontal MEMBER No. to which the line of data corresponds.

The NUMBER of LIVE LOAD LANES is classified by results that pertain to the SUPERSTRUCTURE and SUBSTRUCTURE. They may be varied linearly from the LT. END to the RT. END of the member. When given as MEMBER DATA, the NUMBER OF LIVE LOAD LANES must be given for the LT. END of SUPERSTRUCTURE MEMBER NO. 01. SUBSTRUCTURE MEMBER 01 defaults to 1.0 L. L. Lane when left blank. In both cases, when an entry is made, it is assumed to be constant for both ends of all subsequent members until another entry is made. When the value for the LT. END of a member is not given, it is assumed to equal that of the RT. END of the previous member. The value at the RT. END of a member, when not given, is assumed to equal that of the LT. END of the next member if it is given. Otherwise, the value at the RT. END is assumed to equal that of the LT. END of the same member.

A check mark under P-13 will cause the program to generate live loads as follows for one live load lane.

Each axle of a P-5 truck is placed at each 10th point of each span. Axles are arranged for the truck moving in both directions.

One heavy axle of the P-Series truck is added and the above procedure repeated. This process continues until the P-13 truck is checked.

LIVE LOAD DATA

L. L. No.	Truck - (1 Lane)					Lane - (1 Lane)			No Impact ✓	Number of Live Load Lanes
	P ₁ Kips	D ₁ Ft.	P ₂ Kips	D ₂ Ft.	P ₃ Kips	Uniform Kips/ft.	Moment Rider Kips	Shear Rider Kips		
1										
2										
3										

This input option need be used only when the LIVE LOAD DATA consists of something other than the standard HS20-44 AASHTO live loading plus impact, provided that the NUMBER of LIVE LOAD LANES is given as MEMBER DATA.

If the TRUCK and LANE data for L. L. No. 1 is not given, HS20-44 AASHTO loading (without alternative) is assumed. If either or both is given for L. L. No. 1, it replaces the HS20-44 loading. Alternative loading if required, should be entered as described below.

TRUCK and/or LANE data entries for L. L. No.'s 2 or 3 produce separate results in addition to L. L. No. 1.

The TRUCK load for one lane may consist of one, two or three axles. It is defined by entering the axle loads P₁, P₂, and P₃ (0.1 kips) and their spacing D₁ and D₂ (0.1 ft).

The LANE load for one lane may consist of a UNIFORM load (kips/ft) and/or MOMENT RIDER (0.1 kips) and/or SHEAR RIDER (0.1 kips).

Enter a check mark (✓) when NO IMPACT is desired for the particular L. L. NO.

When the NUMBER of LIVE LOAD LANES is given as LIVE LOAD DATA, it overrides that given as MEMBER DATA. It is constant for all horizontal members and used both for SUPERSTRUCTURE and SUBSTRUCTURE results.

Up to 22 characters of COMMENTS may be made per L. L. No. on which other data is given. When no data is entered for L. L. NO. 1, the comment defaults to 'HS20-44 AASHTO LOADING WITHOUT ALTERNATIVE.'

LIVE LOAD GENERATOR

The live load generator input form is similar to the superstructure Live Load Form. Entries on this form will allow AREA railroad or special live load description. Entries in the "Member Data" portion of the form describes the number of lanes that will be loaded with the special truck described on the "Live Load Data" portion of the form.

MEMBER DATA

Update		Member No.	Number of Live Load Lanes				Plot Date				
C O D E	Line No.		Superstructure		Substructure		Resisting Moment of Unit Steel		Moment & Shear Scale	Influence Lines	
			Lt. End	Rt. End	Lt.	Rt.	Positive	Negative			

LIVE LOAD DATA

Update		L.L. No.	Multi Axle Live Loading							
C O D E	Line No.		P _N	D ₁	P _{N+1}	D ₂	P _{N+2}	D ₃	P _{N+3}	D ₄
			Kips	Ft.	Kips	Ft.	Kips	Ft.	Kips	Ft.
		4								
		4								

					OVER LOAD		Cooper Loading	NO IMPACT ✓	COMBINE	CARD CONTROL
P N+4	D 5	P N+5	D 6	P N+6	Color Code	No of Axles				
Kips	Ft.	Kips	Ft.	Kips						
										1
										2

Live load data is supplied for each axle of the proposed special vehicle. Axle loads in kips and axle spacing in feet may be continued for a maximum of two lines per live load number.

OVERLOAD, COOPER LOADING, and COMBINE are data entry areas reserved for future enhancements.

Impact will be considered unless a check mark (✓) is provided in the "NO IMPACT" field.

LIVE LOAD RESULTS

LIVE LOAD DIAGNOSTICS, if present, will indicate that the live load limitations placed on the frame have been violated or an error was made in the superstructure live load input data.

SUPERSTRUCTURE LIVE LOAD input data is reported as given or assumed.

For each L. L. NO. for which LIVE LOAD DATA was given or assumed, the following results are reported for the tenth points of the horizontal members.

1. NEGATIVE LIVE LOAD MOMENT ENVELOPE AND ASSOCIATED SHEARS. HORIZONTAL MEMBER STRESSES - TOP AND BOTTOM FIBRE.
2. DEAD LOAD PLUS NEGATIVE LIVE LOAD MOMENT ENVELOPE. HORIZONTAL MEMBER STRESSES - TOP AND BOTTOM FIBRE.

3. POSITIVE LIVE LOAD MOMENT ENVELOPE AND ASSOCIATED SHEARS.
4. DEAD LOAD PLUS POSITIVE LIVE LOAD MOMENT ENVELOPE. HORIZONTAL MEMBER STRESSES - TOP AND BOTTOM FIBRE.
5. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS. (POSITIVE, NEGATIVE AND RANGE)
6. DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPES. (POSITIVE AND NEGATIVE)

The dead load plus live load envelopes are reported only if the dead load analysis was performed with all horizontal members loaded. The dead load results are obtained from Trial No. 0 of the basic system as described in earlier instructions.

Be careful when using the dead load plus live load shear envelopes. The dead load shears are computed, and only one ordinate is saved at each tenth point. Therefore, when the dead load includes concentrated loads, the abrupt steps are not shown. If the load is exactly at a tenth point, only the most positive value is retained.

LIVE LOAD SUPPORT RESULTS are also reported for each L. L. NO. for which LIVE LOAD DATA was given or assumed. Dead load is not included. Impact is included, unless otherwise specified.

The MAX. POSITIVE AND NEGATIVE (uplift) AXIAL LOAD at each SUPPORT or TOP of VERTICAL MEMBER is reported, as is TOP and BOTTOM vertical member moments created by the same loading.

The MAX POSITIVE and NEGATIVE LONGITUDINAL MOMENT at the TOP of each VERTICAL MEMBER is reported, as is the AXIAL LOAD and BOTTOM vertical member moment created by the same loading.

Beam sign convention is used for all live load results. Units are kips and feet.

INFLUENCE LINE RESULTS

When requested, the following types of INFLUENCE LINES are reported. Ordinates for each are given at the tenth points and at hinges.

The INFLUENCE LINES for GIRDER MOMENT, reported for each tenth point of the horizontal members, are extended two spans on each side of the span with the influence point.

The INFLUENCE LINES for GIRDER SHEAR, reported for the left end of each horizontal member, are extended two spans on each side of the span with the influence point. From this line, the influence line for shear at any point in that member may be constructed.

The INFLUENCE LINES for REACTION at TOP of COLUMN (or support if no column is present) are extended two spans on each side of the column.

The INFLUENCE LINES for MOMENT at TOP OF COLUMN are extended two spans on each side of the column.

PRESTRESSED DATA

The prestressed data form is used to describe a prestressed cable path which is to be applied to a previously described frame and its dead load, added dead load and live load. The prestressing may be part length, and/or multiple tendon. Input, as described below, consists of three types of information: 1) orientation, 2) cable path geometry, and 3) specifications.

TRIAL NO. is the number of the input cable path configuration. Different cable path geometry or specifications can be tried in a single submittal by varying the trial number.

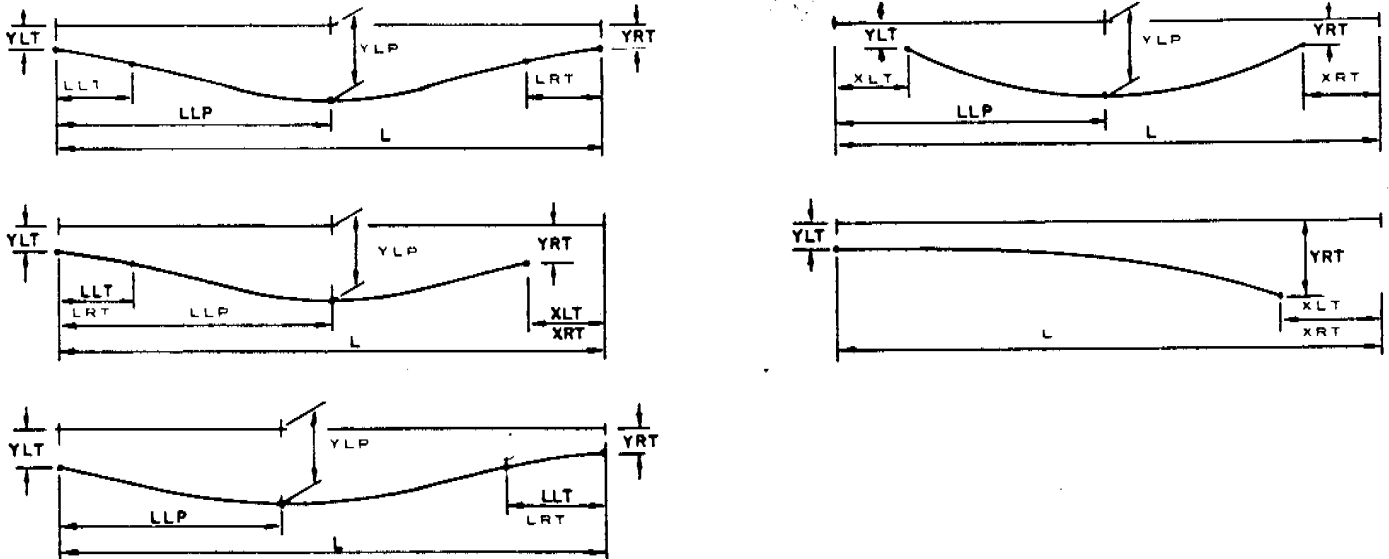
FRAME NO. is the number of structural frame. A frame is defined as the area between hinge and/or end supports. For example, an eight span structure with 2 intermediate hinges would have 3 frames.

PATH NO. is a number or letter used to identify the various cable paths in a multiple tendon prestressed frame. The effects of the multiple paths in the same trial and frame are all added together. When multiple paths are defined, only one path may have an unknown jacking force.

MEMBER NO. is the member for which prestress information is being input. The member number is the same as is shown on the Frame Description input form. Up to 15 horizontal members can be input if prestressed input is submitted. Member numbers need not begin with 1.

Trial No	Frame No	Path No	Member No	LLT	LLP	LRT	YLT	YLP	YRT	XLT	XRT
				%	%	%	ft	ft	ft	ft	ft

The cable path geometry is described by defining a series of four parabolic sections per span. The end of cable locations must also be given.



LLT, LLP, and LRT are the horizontal locations of the points of inflection of the cable. The abbreviations, LLT; LLP and LRT mean "Length to left point", "Length to low point" and "Length to right point." The values to be input are in percent of span, accurate to the nearest 1%. Note that the illustrated path configurations or the illustrated configurations reversed are the only allowable paths. LLP is always the length from the left end of the span to the low point.

YLT, YLP and YRT are the vertical offsets from the top of the deck to the C.G. of the prestress force as shown on the sketch. The abbreviations YLT, YLP and YRT mean "Offset to left point", "Offset to low point", and "Offset to right point." The values are input to the nearest 0.01 of a foot.

XLT and XRT are the horizontal distances from the end of span to the ends of the cable path. The abbreviations XLT and XRT, mean "distance to left end of cable," and "distance to right end of cable."

U is the friction curvature coefficient. If left blank, the default value of 0.25 will be used. A separate value may be input for each span.

K is the friction wobble coefficient per foot of stressing steel. If left blank, a default value of 0.0002 will be used. A separate value may be input for each span.

fs is the ultimate strength of the prestressing steel in kips per square inch. If left blank, a default value of 270 ksi will be used. Only one value may be input for each path.

Specifications										
u	k	fs	% Jack	Anchor Set		Allow. Tension Spec. %	P-Jack KIPS	fc KSI	% Shortening	Losses KSI
$\times 10^{-2}$	$\times 10^{-4}$	KSI		End	LT RT In In					

%JACK is the maximum allowable temporary jacking stress expressed as a percent of the ultimate strength of the prestressing steel. If left blank, a default value of 75% is used. Only one value may be input for each path. If both end stressing is requested, the same value for % Jack is used at each end.

END is the input to request jacking location. Enter "L" for left end jacking enter "R" for right end jacking, enter "B" for both end jacking. If left blank, a default value of "B" is used. Only one value may be entered for each path.

ANCHOR SET, LT, and RT is the length, in eighths of an inch, of the anchor set. If one end jacking was requested no entry need be made for the anchor set of the non-jacked end. Only one value for anchor set left, and one value for anchor set right may be entered per path. If left blank, a default value of 5/8" is used.

ALLOWABLE TENSION is the given value of the allowable maximum tension stress for which the frame is to be designed. Two methods of input are provided. If a check (✓) is placed in the SPEC input field, the allowable tension will be calculated using the specifications in the Bridge Planning and Design Manual, Volume I. The formula is $6\sqrt{f'c}$.

If an entry is made in the % field, the allowable tension is the entered % times $6\sqrt{f'c}$. Only one choice is allowed and only one entry is allowed per path. If left blank, the program will design for no tension (if possible).

P-JACK is the input prestress force in kips. If a value for P-JACK is input for all paths in a given trial and frame, then the program only analyzes the structure and reports the effects. If multiple path prestressing is described, all values of P-JACK except one must be given. The path with no value will have its prestress force designed by the program based on full DL + added DL + LL + I. Stresses are then checked for both the DL + PS and DL + added DL + PS cases to assure that tension in these cases does not exceed zero. If tension is detected, P-JACK is redesigned to eliminate the tension and a warning message is printed. When this occurs, the full allowable tension value may not appear in the final stresses.

f'c is the required concrete strength. This value is used as the basis for calculating the allowable tension. If left blank, a default value of 3.5 ksi will be used.

% SHORTENING is the percent of theoretical elastic shortening to be included in the prestressing calculations based on the final prestress force coefficients. Only those frames with columns affected by shortening will be considered. If left blank, a default value of 100% is used. To eliminate shortening, enter a zero. To obtain any other even 10% increment enter its multiple of 10%.

Losses (ksi) are the losses due to creep and shrinkage. If left blank, a default value of 32 ksi is used.

RESULTS

The following items are listed as they appear in the output for each problem. Whether a particular item appears, depends on the nature of the problem.

First, the FRAME DESCRIPTION input is reported as given, except for the deflection and sideways entries, which do not appear.

SECTION PROPERTIES are reported for each section described with the Section Properties by Parts input option. The input is reported as given, followed by the area, centroid location with respect to the X Y coordinate system chosen, and the moments of inertia about the centroidal X-X and Y-Y axes.

When the above sections supplement a frame member, MEMBER PROPERTIES about the X-X axis are reported. They are the length of the member, minimum moment of inertia about the X-X axis, and the relative stiffness (small k) and carry over factors.

The absence on any message under FRAME DIAGNOSTICS, indicates that no errors have been detected in the data which makes up the frame. The presence of an error message terminates processing of the problem. If the first diagnostic states that 'Errors have been found in either the frame description or cross section data', this indicates that error messages have been printed somewhere in the preceding output of the problem. Although processing is terminated, Load Data input is reported as given, along with error messages pertaining to it.

FRAME PROPERTIES is the result of combining the Frame Description with the Member Properties. Carry Over and Distribution Factors are adjusted for pinned end conditions. At this point, all data pertaining to the frame should be reviewed to determine if it is reasonable and describes the frame as intended.

For each trial, the LOADINGS are reported as given. Errors, if any, in Load Data are reported, and result in processing being terminated for the trial.

FIXED END MOMENTS are the total FEM's for a trial and are adjusted for pinned end conditions.

Distributed MOMENTS and SHEARS are reported at the one-tenth points for each member. In each case, the horizontal members are separated from the vertical members. Beam sign convention is used.

COLUMN REACTIONS are calculated on the assumption that the user followed the rule that the left end of the column was the bottom. Any deviation from this rule will yield incorrect reactions.

The TANGENTIAL ROTATIONS at the ends of each member are measured from the unloaded position, with clockwise being positive.

DEFLECTIONS are measured from the unload position. Positive is downward for horizontal members and to the right for vertical members.

The MAX. POSITIVE AND NEGATIVE (uplift) AXIAL LOAD at each SUPPORT or TOP of VERTICAL MEMBER is reported, as is TOP and BOTTOM vertical member moments created by the same loading.

The MAX POSITIVE and NEGATIVE LONGITUDINAL MOMENT at the TOP of each VERTICAL MEMBER is reported, as is the AXIAL LOAD and BOTTOM vertical member moment created by the same loading.

Beam sign convention is used for all live load results. Units are kips and feet.

INFLUENCE LINE RESULTS

When requested, the following types of INFLUENCE LINES are reported. Ordinates for each are given at the tenth points and at hinges.

The INFLUENCE LINES for GIRDER MOMENT, reported for each tenth point of the horizontal members, are extended two spans on each side of the span with the influence point.

The INFLUENCE LINES for GIRDER SHEAR, reported for the left end of each horizontal member, are extended two spans on each side of the span with the influence point. From this line, the influence line for shear at any point in that member may be constructed.

The INFLUENCE LINES for REACTION at TOP of COLUMN (or support if no column is present) are extended two spans on each side of the column.

The INFLUENCE LINES for MOMENT at TOP of COLUMN are extended two spans on each side of the column.

MODIFICATIONS TO EXISTING SYSTEM

Due to popular demand, the following modifications were made to the existing system. Details of the basis system are described in earlier instructions.

On FRAME DESCRIPTION input, if UNIT WT. is given (accidentally) and the section data (area) was not, the unit wt. is not used and a warning message is printed.

When using SECTION PROPERTIES by PARTS input, if the PART CODE is omitted and data given for AREA and I_{xx} , but not for the PART DIMENSIONS V and H, a message is printed stating that part code 26 (any shape) was assumed.

LIVE LOAD RESULTS

LIVE LOAD DIAGNOSTICS, if present, will indicate that the live load limitations placed on the frame have been violated or an error was made in the superstructure live load input data.

SUPERSTRUCTURE LIVE LOAD input data is reported as given or assumed.

For each L. L. NO. for which LIVE LOAD DATA was given or assumed, the following results are reported for the tenth points of the horizontal members.

1. NEGATIVE LIVE LOAD MOMENT ENVELOPE
2. DEAD LOAD PLUS NEGATIVE LIVE LOAD MOMENT ENVELOPE
3. POSITIVE LIVE LOAD MOMENT ENVELOPE
4. DEAD LOAD PLUS POSITIVE LIVE LOAD MOMENT ENVELOPE
5. LIVE LOAD SHEAR ENVELOPES
(POSITIVE, NEGATIVE and RANGE)
6. DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPES (POSITIVE and NEGATIVE)

The dead load plus live load envelopes are reported only if the dead load analysis was performed with all horizontal members loaded. The dead load results are obtained from Trial No. 0 of the basic system as described in earlier instructions.

Be careful when using the dead load plus live load shear envelopes. The dead load shears are computed, and only one ordinate is saved at each tenth point. Therefore, when the dead load includes concentrated loads, the abrupt steps are not shown. If the load is exactly at a tenth point, only the most positive value is retained.

LIVE LOAD SUPPORT RESULTS are also reported for each L.L. NO. for which LIVE LOAD DATA was given or assumed. Dead load is not included. Impact is included, unless otherwise specified.

If the LOAD DATA dimensions A or B happen to be greater than the member length, the latter is assumed for these dimensions and a message is printed.

The Dead Load analysis (TRIAL NO. 0) will now be performed even if all horizontal members are not loaded. An appropriate message is printed. The analysis performed with this inconsistency will not be added to Live Load results.

MOMENT AND SHEAR PLOTTED RESULTS

Dead load moments and shears are plotted as dashed lines. Live load moments and shears are plotted as solid lines from enveloped data as presented in the printed output. Plots will be annotated to show if the Dead Load is included or excluded from the Live Load envelopes.

INFLUENCE LINE PLOTTED RESULTS

When influence lines are requested the plotted results will produce separate plot frames for each horizontal member. Each plot frame will contain the influence lines for the .2L, .4L, .5L, .6L, .8L, and 1.0L positions along the particular member. Each influence line is delineated by a separate line code shown on the plot.

SAMPLE PROBLEMS

The following sample problems are intended to illustrate the major features of the program Frame System. Problem complexity increases from problem 1 to problem 5 with an expectation that prior problem concepts have been mastered. The following descriptions show which feature the sample problems illustrate:

- Sample problem 1 is an example of the use of the input forms, Frame Description, Section Properties by Parts, and Load Data.
- Sample problem 2 is an example of the use of the Superstructure Section input form and the automatic generation of flaring superstructure member properties.
- Sample problem 3 is an example of the use of the Superstructure Live Load input form. Plotted and printed results for influence lines and HS20-44 Live Load moment and shear envelopes are produced by this problem.
- Sample problem 4 is an example of the use of the Live Load Generator input form. Live Load envelopes are printed for a family of overload trucks consisting of the truck described on the form and successive trucks formed by removal of axles until three axles remain.
- Sample problem 5 is an example of the use of the Prestressed Data input form. Prestress analysis and calculation of jacking force required is provided with the analysis.

SAMPLE PROBLEM 1

PROBLEM

A. General

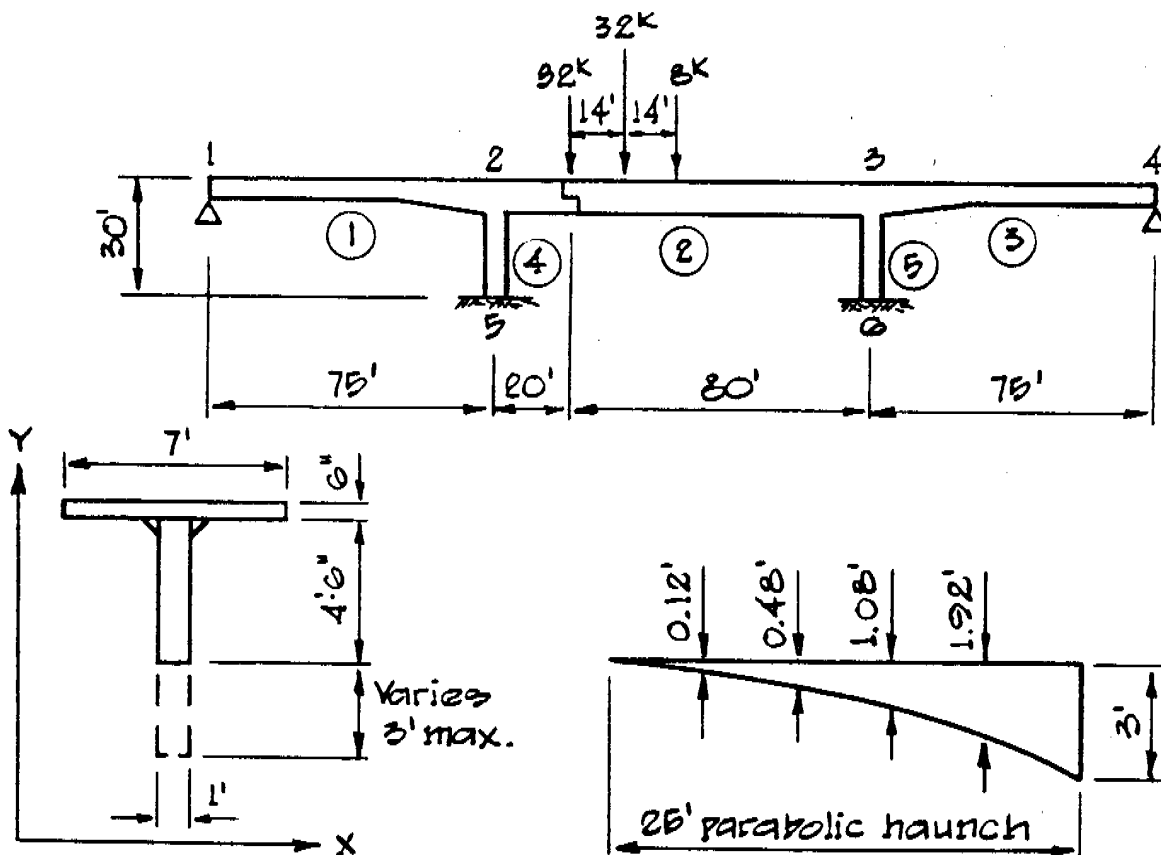
Three-span bridge with one expansion joint. Span properties to computed by program.

B. Loading

Dead load of bent caps and hinge as coded on Load Data form trial 00. Live load as coded on Load Data form trial 01.

C. Section Properties

Columns are prismatic as coded on Frame Description form. Superstructure cross section varies as per Figure 5 and is coded on the Section Properties By Parts form.



DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - FRAME DESCRIPTION
 DS - D93 (REV. 2-75)

BDE0AA

IDENT. SOURCE CHARGE EXPENDITURE SPECIAL DESIGNATION PROGRAM
 DIST. GR. BATCH PROB. DIST. UNIT DIST. UNIT AUTHORIZATION WHEN APPLICABLE NUMBER
 14T 0701 1403314033910002
 S/C 2091, 7310 S/C 2091 B D E 0 3 5

Page 1 of 3
 Name Example #1
 Phone 445-6519

Update	Line No.	Member No.	End Joint		Length	Min. I	Hinge Location or Support Width	Dead Load		Member Properties				Recall	D.L.				
			Lt.	Rt.				Uniform	Unit	-K-		-C-				Member	Reverses	Deflections	Sideway
				Condition	ft.	ft ⁴	ft	k/ft	pcf	Stiffness Factor	Carry Over Factor	Lt.	Rt.	Lt.	Rt.	R	R	S	
	1	1	2	P	6	750		180	150										
	2	2	3		6	1000	200	180	150										
	3	3	4																
	4	5	2		300	1000		600											
	5	6	3		300	1000		600											

S/C 7310

END CONDITION
 C - Cantilever
 P - Pin
 R - Roller

DIRECTION
 G or H - Horizontal

Hinge Location
 Lt. Rt.

DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - LOAD DATA
 DS - D93 (REV. 2-75)

BDE0AA

IDENT. * CODE
 DIST. GR. BATCH PROB. L=Max W on left
 14T 0701 R=Max W on right
 S/C 7318 U=Uniform Load
 P=Point Load

Page 3 of 3
 Name Example #1
 Phone

Update	Line No.	Trial No.	Member No.	Loads		FEMs*		Comments		
				W or P	* CODE	A	B		Left	Right
				k/ft or k	ft.	ft	ft - k	ft - k	Deflections	Sideway
	0002			25200P	00					
				21000P	200					
				25200P	1000					
	0102			32000P	200					
				32000P	340					
				8.000P	480					

S/C 7318

*When FEMs are given, they are not calculated for any load on that member.

DEPARTMENT OF TRANSPORTATION
 FRAME SYSTEM - SECTION PROPERTIES BY PARTS

BDE0AA

DS-D94 (REV. 2-75)

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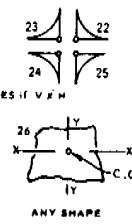
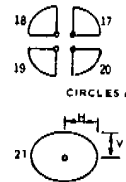
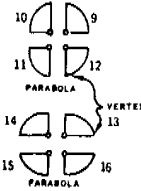
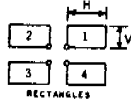
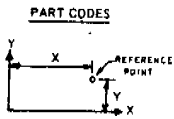
IDENT.
 DIST. GROUP BATCH PROB.
 14T 0701
 S/C 2081, 7312

SOURCE CHARGE EXPENDITURE SPECIAL DESIGNATION PROGRAM
 DIST. UNIT DIST. UNIT AUTHORIZATION WHEN APPLICABLE NUMBER
 B. D. E. 3 5.

Name Example #1

Phone

Update	Line No.	Member No.	CROSS SECTION LOCATION	Recall	Part Code	Part Dimensions		Ref. Pt. Coord.		Area	Any Shape		
						Vertical V or Depth D	Horizontal H	X	Y		ft ²	ft ⁴	ft ⁴
		01	00		01	50	700	00	750				
					01	450	100	300	300				
					07	33	33	300	750				
					08	33	33	400	750				01
			50001										
			600		04	48	100	300	300				
			650			108							
			700			192							
			750			300							02
		02	0002										



IDENT		101 07 01		FRAME SYSTEM				MAY, 01, 1975				PAGE 1				
FRAME DESCRIPTION																
LINE NO.	MEM NO.	JOINT NO.	END JOINT NO.	REV	SPAN	I	SUPPORT ON HINGE	E	DEAD LOAD UNIFORM SFC		L	K	WT	CARRY OVER FACTORS	RECALL MEM	
		LT	RT											LT	RT	
0010	1	1	2	P	6	75.0	0.0	0.0	0.	0.180	150.	0.0	0.0	0.0	0.0	
0020	2	2	3		6	100.0	0.0	20.0	0.	0.180	150.	0.0	0.0	0.0	0.0	
0030	3	3	4			0.0	0.0	0.0	0.	0.0	0.	0.0	0.0	0.0	0.0	010
0040	4	5	2			30.0	10.00	0.0	0.	0.000	0.	0.0	0.0	0.0	0.0	
0050	5	6	3			30.0	10.00	0.0	0.	0.000	0.	0.0	0.0	0.0	0.0	

OUTPUT DESCRIPTION

Page 1 of Frame System output reports the frame description input data. This page is provided to allow verification of input data as received from the keypunch section. If stiffness factor is given use relative stiffness factor on input sheet (i.e., for fixed prismatic beam use 4).

SECTION PROPERTIES

LINE NO.	MEM	LUC	RECALL	+	CODE	V	H	X	Y	AREA	INERTIAS OF PARTS		STIFF
											IXX	IYY	
0010	1	0.0			1	0.50	7.00	0.0	7.50	0.0	0.0	0.0	0.0
0040	1	0.0			1	4.50	1.00	3.00	3.00	0.0	0.0	0.0	0.0
0030	1	0.0			7	0.33	0.33	3.00	7.50	0.0	0.0	0.0	0.0
0020	1	0.0			8	0.33	0.33	4.00	7.50	0.0	0.0	0.0	01

AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID	
	X	Y	X=X	Y=Y
8.11	3.50	6.36	20.09	14.71

LINE NO.	MEM	LUC	RECALL	+	CODE	V	H	X	Y	AREA	INERTIAS OF PARTS		STIFF
											IXX	IYY	
0050	1	50.0	01		0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID	
	X	Y	X=X	Y=Y
8.11	3.50	6.36	20.09	14.71

LINE NO.	MEM	LUC	RECALL	+	CODE	V	H	X	Y	AREA	INERTIAS OF PARTS		STIFF
											IXX	IYY	
0060	1	60.0	01		4	0.48	1.00	3.00	3.00	0.0	0.0	0.0	0.0

AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID	
	X	Y	X=X	Y=Y
8.59	3.50	6.16	25.97	14.75

Pages 2 through 5 reports section properties at user defined cross-section locations along the members. The output is arranged in increasing order of member number and increasing order of cross-section location starting from the left end of the member. Each line of input data is printed for verification followed by a calculated value of area, centroid location, and moment of inertia about centroid for the total section.

IDENT 141 07 01 FRAME SYSTEM MAY, 01, 1975 PAGE 3

SECTION PROPERTIES

LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	Ixx	Iyy	STORE
0070	1	65.0	01		4	1.00	1.00	3.50	5.00	0.0	0.0	0.0	
		RECALL	1					3.50	0.30	0.11	20.09	14.71	
		AREA		CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
				X Y		X=X Y=Y							
		9.19		3.50 5.90		34.67				14.80			

LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	Ixx	Iyy	STORE
0080	1	70.0	01		4	1.92	1.00	3.50	3.00	0.0	0.0	0.0	
		RECALL	1					3.50	0.30	0.11	20.09	14.71	
		AREA		CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
				X Y		X=X Y=Y							
		10.03		3.50 5.53		49.62				14.87			

LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	Ixx	Iyy	STORE
0090	1	75.0	01		4	3.00	1.00	3.50	3.00	0.0	0.0	0.0	02
		RECALL	1					3.50	0.30	0.11	20.09	14.71	
		AREA		CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
				X Y		X=X Y=Y							
		11.11		3.50 5.05		74.02				14.96			

IDENT 141 07 01 FRAME SYSTEM MAY, 01, 1975 PAGE 4

MEMBER 1 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS	CARRY OVER
		LT WT	LT WT
75.0	20.09	4.307 6.000	0.655 0.471

IDENT 141 07 01 FRAME SYSTEM MAY, 01, 1975 PAGE 5

SECTION PROPERTIES

LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	Ixx	Iyy	STORE
0100	2	0.0	02		0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
		RECALL	2					3.50	5.05	11.11	74.02	14.96	
		AREA		CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
				X Y		X=X Y=Y							
		11.11		3.50 5.05		74.02				14.96			

MEMBER 2 PROPERTIES

HINGE AT LOCATION	LENGTH	MIN INERTIA	STIFFNESS	CARRY OVER
			LT WT	LT WT
20.0	100.0	74.02	0.231 3.692	4.000 0.250

Page 5 reports section properties at the beginning or left hand side of member 2. Following the section properties output is the member properties calculated for member 2. The assumption for calculation of member properties is that the member is prismatic since only one cross-section location was given for the member. Output stiffness and carryover factors assume that the member end conditions are fixed-fixed. Member length is obtained from the Frame Description form.

IDENT 141 07 01

FRAME SYSTEM

MAY, 01, 1975

PAGE 6

FRAME DIAGNOSTICS

NO ERRORS FOUND

FRAME PROPERTIES

MEM NO	JT		END CONN		DIR	SPAN	I	SUPPORT OR HINGE	E	CARRY OVER FACTORS		DISTRIBUTION FACTORS	
	LT	RT	LT	RT						LT	RT	LT	RT
1	1	2	P	G	G	75.0	20.09	0.0	750.	0.055	0.0	0.0	0.428
2	2	3		G	G	100.0	74.02	20.0	750.	4.000	0.250	0.005	0.527
3	3	4	P	G	G	75.0	20.09	0.0	750.	0.0	0.055	0.210	0.0
4	5	2				30.0	10.00	0.0	750.	0.500	0.500	0.0	0.507
5	6	3				30.0	10.00	0.0	750.	0.500	0.500	0.0	0.257

Page 6 reports the frame properties as assembled from the Frame Description and Section Properties by Parts forms. The message "no errors found" indicates that the program will attempt to process the loadings specified by the user. If an error message is encountered at this point further load processing is terminated out loading conditions are scanned for Syntax errors.

IDENT 141 07 01

FRAME SYSTEM

MAY, 01, 1975

PAGE 7

LOAD DATA TRIAL 0

LINE	MEM	W	OR	P	LOAD CODE	FIXED END MOMENTS			COMMENTS
						A	B	DEFLT	
0030	2	25,200			P	0.0	0.0	0.	CAP WT.
0020	2	21,000			P	20.0	0.0	0.	HINGE WT.
0010	2	25,200			P	100.0	0.0	0.	CAP WT.

FIXED END MOMENTS TRIAL 0

MEM NO	FIXED END MOMENTS		MEM NO	FIXED END MOMENTS		MEM NO	FIXED END MOMENTS	
	LT	RT		LT	RT		LT	RT
1	0.	-1250.	2	-1869.	-1586.	3	-1250.	0.
4	0.	0.	5	0.	0.			

Page 7 reports the input data received from the load data form. Data for each trial is assembled together and the resulting fixed end moments are printed for all loads of the trial. Fixed end moments have been adjusted for pinned or roller end conditions.

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*** SIDESWAY NOT CONSIDERED. ***

HORIZONTAL MEMBER MOMENTS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	202.	325.	369.	336.	223.	32.	-238.	-587.	-1020.	-1544.
2	-1893.	-854.	0.	459.	734.	824.	730.	451.	-13.	-662.	-1495.
3	-1362.	-456.	-441.	-110.	141.	314.	408.	424.	361.	220.	0.

WARNING - MEMBER DEPTHS WERE NOT USED FOR ALL MEMBERS SIN STRESSES WERE NOT CALC.

VERTICAL MEMBER MOMENTS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
4	174.	122.	70.	17.	-35.	-87.	-140.	-192.	-244.	-297.	-349.
5	-66.	-46.	-27.	-7.	13.	33.	53.	73.	93.	113.	133.

HORIZONTAL MEMBER SHEARS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	32.1	21.7	11.2	0.7	-9.8	-20.2	-30.7	-41.2	-52.0	-63.0	-76.5
2	136.3	94.0	76.2	36.7	16.2	-0.2	-18.7	-37.1	-55.0	-74.1	-117.7
3	74.1	61.1	49.6	38.8	28.3	17.0	7.3	-3.1	-13.0	-24.1	-34.6

VERTICAL MEMBER SHEARS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
4	-17.4	-17.4	-17.4	-17.4	-17.4	-17.4	-17.4	-17.4	-17.4	-17.4	-17.4

Pages 8, 9 & 10 provide moments, shears, reactions, rotations and deflections for load trial β . Member weight for vertical members is calculated from member length and uniform dead load entered on frame description form. Deflections at quarter points for trial β is provided automatically with provision for additional deflection output when requested on Frame Description form.

IDENT 14T 07 01 FRAME SYSTEM MAY, 01, 1975 PAGE 9

*** SIDESWAY NOT CONSIDERED. ***

VERTICAL MEMBER SHEARS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
5	6.6	6.6	6.6	6.6	6.6	6.6	6.6	6.6	6.6	6.6	6.6

VERTICAL MEMBER REACTIONS TRIAL 0

MEM NO	LT REACTION	RT REACTION	MEMBER WEIGHT
4	232.8	214.8	18.0
5	209.8	191.8	18.0

OUTPUT

Sample Problem I

IDENT 141 07 01 FRAME SYSTEM MAY, 01, 1975 PAGE 10

TRIAL 0

TANGENTIAL ROTATIONS - RADIANS - CLOCKWISE POSITIVE			TANGENTIAL ROTATIONS - RADIANS - CLOCKWISE POSITIVE			TANGENTIAL ROTATIONS - RADIANS - CLOCKWISE POSITIVE		
SPAN	LT. END	RT. END	SPAN	LT. END	RT. END	SPAN	LT. END	RT. END
1	0.002498	0.002422	2	0.002422	-0.000922	3	-0.000922	-0.003580
4	0.000000	0.002422	5	0.000000	-0.000922			

HORIZONTAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END - DOWNWARD POSITIVE

MEMBER	E#	750.	0.0	0.041	0.032	-0.008	0.0
MEMBER 1	E# 750.	0.0	0.041	0.032	-0.008	0.0	
MEMBER 2	E# 750.	0.0	0.040	0.099	0.055	0.0	
	LONG HINGE	LT	1/4	1/2	3/4	RT	
		0.078	0.100	0.088	0.042	0.0	

MEMBER 3	E# 750.	0.0	0.014	0.059	0.059	0.0	
----------	---------	-----	-------	-------	-------	-----	--

VERTICAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END.

MEMBER 4	E# 750.	0.0	-0.003	-0.009	-0.010	0.0	
MEMBER 5	E# 750.	0.0	0.001	0.003	0.004	0.0	

IDENT 141 07 01 FRAME SYSTEM MAY, 01, 1975 PAGE 11

LOAD DATA TRIAL 1

LINE	MEM	W	DIR	P	LOAD CODE	A	B	FIXED END MOMENTS		DEFLT	COMMENTS
								LEFT	RIGHT		
0060	2	32,000		P		20.0	0.0	0.	0.	10	TRUCK LOAD
0050	2	32,000		P		34.0	0.0	0.	0.		1 LANE
0040	2	0,000		P		48.0	0.0	0.	0.		NO IMPACT

FIXED END MOMENTS TRIAL 1

MEM NO	FIXED END MOMENTS		MEM NO	FIXED END MOMENTS		MEM NO	FIXED END MOMENTS	
	LT	RT		LT	RT		LT	RT
1	0.	0.	2	-1175.	-369.	3	0.	0.
4	0.	0.	5	0.	0.			

Page 11 reports the load data for trial 1. Fixed end moments due to the applied loads are also calculated and printed for the load trial.

DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM- LOAD DATA

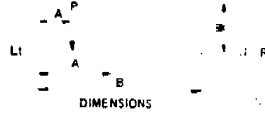
DS-095 (REV. 2-75)

BDE0AA

Page 3 of 4

IDENT * CODE
DIST. CR. BATCH PROB
14T 0703
S/C 7316
L=Max. W on left
R=Max. W on right
U=Uniform Load
P=Point Load

SIGN CONVENTIONS



Phone

Update	Line No.	Trial No.	Member No.	W or P k/ft or k	Loads		FEMs*		Comments
					A	B	Left	Right	
	0 1			14037P	810				DIAPH DIAPH CAP WT.
	0 2			14037P	750				
	0 2			250 OP	∞				

S/C 7316

*When FEMs are given, they are not calculated for any load on that member

DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM- SUPERSTRUCTURE LIVE LOAD

DS-D125 (REV. 2-75)

BDE0AA

Page 4 of 4

IDENT
DIST. CR. BATCH PROB
14T 0703
S/C 7320, 7321

Name Example #3

Phone

MEMBER DATA

Update	Line No.	Member No.	Number of Live Load Lanes				Plot Data				COMMENTS
			Superstructure		Substructure		Resisting Moment		Moment & Shear	Influence Lines	
			Lt. End	Rt. End	Lt.	Rt.	Positive	Negative			
		1	2, 4, 3		1, 0	4, 500	50, 0	1	✓	2 SPAN, EXAMPLE W/ INFL. & P.L.T	

S/C 7320

Frame Description data with the horizontal members numbered consecutively starting with 01 must accompany this data

Member Data - When the Number of L.L. Lanes is given, it must be given for the left end of Superstructure Member 01. (Substructure Member 01 defaults to 1.0 when left blank.) Thereafter, it is assumed to be constant until another entry is made.

Live Load Data - For AASHO HS20-44 loading, leave Truck and Lane data blank for L.L. No. 1. When this data is given, it replaces the HS20-44 loading. An entry for the Number of Live Load Lanes, overrides that given as Member Data. Data entries for L.L. No.'s 2 and 3 produce separate results in addition to L.L. No. 1.

Influence Lines - When checked, a plot of the influence lines will be produced along with the printed results.

LIVE LOAD DATA

Update	Line No.	L.L. No.	Truck - (1 Lane)					Uniform	Moment Rider	Shear Rider	No. Impact	Number of Live Load Lanes	COMMENTS
			P ₁	D ₁	P ₂	D ₂	P ₃						
	1												
	2												
	3												

S/C 7321

IDENT		FRAME SYSTEM										MAY, 02, 1975		PAGE 1	
FRAME DESCRIPTION															
LINE NO.	MEM NO.	JOINT NO.	END COND.	DIR	SPAN	SUPPORT ON	DEAD LOAD	K		CARRY OVER FACTORS		WELL MEM			
		LT	RT			I	UNIFORM	SEC	LT	RT	LT	RT			
0010	1	1	2	M	162.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
0020	2	2	3	M	150.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
0030	3	4	2		26.0	84.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0		

IDENT		FRAME SYSTEM										MAY, 02, 1975		PAGE 2	
SECTION PROPERTIES															
LINE NO.	MEM NO.	LUC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STONE			
						WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB				
0010	1	0.0		0.0	0.0	34.0	6.50	6.75	5.75	2	12.	01			
				LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG					
				TYPE	WEB FACTOR	TYPE	WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.				
				0	12.	0	12.	3.5	7.	11.	3.5	7.	11.		
				CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID									
				X	Y	X=X	Y=Y								
				17.00	3.63	343.63	4987.14								

LINE NO.	MEM NO.	LUC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STONE
						WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB	
0020	1	140.0	01	0.0	0.0	0.0	0.0	0.0	0.0	0	0.	
				LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG		
				TYPE	WEB FACTOR	TYPE	WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.	
				0	0.	0	0.	0.0	0.	0.	0.0	0.
				CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID						
				X	Y	X=X	Y=Y					
				17.00	3.63	343.63	4987.14					

IDENT		FRAME SYSTEM										MAY, 02, 1975		PAGE 3	
SECTION PROPERTIES															
LINE NO.	MEM NO.	LUC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STONE			
						WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB				
0030	1	162.0		0.0	0.0	34.0	6.50	6.75	6.00	2	12.	02			
				LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG					
				TYPE	WEB FACTOR	TYPE	WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.				
				0	12.	0	12.	3.5	7.	11.	3.5	7.	11.		
				CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID									
				X	Y	X=X	Y=Y								
				17.00	3.41	381.06	5224.21								

MEMBER 1 PROPERTIES							
LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER			
		LT	RT	LT	RT		
162.0	343.63	4.021	4.098	0.509	0.499		

```

IDENT 141 07 03                FRAME SYSTEM                MAY. 02, 1975                PAGE 4
SECTION PROPERTIES
LINE MEM  LUC  RECALL          X       Y       SUPERSTRUCTURE      SLAB THICKNESS  INT. GIRDER      STORE
0040  2     0.0  02           0.0   0.0           WIDTH  DEPTH        TOP    BOTTOM    NO.  WEB
                          0.0   0.0           0.0   0.0           0.0   0.0           0    0.
               LT, EXT. GIRDER          RT, EXT. GIRDER          LT. OVERHANG          RT. OVERHANG
               TYPE  WEB  FACTOR      TYPE  WEB  FACTOR      LENGTH EXT. INT.      LENGTH EXT. INT.
LINE        0      0.0  0.0           0      0.0  0.0           0.0    0.    0.    0.0    0.    0.
NUM. MEM    + CODE  V  H  X  Y        AREA  IXX  IYY  STORE
              RECALL 2              17.00  3.41  59.85  381.06  5224.21
              AREA        CENTROID LOCATION          MOMENT OF INERTIA ABOUT CENTROID
                        X  Y              X=X  Y=Y
                59.85      17.00   3.41              381.06       5224.25
    
```

```

LINE MEM  LUC  RECALL          X       Y       SUPERSTRUCTURE      SLAB THICKNESS  INT. GIRDER      STORE
0050  2     22.0  01           0.0   0.0           WIDTH  DEPTH        TOP    BOTTOM    NO.  WEB
                          0.0   0.0           0.0   0.0           0.0   0.0           0    0.
               LT, EXT. GIRDER          RT, EXT. GIRDER          LT. OVERHANG          RT. OVERHANG
               TYPE  WEB  FACTOR      TYPE  WEB  FACTOR      LENGTH EXT. INT.      LENGTH EXT. INT.
LINE        0      0.0  0.0           0      0.0  0.0           0.0    0.    0.    0.0    0.    0.
NUM. MEM    + CODE  V  H  X  Y        AREA  IXX  IYY  STORE
              RECALL 1              17.00  3.63  55.54  343.63  4987.14
              AREA        CENTROID LOCATION          MOMENT OF INERTIA ABOUT CENTROID
                        X  Y              X=X  Y=Y
                55.54      17.00   3.63              343.63       4987.16
    
```

```

IDENT 141 07 03                FRAME SYSTEM                MAY. 02, 1975                PAGE 5
SECTION PROPERTIES
LINE MEM  LUC  RECALL          X       Y       SUPERSTRUCTURE      SLAB THICKNESS  INT. GIRDER      STORE
0060  2     150.0  01          0.0   0.0           WIDTH  DEPTH        TOP    BOTTOM    NO.  WEB
                          0.0   0.0           0.0   0.0           0.0   0.0           0    0.
               LT, EXT. GIRDER          RT, EXT. GIRDER          LT. OVERHANG          RT. OVERHANG
               TYPE  WEB  FACTOR      TYPE  WEB  FACTOR      LENGTH EXT. INT.      LENGTH EXT. INT.
LINE        0      0.0  0.0           0      0.0  0.0           0.0    0.    0.    0.0    0.    0.
NUM. MEM    + CODE  V  H  X  Y        AREA  IXX  IYY  STORE
              RECALL 1              17.00  3.63  55.54  343.63  4987.14
              AREA        CENTROID LOCATION          MOMENT OF INERTIA ABOUT CENTROID
                        X  Y              X=X  Y=Y
                55.54      17.00   3.63              343.63       4987.16
    
```

```

MEMBER 2 PROPERTIES
              LENGTH          MIN INERTIA          STIFFNESS          CARRY OVER
               LT           RT           LT           RT           LT           RT
                150.0          343.63           4.105          4.023           0.499          0.504
    
```

```

IDENT 141 07 03                FRAME SYSTEM                MAY. 02, 1975                PAGE 6
FRAME DIAGNOSTICS
      NO ERRORS FOUND
FRAME PROPERTIES
MEM  JT  JT  ENO  SUPPOR  CARRY OVER  DISTRIBUTION
NU   LT  RT  COND  OR  MINGE  E           FACTORS           FACTORS
                         LT   RT           LT   RT           LT   RT
 1   1   2   R     G     162.0  343.63  0.0   750.  0.504  0.0   0.0  0.254
 2   2   3   R     G     150.0  343.63  0.0   750.  0.0   0.504  0.275  0.0
 3   4   2   R     G     28.0   84.00  0.0   750.  0.500  0.500  0.0  0.471
    
```

OUTPUT

Sample Problem 2

IDENT 141 07 02 FRAME SYSTEM MAY, 02, 1975 PAGE 27
 LL NO. 2. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS

MEMBER	1	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
PUS. V			314.0	265.0	218.4	173.8	132.3	94.8	61.4	34.5	12.1	0.0
MOMENT			0.0	3186.9	5241.7	6255.3	6352.1	5649.6	4450.0	2941.3	1104.2	971.4
NEG. V			-34.1	-34.1	-40.0	-72.8	-117.7	-165.5	-210.9	-253.4	-292.1	-320.4
MOMENT			0.0	-408.7	2795.6	4264.8	5583.4	6072.7	5583.0	4256.5	2200.5	-172.5
RANGE			348.6	299.6	258.5	246.6	250.1	260.3	272.4	287.7	304.2	355.4

LL NO. 2. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS

MEMBER	2	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
PUS. V			352.3	318.7	278.6	234.3	187.4	141.7	97.6	58.0	25.3	25.3
MOMENT			-3202.2	5.4	2411.9	5133.4	6424.9	6680.3	5432.0	4351.3	129.2	533.4
NEG. V			-40.0	-40.0	-40.6	-52.5	-69.8	-132.4	-178.1	-224.7	-270.0	-312.0
MOMENT			1027.6	977.6	327.4	4092.1	5723.8	6624.9	6571.1	5477.2	3346.5	521.1
RANGE			393.0	359.3	319.3	286.8	277.7	274.0	275.7	282.7	295.3	337.2

LL NO. 2. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS

MEMBER	3	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
PUS. V			352.0	314.9	278.5	233.8	187.0	140.5	96.6	57.0	26.5	26.5
MOMENT			-3265.0	380.9	3675.9	6168.0	7574.5	7784.1	6657.0	5024.3	262.1	753.0
NEG. V			-25.0	-25.0	-26.7	-59.3	-98.9	-143.2	-189.9	-236.5	-280.4	-320.7
MOMENT			1147.2	685.2	2753.6	5117.6	6927.5	7800.8	7523.3	6052.4	3516.8	210.4
RANGE			377.6	343.9	305.2	293.1	280.0	283.7	286.5	294.1	307.5	347.3

IDENT 141 07 02 FRAME SYSTEM MAY, 02, 1975 PAGE 28
 LL NO. 2. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS

MEMBER	4	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
PUS. V			357.3	328.6	295.4	257.6	216.3	172.2	125.8	77.9	34.8	35.1
MOMENT			-2840.6	254.0	3114.2	5455.9	7039.4	7607.2	7181.9	5464.4	3240.0	441.1
NEG. V			-6.1	-6.1	-15.7	-39.7	-69.1	-103.4	-141.8	-183.7	-224.3	-275.0
MOMENT			459.7	773.7	1761.6	3888.3	5804.1	7237.6	7942.8	7715.4	6392.5	3849.4
RANGE			363.4	335.0	311.1	297.3	285.4	275.6	267.7	261.6	267.1	310.1

IDENT 141 07 02 FRAME SYSTEM MAY, 02, 1975 PAGE 29
 LL NO. 2. DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE

MEMBER	1	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
PUS. V			465.1	742.3	521.3	302.8	87.6	-123.8	-351.0	-552.5	-748.5	-925.4
NEG. V			616.5	442.0	262.8	56.2	-162.5	-384.1	-623.9	-840.1	-1052.7	-1260.8

LL NO. 2. DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE

MEMBER	2	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
PUS. V			1458.9	1193.4	921.6	645.5	367.4	89.3	-207.0	-474.4	-742.9	-974.6
NEG. V			1065.9	834.1	602.3	358.8	89.6	-184.7	-462.7	-761.1	-1038.2	-1311.9

LL NO. 2. DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE

MEMBER	3	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
PUS. V			1798.8	1374.5	1066.2	753.4	438.7	124.2	-208.2	-515.2	-814.2	-1042.2
NEG. V			1421.2	1030.6	761.0	460.5	152.7	-159.5	-444.7	-804.3	-1121.7	-1429.5

LL NO. 2. DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE

MEMBER	4	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
PUS. V			1762.2	1522.6	1275.0	1014.9	758.1	490.3	142.6	-85.3	-357.4	-597.3
NEG. V			1398.7	1187.7	963.9	722.0	472.6	214.7	-75.1	-346.9	-624.5	-907.4

IDENT 101 07 02
LL NO. 2.

FRAME SYSTEM
LIVE LOAD SUPPORT RESULTS

MAY, 02, 1975

PAGE 30

	MAX. AXIAL LOAD	AXIAL LOAD		MAX. AXIAL LOAD	LONGITUDINAL MOMENT	
		TOP	BOT.		TOP	BOT.
SUPPORT JT. 1						
POSITIVE	314.0	0.	0.	0.0	0.	0.
NEGATIVE	-34.1	0.	0.	0.0	0.	0.
MEMBER 5						
POSITIVE	363.6	-455.	227.	290.3	1765.	-693.
NEGATIVE	-49.6	548.	-274.	289.6	-2076.	1036.
MEMBER 6						
POSITIVE	379.2	-396.	198.	272.8	1702.	-651.
NEGATIVE	-31.8	330.	-165.	280.6	-1985.	982.
MEMBER 7						
POSITIVE	361.3	439.	-219.	277.8	2194.	-1097.
NEGATIVE	-32.7	-384.	192.	282.6	-1892.	946.
SUPPORT JT. 5						
POSITIVE	323.1	0.	0.	0.0	0.	0.
NEGATIVE	-35.1	0.	0.	0.0	0.	0.

THE RATIO OF SUBSTRUCTURE / SUPERSTRUCTURE LOADING IS 1.000

***** MATCH TOTALS 26 FRAME UNITS 12 L.L. UNITS 0 PLOT UNITS 0 PRESTRESS UNITS COST= \$ 6.32

SAMPLE PROBLEM 3

PROBLEM

A. General

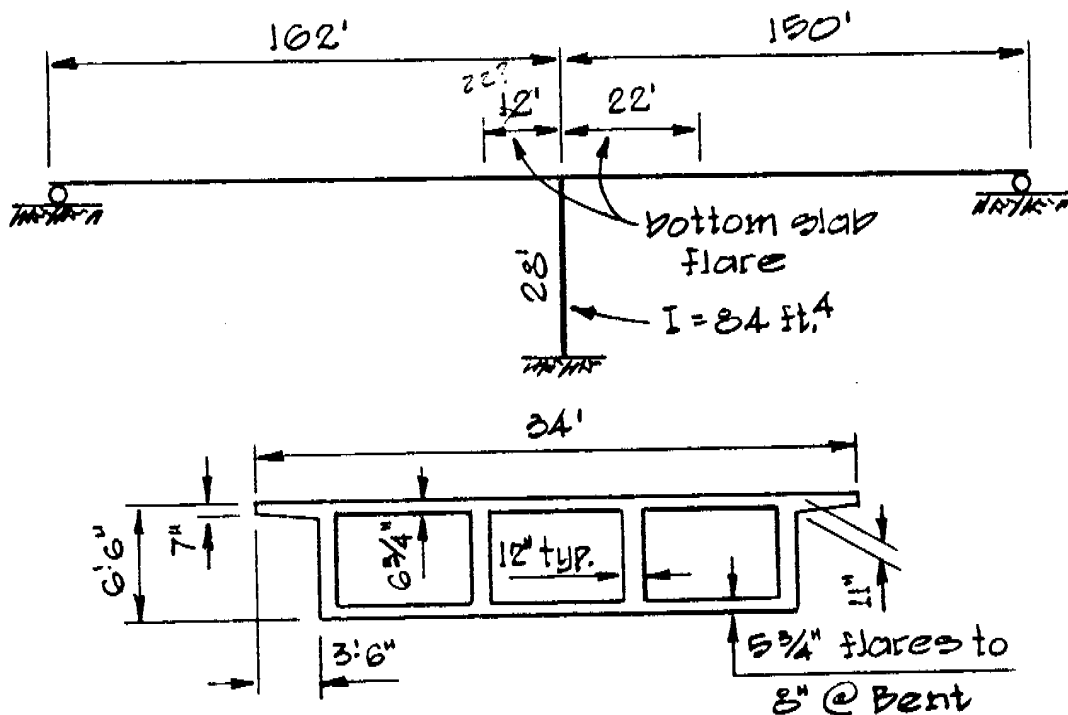
Two-span bridge with no expansion joints. Span properties to be computed by program. Influence lines for moment and shear to be automatically printed and plotted. Moment and shear diagram envelopes to be printed and plotted for AASHTO HS20-44 loading.

B. Section Properties

Column prismatic as coded on Frame Description form. Superstructure cross-section varies with a bottom slab flare near the bent as coded on Superstructure Sections input form. (See fig. 7)

C. Loading

Dead load of diaphragms as coded on Load Data form trial 00. Live load of 2.43 lanes of AASHTO HS20-44 without alternative.



DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - FRAME DESCRIPTION
 DS-D93 (REV 2 75)

BDE0AA

Page 1 of 4

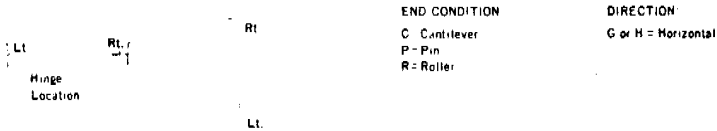
Name Example #3

IDENT		SOURCE		CHARGE		EXPENDITURE AUTHORIZATION		SPECIAL DESIGNATION WHEN APPLICABLE		PROGRAM NUMBER	
DIST.	GR. BATCH	DIST.	UNIT	DIST.	UNIT						
14T	0703	14033	14033	910002						BDE035	
S.C. 2091, 7310		S.C. 2091									

Phone

Update	Line No.	Member No.	End Joint No.		End Condition Direction	Length	Min. I	Hinge Location or Support Width	Dead Load		Member Properties				Recall	DL			
			Lt.	Rt.					Unit	Uniform	-K- Shiftness Factor		-C- Carry Over Factor				Member Reverse	Deflections	S
			ft.	ft.					pcf	k/ft.	Lt.	Rt.	Lt.	Rt.					
	1	1	2R	H	1620					150									
	2	2	3	RH	1500					150									
	3	4	2		280	8400													

S.C. 7310



DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - SUPERSTRUCTURE SECTIONS
 DS D112 (REV 4/75)

BDE0AA

Page 2 of 4

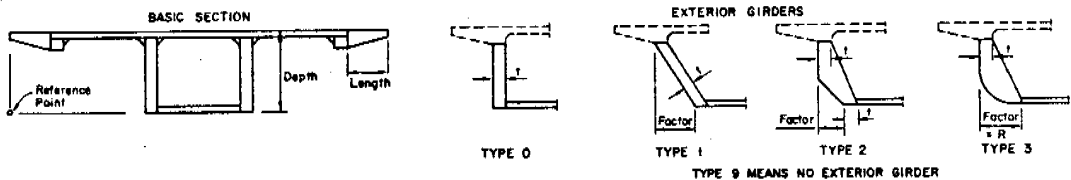
Name Example #3

IDENT		SOURCE		CHARGE		EXPENDITURE AUTHORIZATION		SPECIAL DESIGNATION WHEN APPLICABLE		PROGRAM NUMBER	
DIST.	GROUP BATCH	DIST.	UNIT	DIST.	UNIT						
14T	0703	14033	14033							BDE035	
S.C. 2091, 7311		S.C. 2091									

Phone

UPDATE	LINE NO.	MEMBER NO.	CROSS SECTION LOCATION (FT)	REF. PT. COORD. X (FT)	REF. PT. COORD. Y (FT)	S.S. DAT. WIDTH E.O.-E.O. (FT)	DEPTH (IN.)	STORAGE	EXTERIOR GIRDERS				OVERHANGS				
									LEFT WEB THICK (IN.)	RIGHT WEB THICK (IN.)	LEFT FACTOR (FT)	RIGHT FACTOR (FT)	LEFT LENGTH (FT)	RIGHT LENGTH (FT)	LEFT INT THICK (IN.)	RIGHT INT THICK (IN.)	LEFT EXT THICK (IN.)
			00			340	75	575	2	2012	012		35	711	35	711	01
			4.00.01														
			6.20			340	75	575	2	2012	012		35	711	35	711	02
			2.00.02														
			2.22.01														
			2.1500.01														

S/C 7311



OUTPUT

Sample Problem 1

IDENT 141 07 01

FRAME SYSTEM

MAY, 01, 1975

PAGE 12

*** SIDESWAY NOT CONSIDERED. ***

HORIZONTAL MEMBER MOMENTS TRIAL 1

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-54.	-109.	-163.	-217.	-271.	-326.	-380.	-434.	-488.	-543.
2	-1187.	-593.	0.	273.	555.	242.	166.	39.	-67.	-214.	-340.
3	-156.	-140.	-124.	-109.	-93.	-76.	-62.	-47.	-31.	-16.	0.

WARNING - MEMBER DEPTHS WERE NOT USED FOR ALL MEMBERS SO STRESSES WERE NOT CALC.

VERTICAL MEMBER MOMENTS TRIAL 1

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
4	322.	225.	129.	32.	-64.	-101.	-250.	-354.	-451.	-548.	-604.
5	-92.	-65.	-37.	-9.	18.	46.	74.	102.	129.	157.	185.

HORIZONTAL MEMBER SHEARS TRIAL 1

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	-7.2	-7.2	-7.2	-7.2	-7.2	-7.2	-7.2	-7.2	-7.2	-7.2	-7.2
2	59.3	59.3	59.3	27.3	-4.7	-12.7	-12.7	-12.7	-12.7	-12.7	-12.7
3	2.1	2.1	2.1	2.1	2.1	2.1	2.1	2.1	2.1	2.1	2.1

VERTICAL MEMBER SHEARS TRIAL 1

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
4	-32.2	-32.2	-32.2	-32.2	-32.2	-32.2	-32.2	-32.2	-32.2	-32.2	-32.2

Pages 12, 13 & 14 provide moments, shears, deflections, rotations and reactions for load trial 1. Deflections and rotations at tenth points along the horizontal members were requested on the Load Data form.

IDENT 141 07 01

FRAME SYSTEM

MAY, 01, 1975

PAGE 13

*** SIDESWAY NOT CONSIDERED. ***

VERTICAL MEMBER SHEARS TRIAL 1

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
5	9.2	9.2	9.2	9.2	9.2	9.2	9.2	9.2	9.2	9.2	9.2

VERTICAL MEMBER REACTIONS TRIAL 1

MEM NO	LT REACTION	RT REACTION	MEMBER WEIGHT
4	66.6	66.6	
5	14.7	14.7	

OUTPUT

Sample Problem I

IDENT 141 07 01

FRAME SYSTEM

FAT. 01, 1975

PAGE 14

TRIAL 1

TANGENTIAL ROTATIONS - RADIAN - CLOCKWISE POSITIVE

SPAN	LT. END	RT. END	SPAN	LT. END	RT. END	SPAN	LT. END	RT. END
1	-0.002930	0.004474	2	0.004474	-0.001203	3	-0.001203	0.000840
4	-0.000000	0.004474	5	0.000000	-0.001203			

HORIZONTAL MEMBER DEFLECTIONS IN FEET AT 1/10 POINTS FROM LEFT END - DOWNWARD POSITIVE

MEMBER	E*	750.	0.0	-0.022	-0.042	-0.060	-0.073	-0.081
			-0.081	-0.073	-0.057	-0.031	0.0	
MEMBER 2	E*	750.	0.0	0.051	0.104	0.105	0.097	0.084
			0.068	0.051	0.032	0.015	0.0	
	LONG HINGE	LT	1/4	1/2	3/4	RT		
			0.109	0.097	0.068	0.032	0.0	
MEMBER 3	E*	750.	0.0	-0.009	-0.010	-0.021	-0.023	-0.023
			-0.021	-0.017	-0.012	-0.006	0.0	

VERTICAL MEMBER DEFLECTIONS IN FEET AT 1/10 POINTS FROM LEFT END.

MEMBER	E*	750.	0.0	-0.001	-0.004	-0.008	-0.013	-0.017
			-0.014	-0.020	-0.017	-0.011	0.0	
MEMBER 5	E*	750.	0.0	0.000	0.001	0.002	0.004	0.005
			0.000	0.000	0.005	0.003	0.0	

**** BATCH TOTALS 32 FRAME UNITS 0 L.L. UNITS 0 PILE UNITS 0 PRESTRESS UNITS COST = 0.64

SAMPLE PROBLEM 2

PROBLEM

A. General

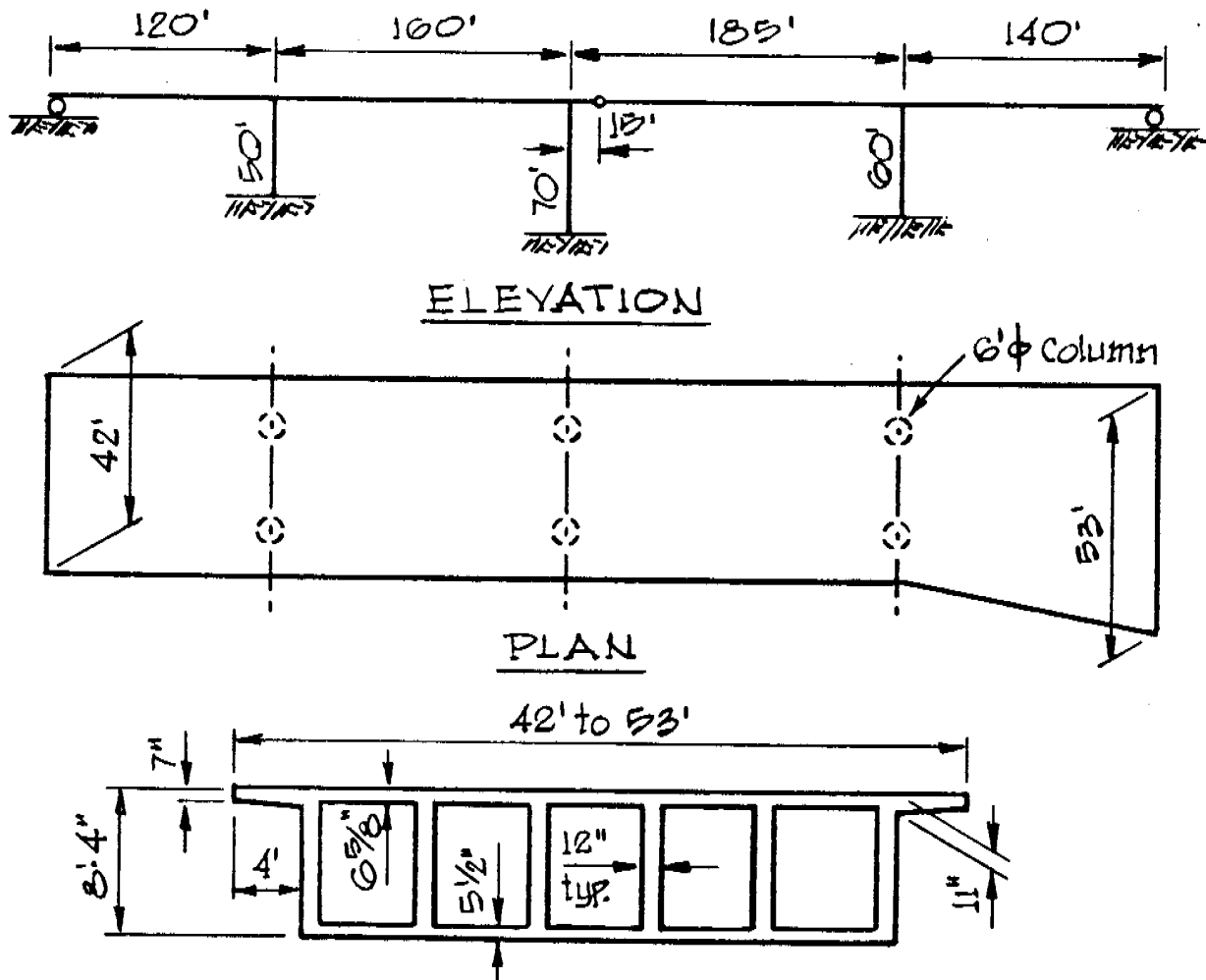
Four-span bridge with one expansion joint. Span properties to be computed by program.

B. Section Properties

Columns prismatic as coded on Frame Description form. Superstructure cross-section varies as per figure 6 and coded on Superstructure Sections input form.

C. Loading

Dead load of diaphragms, AC surfacing, and hinge as coded on Load Data form trial 00. Live loading as coded on Superstructure Live Load form.



DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - FRAME DESCRIPTION
 DS-D93 (REV 2 75)

BDE0AA

Page 1 of 4

IDENT: 14T 0702
 SOURCE: 1403314033910002
 CHARGE: 1403314033910002
 EXPENDITURE AUTHORIZATION: 1403314033910002
 SPECIAL DESIGNATION WHEN APPLICABLE:
 PROGRAM NUMBER: BDE035
 S.C. 2081, 7310

Name Example #2

Phone

Update CODE	Line No.	Member No.	End Joint No.		End Condition	Length	Min. I	Hinge Location or Support Width	Dead Load	Unit	Member Properties		Recall	D.L.
			Lt.	Rt.							Stiffness Factor	Carry Over Factor		
	1	1	2	R	G	1200			360	150				
	2	2	3	G		1600								
	3	3	4	G		1850								
	4	4	5	R	G	1400								
	5	6	2			500	12724							
	6	7	3			700								
	7	8	4			600								

S.C. 7310

END CONDITION:
 C - Cantilever
 P - Pin
 R - Roller

DIRECTION:
 G or H - Horizontal

Merge Location:
 Lt. Rt.

DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - SUPERSTRUCTURE SECTIONS
 DS D112 (REV 4/75)

BDE0AA

Page 2 of 4

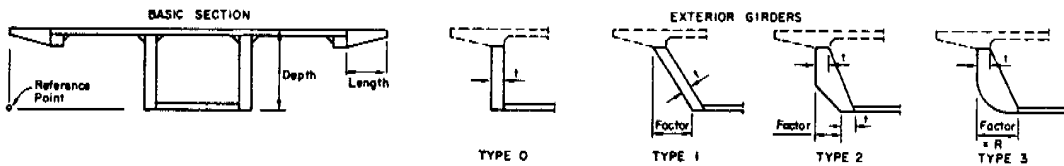
IDENT: 14T 0702
 SOURCE: 1403314033910002
 CHARGE: 1403314033910002
 EXPENDITURE AUTHORIZATION: 1403314033910002
 SPECIAL DESIGNATION WHEN APPLICABLE:
 PROGRAM NUMBER: BDE035
 S.C. 2081, 7311

Name Example #2

Phone

UPDATE CODE	LINE NO.	MEMBER NO.	CROSS SECTION LOCATION (FT)	REF. PT. COORD. X (FT)	REF. PT. COORD. Y (FT)	S.S. DATA WIDTH (FT)	S.S. DATA DEPTH (IN)	INT. GIRDERS (IN)	EXTERIOR GIRDERS			OVERHANGS			STORE
									LEFT	RIGHT	TYPE	LEFT	RIGHT	TYPE	
	01					420	53	550				40	40		01
	02		01												
	03		01												
	04					420	53	550				40	40		
	04	1400				530	53	550				40	40		

S/C 7311



TYPE 9 MEANS NO EXTERIOR GIRDER

DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM- LOAD DATA

DS-D51 (REV. 2-75)

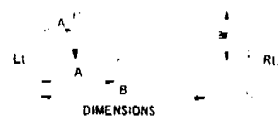
BDE0AA

Page 3 of 4

IDENT
DIST. GR. BATCH PROB.
14T 0702
S/C 7316

* CODE
L - Max. W on left
R - Max. W on right
U - Uniform Load
P - Point Load

SIGN CONVENTIONS



Name Example #1
Phone

Update	Line No.	Trial No.	Member No.	Wor P	Code	A	B	Left	Right	Comments
				k/ft or k		ft	ft	ft-k	ft-k	
	0001			20500P	600					DIAP
	02			P	800					DIAP
	03			P	1000					DIAP
	03			122600P	D150					HINGE
	04			24600P	700					DIAP
	01			1400U						AC SURFACING
	02									
	03									
	04									
	04			0385R						

S/C 7316 *When FEMs are given, they are not calculated for any load on that member.

DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM- SUPERSTRUCTURE LIVE LOAD

DS-D125 (REV. 2-75)

BDE0AA

Page 4 of 4

IDENT
DIST. GR. BATCH PROB.
14T 0702
S/C 7320, 7321

Name Example #2
Phone

Update	Line No.	Member No.	Number of Live Load Lanes		Plot Data		COMMENTS
			Superstructure	Substructure	Resisting Moment of Unit Steel		
			Lt. End	Rt. End	Positive	Negative	
	01	30	0	27			EMPTY CREEK BRIDGE
	04			37.26		30	

S/C 7320

Update	Line No.	L.L. No.	Truck - (1 Lane)					Uniform	Moment Rider	Shear Rider	Number of Live Load Lanes	COMMENTS
			P ₁	D ₁	P ₂	D ₂	P ₃	Kips/ft	Kips	Kips		
	1											
	2		700	130	1300	280	1300					100 CONSTRUCTION LOAD
	3											

S/C 7321

IDENT 141 07 02 FRAME SYSTEM MAY, 02, 1975 PAGE 1

FRAME DESCRIPTION

LINE NO.	MEM NO.	JOINT NO.		END COND	DIR	SPAN	SUPPORT		I	E	DEAD LOAD		K		CARRY OVER FACTORS		RECALL MEM
		LT	RT				OW	HINGE			UNIFORM	SPC	LT	RT	LT	RT	
0010	1	1	2	R	G	120.0	0.0	0.0	0.	0.360	150.	0.0	0.0	0.0	0.0		
0020	2	2	3		G	160.0	0.0	0.0	0.	0.360	150.	0.0	0.0	0.0	0.0		
0030	3	3	4		G	185.0	0.0	0.0	0.	0.360	150.	0.0	0.0	0.0	0.0		
0040	4	4	5	R	G	140.0	0.0	0.0	0.	0.360	150.	0.0	0.0	0.0	0.0		
0050	5	6	2			50.0	127.24	0.0	0.	0.0	0.	0.0	0.0	0.0	0.0		
0060	6	7	3			70.0	127.24	0.0	0.	0.0	0.	0.0	0.0	0.0	0.0		
0070	7	8	4			60.0	127.24	0.0	0.	0.0	0.	0.0	0.0	0.0	0.0		

IDENT 141 07 02 FRAME SYSTEM MAY, 02, 1975 PAGE 2

SECTION PROPERTIES

LINE NO.	MEM NO.	LOL	RECALL	X		Y		SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STONE
				TOP	BOTTOM	NO.	MEM	LT.	RT.	LENGTH	EXT.	INT.	LENGTH	
0010	1	0.0		0.0	0.0	42.0	8.33	6.63	5.50	4	12.		01	
				LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG				
				TYPE	WEB FACTOR	TYPE	WEB FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.	
				0	12.	0	12.	4.0	7.	11.	4.0	7.	11.	

*** SOME OF THE ABOVE DATA HAS BEEN ASSUMED. ***

AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID	
	X	Y	X-X	Y-Y
84.64	21.00	4.57	801.52	1106.41

MEMBER 1 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
		LT	RT	LT	RT
120.0	801.52	4.000	4.000	0.500	0.500

Page 2 reports the member properties of the first horizontal member. Default values are provided by the program for exterior girders with a type β girder 12 inches thick as the assumed data. Left and right deck overhangs are specified as being four feet long with thickness of 7 inches at edge of deck and 11 inches at the edge of the exterior girder. Pages 3 and 4 provide similar data except the properties of the members have been recalled from member 1.

OUTPUT

Sample Problem 2

IDENT 141 07 02 FRAME SYSTEM MAY, 02, 1975 PAGE 3

SECTION PROPERTIES

LINE MEM	LUC	RECALL	X		Y		SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE	
			TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	WIDTH	DEPTH	TOP	BOTTOM		NO.
0020	2	0,0	01	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0		
			LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG					
			TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.
			0	0,	0,0	0	0,	0,0	0,0	0,	0,	0,0	0,	0,
LINE NO. MEM	LUC	RECALL	= CODE		V	H	X	Y	INERTIAS OF PARTS			STORE		
			1						AREA	I _{XX}	I _{YY}			
							21,00	4,57	84,84	801,52	11086,41			
AREA		CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID									
84,84		X Y			X=X Y=Y									
		21,00 4,57			801,52 11086,45									

MEMBER 2 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
		LT	RT	LT	RT
160,0	801,52	4,000	4,000	0,500	0,500

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SECTION PROPERTIES

LINE MEM	LUC	RECALL	X		Y		SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE	
			TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	WIDTH	DEPTH	TOP	BOTTOM		NO.
0030	3	0,0	01	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0			
			LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG					
			TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.
			0	0,	0,0	0	0,	0,0	0,0	0,	0,	0,0	0,	0,
LINE NO. MEM	LUC	RECALL	= CODE		V	H	X	Y	INERTIAS OF PARTS			STORE		
			1						AREA	I _{XX}	I _{YY}			
							21,00	4,57	84,84	801,52	11086,41			
AREA		CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID									
84,84		X Y			X=X Y=Y									
		21,00 4,57			801,52 11086,45									

MEMBER 3 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
		LT	RT	LT	RT
185,0	801,52	4,000	4,000	0,500	0,500

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FRAME SYSTEM

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FRAME DIAGNOSTICS

NO ERRORS FOUND

FRAME PROPERTIES

MEM NO	JT		END COND		DIR	SPAN	I	SUPPORT OR HINGE	E	CARRY OVER FACTORS		DISTRIBUTION FACTORS	
	LI	RT	LI	RT						LT	RT	LI	RT
1	1	2	H		G	120.0	801.52	0.0	750.	0.500	0.0	0.0	0.399
2	2	3			G	160.0	801.52	0.0	750.	0.500	0.500	0.399	0.449
3	3	4			G	185.0	801.52	0.0	750.	0.500	0.500	0.368	0.367
4	4	5		H	G	140.0	841.20	0.0	750.	0.0	0.475	0.424	0.0
5	0	2				50.0	127.24	0.0	750.	0.500	0.500	0.0	0.203
6	7	3				70.0	127.24	0.0	750.	0.500	0.500	0.0	0.163
7	0	4				60.0	127.24	0.0	750.	0.500	0.500	0.0	0.149

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FRAME SYSTEM

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PAGE 8

LOAD DATA TRIAL 0

LINE	MEM	#	DIR	P	LOAD CODE	FIXED END MOMENTS		DEFLT	COMMENTS
						A	B		
0020	1				U	0.0	0.0	0.	AC SURFACING
						ASSUMED DATA 120.0			
0010	1				P	60.0	0.0	0.	DIAP
0040	2				P	80.0	0.0	0.	DIAP
0030	2				U	0.0	0.0	0.	AC SURFACING
						ASSUMED DATA 160.0			
0060	3				P	100.0	0.0	0.	DIAP
0050	3				U	0.0	0.0	0.	AC SURFACING
						ASSUMED DATA 185.0			
0070	3				P	15.0	0.0	0.	HINGE
0100	4				U	0.0	0.0	0.	AC SURFACING
						ASSUMED DATA 140.0			
0090	4				H	0.0	0.0	0.	AC SURFACING
						ASSUMED DATA 140.0			
0080	4				P	70.0	0.0	0.	DIAP

FIXED END MOMENTS TRIAL 0

MEM NO	FIXED END MOMENTS		MEM NO	FIXED END MOMENTS		MEM NO	FIXED END MOMENTS	
	LT	RT		LT	RT		LT	RT
1	0.	-26535.	2	-31312.	-31312.	3	-43301.	-41959.
4	-30650.	0.	5	0.	0.	6	0.	0.
7	0.	0.						

Page 8 reports the load data input and fixed end moment output for Load Data Trial 0. This loading is additive to the uniform loads generated by the program from the uniform dead load and the unit weight specified on the Frame Description form.

SIDESWAY DIAGNOSTICS

NO ERRORS FOUND

RESULTS OF 1 INCH SWAY TO THE RIGHT

VERTICAL MEMBER	SHEAR (KIPS)	MOMENTS (FT-KIPS)		BASED ON E = 3000 KSI
		LT	RT	
5	375.8	-9928.	8863.	
6	152.9	-5437.	5265.	
7	220.3	-6950.	6267.	

Page 9 reports the moments and shears for a one inch movement to the right of the described frame. The output is a result of the entry "S" on the Frame Description form. All succeeding output labeled "Sidesway Included" will include the effects of sidesway in the moments, shears and reactions.

*** SIDESWAY INCLUDED. ***

HORIZONTAL MEMBER MOMENTS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	6763.	11441.	14032.	14538.	12958.	9046.	3047.	-5037.	-15206.	-27462.
2	-27511.	-11661.	481.	6914.	13639.	14656.	11636.	4909.	-5527.	-19671.	-37524.
3	-39344.	-15548.	1502.	13595.	20729.	22906.	19900.	11765.	-1293.	-14326.	-42316.
4	-40982.	-22787.	-7570.	4626.	13757.	19780.	22305.	21633.	17722.	10525.	0.

HORIZONTAL MEMBER STRESSES TRIAL 0 BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-268.	-453.	-556.	-576.	-513.	-356.	-121.	199.	602.	1047.
2	1089.	462.	-19.	-353.	-540.	-580.	-461.	-104.	219.	774.	1485.
3	1560.	615.	-59.	-538.	-821.	-907.	-766.	-466.	51.	765.	1675.
4	1552.	844.	275.	-164.	-479.	-675.	-746.	-710.	-571.	-353.	0.

HORIZONTAL MEMBER STRESSES TRIAL 0 TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	220.	373.	457.	474.	422.	295.	99.	-164.	-445.	-895.
2	-896.	-360.	16.	290.	444.	478.	374.	160.	-180.	-641.	-1223.
3	-1284.	-507.	49.	443.	675.	746.	646.	384.	-42.	-630.	-1374.
4	-1266.	-689.	-224.	134.	391.	551.	609.	580.	466.	272.	0.

OUTPUT

Sample Problem 2

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FRAME SYSTEM

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*** SIDESWAY INCLUDED. ***

VERTICAL MEMBER MOMENTS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
5	-186.	-173.	-159.	-145.	-131.	-118.	-104.	-90.	-77.	-63.	-49.
6	828.	558.	288.	16.	-252.	-521.	-791.	-1061.	-1331.	-1601.	-1870.
7	-814.	-599.	-384.	-169.	46.	260.	475.	690.	905.	1120.	1335.

HORIZONTAL MEMBER SHEARS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	650.5	476.7	302.9	129.0	-44.8	-218.6	-412.9	-586.8	-760.6	-934.4	-1108.2
2	1106.5	674.7	643.0	411.2	179.4	-52.3	-304.6	-536.4	-768.1	-999.4	-1231.7
3	1446.2	1055.6	767.6	519.6	251.7	-16.3	-304.8	-572.6	-840.6	-1108.6	-1376.7
4	1404.9	1193.8	979.6	762.2	541.7	318.1	66.7	-163.2	-396.2	-632.4	-871.7

VERTICAL MEMBER SHEARS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
5	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.7
6	-38.5	-38.5	-38.5	-38.5	-38.5	-38.5	-38.5	-38.5	-38.5	-38.5	-38.5
7	35.8	35.8	35.8	35.8	35.8	35.8	35.8	35.8	35.8	35.8	35.8

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FRAME SYSTEM

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VERTICAL MEMBER REACTIONS TRIAL 0

MEM NO	LT REACTION	RT REACTION	MEMBER WEIGHT
5	2214.8	2214.8	0.0
6	2677.9	2677.9	0.0
7	2781.6	2781.6	0.0

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FRAME SYSTEM

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TRIAL 0

TANGENTIAL ROTATIONS - RADIANS - CLOCKWISE POSITIVE

SPAN	LT. END	RT. END	SPAN	LT. END	RT. END	SPAN	LT. END	RT. END
1	0.005917	0.000428	2	0.000428	0.002656	3	0.002656	-0.001137
4	-0.001137	-0.008783	5	0.000000	0.000428	6	0.000000	0.002656
7	0.000000	-0.001137						

HORIZONTAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END - DOWNWARD POSITIVE

MEMBER	E= 750.	0.0	0.149	0.175	0.076	0.0
MEMBER 1	E= 750.	0.0	0.153	0.246	0.107	0.0
MEMBER 3	E= 750.	0.0	0.373	0.609	0.345	0.0
MEMBER 4	E= 750.	0.0	0.134	0.306	0.260	0.0

VERTICAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END.

MEMBER	E= 750.	0.0	0.001	0.004	0.008	0.013
MEMBER 6	E= 750.	0.0	-0.007	-0.017	-0.015	0.013
MEMBER 7	E= 750.	0.0	0.005	0.015	0.020	0.013

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FRAME SYSTEM

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PAGE 14

LIVE LOAD DIAGNOSTICS

NO ERRORS FOUND

SUPERSTRUCTURE LIVE LOAD EMPTY CREEK BRIDGE

LINE NO.	MEM NO.	NUMBER OF LIVE LOAD LANES				RESISTING MOMENT (K		POSITIVE	NEGATIVE	PLOT ENV.	PLUT M & S SCALE	INFLU- ENCE LINES	P13
		LT,END	RT,END	LT,END	RT,END	UNIT STEEL							
0010	1	3.000	3.000	2.7	2.7	0.	0.	0	0	NO	NO		
	2	3.000	3.000	2.7	2.7	0.	0.						
	3	3.000	3.000	2.7	2.7	0.	0.						
0020	4	3.000	3.720	2.7	3.0	0.	0.						

LIVE LINE NO.	LOAD NO.	-----TRUCK-----					-----LANE-----				IMPACT	NO. LL LNS.	LIVE LOAD SIDESWAY	COMMENTS
		P1	D1	P2	D2	P3	UNIFORM	MUM. RIDER	SHEAR RIDER					
1.		0.0	14.0	32.0	14.0	32.0	0.640	18.0	26.0	YES	0.0	NO	HS20-44 AASHO LOADING WITHOUT ALTERNATIVE CONSTRUCTION LOAD	
0010	2.	70.0	13.0	130.0	28.0	130.0	0.0	0.0	0.0	YES	1.00	NO		

Page 14 reports the input values for standard AASHTO superstructure live load. The standard HS20-44 truck is generated, for live load number 1 when no data is provided for Live Load data. The number of lanes specified as member data is used as the number of live load lanes if no data is supplied for lanes on the Live Load data input. Live Load Data for LL Number 2 is specified such that the specific axle loading will be moved across the superstructure to generate moment and shear envelopes. Maximum results will need to be compared between Live Load number 1 and 2 to obtain absolute maximums.

IDENT 141 07 02

FRAME SYSTEM

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PAGE 15

LL NO. 1.

NEGATIVE LIVE LOAD MOMENT ENVELOPE AND ASSOCIATED SHEARS

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-330.	-661.	-991.	-1321.	-1652.	-1982.	-2312.	-2717.	-4161.	-6540.
SHEAR	0.0	-27.5	-27.5	-27.5	-27.5	-27.5	-27.5	-27.5	-27.5	-164.5	-232.7
2	-7072.	-3703.	-1767.	-1550.	-1835.	-2119.	-2404.	-2688.	-3124.	-4942.	-6331.
SHEAR	245.4	170.2	6.2	-17.6	-17.6	-17.6	-17.6	-17.6	4.1	-102.7	-250.8
3	-8694.	-4536.	-2263.	-1894.	-1893.	-1891.	-1890.	-1888.	-2350.	-4780.	-9049.
SHEAR	264.7	177.8	4.1	0.1	0.1	0.1	0.1	0.1	-11.5	-165.3	-269.4
4	-6085.	-5356.	-3451.	-3001.	-2572.	-2143.	-1715.	-1286.	-857.	-429.	0.
SHEAR	276.9	118.5	-24.1	30.6	30.6	30.6	30.6	30.6	30.6	30.6	0.0

HORIZONTAL MEMBER STRESSES LL MAX NEG BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	13.	26.	39.	52.	65.	78.	92.	104.	166.	261.
2	280.	147.	70.	61.	73.	84.	95.	106.	124.	196.	350.
3	344.	186.	90.	75.	75.	75.	75.	75.	93.	189.	358.
4	329.	198.	125.	107.	90.	73.	57.	42.	26.	14.	0.

HORIZONTAL MEMBER STRESSES LL MAX NEG TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-11.	-22.	-32.	-43.	-54.	-65.	-75.	-84.	-136.	-215.
2	-230.	-121.	-58.	-51.	-60.	-69.	-78.	-86.	-102.	-161.	-271.
3	-283.	-148.	-74.	-62.	-62.	-62.	-62.	-62.	-77.	-156.	-295.
4	-268.	-162.	-102.	-87.	-73.	-60.	-47.	-34.	-23.	-11.	0.

Pages 15 reports the negative live load moment envelope, associated shears, top member stresses, and bottom member stresses. Associated shears are the shears that are produced at the point in question when the envelope moment was produced. Stresses are calculated assuming that section properties do not have composite materials.

OUTPUT

Sample Problem 2

IDENT 141 07 02		FRAME SYSTEM										MAY, 02, 1975		PAGE 16	
LL NO. 1.		DEAD LOAD PLUS NEGATIVE LIVE LOAD MOMENT ENVELOPE													
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT				
1	0.	6433.	10760.	13042.	13217.	11306.	7000.	735.	-7754.	-19387.	-34056.				
2	-34553.	-15364.	-1206.	7364.	11604.	12537.	9233.	2221.	-6651.	-24013.	-45855.				
3	-48088.	-20084.	-761.	11700.	18837.	21015.	18010.	9695.	-3643.	-24105.	-51365.				
4	-44667.	-26143.	-11022.	1626.	11166.	17637.	20590.	20346.	16865.	10097.	0.				
MEM		HORIZONTAL MEMBER STRESSES FOR DL+LL MAX NEG BOTTOM FIBRE													
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT				
1	0.	-255.	-427.	-516.	-523.	-448.	-280.	-29.	307.	768.	1348.				
2	1364.	608.	51.	-292.	-407.	-496.	-360.	-68.	342.	974.	1615.				
3	1904.	795.	30.	-463.	-746.	-832.	-713.	-392.	144.	954.	2033.				
4	1861.	1043.	400.	-58.	-389.	-602.	-689.	-668.	-543.	-319.	0.				
MEM		HORIZONTAL MEMBER STRESSES FOR DL+LL MAX NEG TOP FIBRE													
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT				
1	0.	210.	351.	425.	431.	368.	230.	24.	-253.	-632.	-1110.				
2	-1127.	-501.	-42.	240.	385.	408.	301.	72.	-282.	-802.	-1494.				
3	-1567.	-654.	-25.	361.	614.	665.	567.	322.	-119.	-765.	-1674.				
4	-1534.	-851.	-326.	47.	316.	491.	562.	545.	443.	261.	0.				

Pages 16 through 21 have similar output with page headings describing reported values. Shear results report only one value per tenth point so that abrupt changes at the tenth points will not be printed.

IDENT 141 07 02		FRAME SYSTEM										MAY, 02, 1975		PAGE 17	
LL NO. 1.		POSITIVE LIVE LOAD MOMENT ENVELOPE AND ASSOCIATED SHEARS													
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT				
1	0.	2413.	4052.	4984.	5341.	5182.	4563.	3498.	2122.	1170.	920.				
SHEAR	0.0	161.0	152.0	101.4	74.8	-106.1	+130.8	-153.2	-173.0	-84.4	6.2				
2	1393.	1514.	2664.	4191.	5200.	5556.	5326.	4430.	2953.	1467.	1145.				
SHEAR	-27.9	63.0	158.2	133.3	106.2	78.2	-105.6	-132.9	-156.2	-82.9	16.0				
3	1258.	1505.	3200.	4908.	6252.	6666.	6117.	4629.	3165.	1215.	964.				
SHEAR	-16.0	78.4	155.9	130.6	76.6	-34.9	-84.0	-136.4	-160.6	-77.9	16.0				
4	666.	1133.	2851.	4657.	6123.	7052.	7291.	6906.	5665.	3421.	0.				
SHEAR	-3.7	97.6	171.7	176.5	130.1	105.2	-66.7	-116.2	-173.7	-206.6	0.0				
MEM		HORIZONTAL MEMBER STRESSES LL MAX POS BOTTOM FIBRE													
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT				
1	0.	-96.	-160.	-197.	-211.	-205.	-181.	-138.	-84.	-46.	-37.				
2	-55.	-52.	-105.	-166.	-206.	-220.	-211.	-175.	-117.	-58.	-45.				
3	-50.	-60.	-127.	-194.	-247.	-264.	-242.	-191.	-123.	-48.	-36.				
4	-25.	-42.	-103.	-165.	-213.	-241.	-244.	-227.	-162.	-106.	0.				
MEM		HORIZONTAL MEMBER STRESSES LL MAX POS TOP FIBRE													
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT				
1	0.	79.	132.	162.	174.	164.	144.	114.	64.	34.	30.				
2	45.	43.	87.	137.	164.	181.	174.	160.	96.	46.	37.				
3	41.	49.	104.	160.	204.	217.	194.	157.	101.	40.	31.				
4	21.	34.	84.	135.	174.	196.	194.	185.	144.	68.	0.				

OUTPUT

Sample Problem 2

IDENT 14T 07 02		FRAME SYSTEM										MAY, 02, 1975		PAGE 20
LL NO. 1,		LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS												
MEMBER	4	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
PUS. V			314.4	279.8	245.0	210.4	161.1	153.4	122.4	88.4	62.2	41.4	33.3	
MOMENT			-6620.4	-2789.1	453.4	2656.0	6086.8	6434.0	7026.0	6192.9	3232.7	1691.8	1200.7	
NEG. V			-5.2	-9.5	-20.6	-40.8	-65.4	-94.2	-126.9	-163.0	-202.3	-244.3	-268.6	
MOMENT			732.2	1197.0	2306.1	3494.1	5493.4	6594.9	7105.0	6847.4	5664.8	3420.5	0.0	
RANGE			314.3	289.3	265.6	251.2	246.5	247.6	249.3	251.4	264.5	285.7	321.9	

IDENT 14T 07 02		FRAME SYSTEM										MAY, 02, 1975		PAGE 21
LL NO. 1,		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE												
MEMBER	1	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
PUS. V			864.7	677.6	471.7	266.9	63.6	-137.1	-355.9	-551.1	-740.6	-922.4	-1099.9	
NEG. V			620.4	441.2	250.1	55.6	-150.0	-354.1	-576.8	-776.6	-973.6	-1177.1	-1382.7	

LL NO. 1,		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE											
MEMBER	2	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
PUS. V			1396.7	1126.2	854.3	584.6	322.6	59.8	-222.9	-481.4	-730.9	-975.4	-1208.4
NEG. V			1066.6	835.8	596.9	346.6	95.2	-163.1	-446.4	-713.2	-983.2	-1255.4	-1528.6

LL NO. 1,		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE											
MEMBER	3	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
PUS. V			1757.4	1521.5	1008.6	698.2	391.6	42.5	-226.3	-520.0	-805.8	-1085.0	-1354.1
NEG. V			1421.3	1029.5	750.0	463.8	171.5	-127.0	-448.6	-755.6	-1066.1	-1378.4	-1642.6

LL NO. 1,		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE											
MEMBER	4	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
PUS. V			1714.0	1473.6	1224.6	972.7	722.8	471.5	189.1	-74.8	-334.0	-591.0	-838.4
NEG. V			1399.7	1164.3	959.0	721.5	476.3	223.9	60.1	-326.2	-598.5	-876.7	-1160.4

IDENT 14T 07 02		FRAME SYSTEM						MAY, 02, 1975		PAGE 22
LL NO. 1,		LIVE LOAD SUPPORT RESULTS								
		MAX. AXIAL LOAD			MAX. LONGITUDINAL MOMENT					
		AXIAL LOAD	-----MOMENT----- TOP	BOT.	AXIAL LOAD	-----MOMENT----- TOP	BOT.			
SUPPORT	JT. 1									
	POSITIVE	210.7	0.	0.	0.0	0.	0.			
	NEGATIVE	-27.1	0.	0.	0.0	0.	0.			
MEMBER	5									
	POSITIVE	427.2	-389.	194.	164.3	1420.	-710.			
	NEGATIVE	-41.6	460.	-230.	230.0	-1507.	754.			
MEMBER	6									
	POSITIVE	466.3	-290.	145.	195.4	1363.	-682.			
	NEGATIVE	-37.9	122.	-61.	237.7	-1646.	623.			
MEMBER	7									
	POSITIVE	477.2	376.	-180.	251.6	1724.	-662.			
	NEGATIVE	-25.0	-294.	147.	211.8	-1530.	765.			
SUPPORT	JT. 5									
	POSITIVE	233.7	0.	0.	0.0	0.	0.			
	NEGATIVE	-29.9	0.	0.	0.0	0.	0.			

Page 22 reports the live load support results for live load number 1. Maximum axial loads and moments are produced for maximum axial load and maximum longitudinal moment.

OUTPUT

Sample Problem 3

IDENT 14T 07 03		FRAME SYSTEM		MAY, 02, 1975		PAGE 7		
LOAD DATA TRIAL 0								
LINE	MEM	W OR P	LOAD CODE	A	B	FIXED END MOMENTS LEFT	RIGHT DEFLT	COMMENTS
0010	1	14.037	P	01.0	0.0	0.	0.	DIAPH
0030	2	25.000	P	0.0	0.0	0.	0.	CAP WT.
0020	2	14.037	P	75.0	0.0	0.	0.	DIAPH

FIXED END MOMENTS TRIAL 0								
MEM NO	FIXED END MOMENTS LT	RT	MEM NO	FIXED END MOMENTS LT	RT	MEM NO	FIXED END MOMENTS LT	RT
1	0.	-28246.	2	-24273.	0.	3	0.	0.

IDENT 14T 07 03		FRAME SYSTEM		MAY, 02, 1975		PAGE 8	
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*** SIDESWAY NOT CONSIDERED. ***

HORIZONTAL MEMBER MOMENTS TRIAL 0											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	7234.	12282.	15144.	15819.	14308.	10383.	4271.	-4026.	-14512.	-27235.
2	-25366.	-14243.	-5044.	2279.	7727.	11301.	12790.	12404.	10143.	6009.	0.

HORIZONTAL MEMBER STRESSES TRIAL 0 BOTTOM FIBRE											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-531.	-901.	-1111.	-1161.	-1050.	-762.	-313.	295.	1019.	1693.
2	1577.	991.	370.	-167.	-567.	-829.	-936.	-910.	-744.	-441.	0.

HORIZONTAL MEMBER STRESSES TRIAL 0 TOP FIBRE											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	419.	712.	878.	917.	830.	602.	245.	-233.	-835.	-1533.
2	-1426.	-818.	-292.	132.	448.	655.	742.	719.	588.	348.	0.

VERTICAL MEMBER MOMENTS TRIAL 0											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
3	-935.	-654.	-374.	-93.	187.	467.	748.	1028.	1309.	1569.	1869.

HORIZONTAL MEMBER SHEARS TRIAL 0											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	514.1	379.1	244.1	109.2	-25.6	-160.8	-309.8	-444.7	-579.7	-715.2	-856.8

IDENT 14T 07 03		FRAME SYSTEM		MAY, 02, 1975		PAGE 9	
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*** SIDESWAY NOT CONSIDERED. ***

HORIZONTAL MEMBER SHEARS TRIAL 0											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
2	832.7	676.4	550.7	425.7	300.7	175.8	36.8	-88.2	-213.2	-338.1	-463.1

VERTICAL MEMBER SHEARS TRIAL 0											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
3	100.1	100.1	100.1	100.1	100.1	100.1	100.1	100.1	100.1	100.1	100.1

VERTICAL MEMBER REACTIONS TRIAL 0			
MEM NO	LT REACTION	RT REACTION	MEMBER WEIGHT
3	1689.5	1689.5	0.0

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TRIAL 0

TANGENTIAL ROTATIONS = RADIAN = CLOCKWISE POSITIVE

SPAN	LT. END	RT. END	SPAN	LT. END	RT. END	SPAN	LT. END	RT. END
1	0.020637	-0.001442	2	-0.001443	-0.015073	3	0.000000	-0.001442

HORIZONTAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END = DOWNWARD POSITIVE

MEMBER	E=	750.	0.0	0.708	0.847	0.409	0.0
MEMBER 1							
MEMBER 2				0.236	0.549	0.474	0.0

VERTICAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END.

MEMBER	E=	750.	0.0	0.002	0.005	0.000	0.0
MEMBER 3							

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LIVE LOAD DIAGNOSTICS

NO ERRORS FOUND

SUPERSTRUCTURE LIVE LOAD 2 SPAN EXAMPLE W/INFL&PLT

LINE NO.	MEM NO.	NUMBER OF LIVE LOAD LANES				RESISTING MOMENT OF UNIT STEEL		PLOT M & S ENV.	PLOT SCALE	INFLU- ENCE LINES	FIS		
		LT. END	RT. END	LT. END	RT. END	POSITIVE	NEGATIVE						
0010	1	2.430	2.430	1.0	1.0	4500.	5000.	1	0	YES	NO		
	2	2.430	2.430	1.0	1.0	4500.	5000.						
LIVE LINE NO.	LOAD NO.	TRUCK					LANE			NO. LIVE LL LNS.	LIVE LOAD SIDESWAY	COMMENT	
		P1	D1	P2	D2	P3	UNIFORM	MUM. RIDER	SHEAR RIDER				IMPACT
1.		14.0	14.0	32.0	14.0	32.0	0.640	18.0	26.0	YES	0.0	NO	MS20-44 AASHO LOADING WITHOUT ALTERNATIVE

Page 11 reports the input values for Superstructure Live Load input data. In this example influence lines have been requested as well as a moment and shear plot for live load number 1.

INFLUENCE LINES FOR GIRDER MOMENT

AT 0.1 L - MEMBER 1											
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
NU											
1	0.0	13.972	11.780	9.663	7.650	5.797	4.123	2.670	1.476	0.577	0.0
2	0.0	-0.329	-0.558	-0.692	-0.745	-0.728	-0.653	-0.530	-0.373	-0.192	0.0

AT 0.2 L - MEMBER 1											
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
NU											
1	0.0	11.743	23.560	19.325	15.312	11.594	8.245	5.340	2.952	1.154	0.0
2	0.0	-0.659	-1.115	-1.385	-1.490	-1.456	-1.305	-1.061	-0.746	-0.585	0.0

AT 0.3 L - MEMBER 1											
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
NU											
1	0.0	9.515	19.141	28.988	22.968	17.391	12.368	8.010	4.426	1.731	0.0
2	0.0	-0.988	-1.673	-2.077	-2.236	-2.164	-1.958	-1.591	-1.119	-0.577	0.0

AT 0.4 L - MEMBER 1											
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
NU											
1	0.0	7.287	14.721	22.451	30.624	23.188	16.491	10.660	5.903	2.308	0.0
2	0.0	-1.318	-2.230	-2.769	-2.981	-2.912	-2.610	-2.121	-1.492	-0.769	0.0

AT 0.5 L - MEMBER 1											
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
NU											
1	0.0	5.058	10.301	15.913	22.080	28.985	20.613	13.350	7.379	2.885	0.0
2	0.0	-1.647	-2.788	-3.461	-3.726	-3.641	-3.263	-2.652	-1.865	-0.962	0.0

Pages 12 through 17 provide the influence lines for moment, shears, and reactions. Plotted results for influence lines and Live load moment and shear envelopes are shown at the end of the output for this sample problem.

INFLUENCE LINES FOR GIRDER MOMENT

AT 0.6 L - MEMBER 1											
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
NU											
1	0.0	2.830	5.881	9.376	13.536	18.582	24.736	18.020	8.855	3.462	0.0
2	0.0	-1.977	-3.345	-4.154	-4.471	-4.369	-3.916	-3.182	-2.238	-1.154	0.0

AT 0.7 L - MEMBER 1											
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
NU											
1	0.0	0.802	1.462	2.839	4.492	8.179	12.654	18.690	10.331	4.039	0.0
2	0.0	-2.306	-3.903	-4.846	-5.217	-5.097	-4.568	-3.712	-2.611	-1.346	0.0

AT 0.8 L - MEMBER 1											
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
NU											
1	0.0	-1.627	-2.958	-3.698	-3.552	-2.224	0.581	5.160	11.807	4.616	0.0
2	0.0	-2.836	-4.460	-5.538	-5.962	-5.825	-5.221	-4.243	-2.984	-1.539	0.0

AT 0.9 L - MEMBER 1											
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
NU											
1	0.0	-3.855	-7.378	-10.236	-12.096	-12.627	-11.496	-8.370	-2.917	5.143	0.0
2	0.0	-2.965	-5.018	-6.230	-6.707	-6.553	-5.873	-4.773	-3.357	-1.731	0.0

AT 1.0 L - MEMBER 1											
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
NU											
1	0.0	-6.063	-11.798	-16.773	-20.640	-23.030	-23.573	-21.900	-17.641	-10.430	0.0
2	0.0	-3.294	-5.575	-6.923	-7.452	-7.281	-6.526	-5.303	-3.730	-1.924	0.0

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INFLUENCE LINES FOR GIRDER MOMENT													
AT 0.0 L - MEMBER 2													
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.0	-2.244	-4.352	-6.188	-7.614	-8.496	-8.696	-8.079	-6.506	-3.848	0.0		
2	0.0	-9.390	-15.690	-19.731	-21.240	-20.752	-18.680	-15.115	-10.632	-5.462	0.0		
AT 0.1 L - MEMBER 2													
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.0	-2.020	-3.917	-5.569	-6.853	-7.646	-7.827	-7.271	-5.857	-3.463	0.0		
2	0.0	5.049	-2.301	-7.258	-10.116	-11.177	-10.740	-9.104	-6.569	-3.434	0.0		
AT 0.2 L - MEMBER 2													
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.0	-1.745	-3.482	-4.950	-6.092	-6.797	-6.957	-6.463	-5.206	-3.078	0.0		
2	0.0	4.488	11.288	5.216	1.008	-1.602	-2.880	-3.092	-2.505	-1.366	0.0		
AT 0.3 L - MEMBER 2													
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.0	-1.571	-3.047	-4.331	-5.330	-5.947	-6.087	-5.655	-4.556	-2.643	0.0		
2	0.0	3.927	9.877	17.689	12.132	7.973	4.980	2.919	1.556	0.662	0.0		
AT 0.4 L - MEMBER 2													
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.0	-1.347	-2.811	-3.715	-4.569	-5.098	-5.218	-4.847	-3.905	-2.509	0.0		
2	0.0	3.366	8.406	15.162	23.256	17.549	12.840	8.931	5.621	2.711	0.0		

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INFLUENCE LINES FOR GIRDER MOMENT													
AT 0.5 L - MEMBER 2													
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.0	-1.122	-2.176	-3.094	-3.807	-4.248	-4.348	-4.040	-3.254	-1.924	0.0		
2	0.0	2.805	7.055	12.635	19.380	27.124	20.700	14.942	9.684	4.759	0.0		
AT 0.6 L - MEMBER 2													
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.0	-0.898	-1.741	-2.475	-3.046	-3.398	-3.479	-3.232	-2.603	-1.539	0.0		
2	0.0	2.244	5.644	10.108	15.504	21.699	28.560	20.954	13.747	6.807	0.0		
AT 0.7 L - MEMBER 2													
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.0	-0.673	-1.306	-1.856	-2.284	-2.549	-2.609	-2.424	-1.952	-1.154	0.0		
2	0.0	1.683	4.233	7.581	11.628	16.274	21.420	26.965	17.810	8.855	0.0		
AT 0.8 L - MEMBER 2													
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.0	-0.449	-0.870	-1.238	-1.523	-1.699	-1.739	-1.616	-1.302	-0.770	0.0		
2	0.0	1.122	2.822	5.054	7.752	10.849	14.280	17.977	21.674	10.904	0.0		
AT 0.9 L - MEMBER 2													
MEM	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.0	-0.224	-0.435	-0.619	-0.761	-0.850	-0.870	-0.808	-0.651	-0.385	0.0		
2	0.0	0.561	1.411	2.527	3.876	5.425	7.140	8.988	10.937	12.952	0.0		

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INFLUENCE LINES FOR GIRDER SHEAR

AT LEFT END = MEMBER 1

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	1.000	0.862	0.727	0.596	0.473	0.358	0.254	0.165	0.091	0.036	0.0
2	0.0	-0.020	-0.034	-0.043	-0.046	-0.045	-0.040	-0.033	-0.023	-0.012	0.0

AT LEFT END = MEMBER 2

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.0	0.015	0.029	0.041	0.051	0.057	0.056	0.054	0.043	0.026	0.0
2	1.000	0.963	0.906	0.832	0.742	0.638	0.524	0.401	0.271	0.137	0.0

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INFLUENCE LINES

REACTION AT LT END MEMBER 1

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	1.000	0.862	0.727	0.596	0.473	0.358	0.254	0.165	0.091	0.036	0.0
2	0.0	-0.020	-0.034	-0.043	-0.046	-0.045	-0.040	-0.033	-0.023	-0.012	0.0

REACTION AT TOP OF COLUMN 3

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.0	0.153	0.302	0.445	0.576	0.699	0.803	0.889	0.952	0.990	1.000
2	1.000	0.983	0.940	0.874	0.788	0.683	0.564	0.434	0.294	0.146	0.0

MOMENT AT TOP OF COLUMN 3

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.0	3.859	7.445	10.585	13.026	14.534	14.877	13.821	11.133	6.562	0.0
2	0.0	-6.095	-10.315	-12.806	-13.786	-13.471	-12.074	-9.812	-6.901	-3.559	0.0

REACTION AT RT END MEMBER 2

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.0	-0.015	-0.029	-0.041	-0.051	-0.057	-0.056	-0.054	-0.043	-0.026	0.0
2	0.0	0.037	0.094	0.168	0.256	0.362	0.476	0.599	0.729	0.863	1.000

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LL NO. 1. NEGATIVE LIVE LOAD MOMENT ENVELOPE AND ASSOCIATED SHEARS

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-172.	-344.	-517.	-689.	-861.	-1033.	-1205.	-1989.	-4240.	-7471.
SHEAR	0.0	-10.0	-10.0	-10.0	-10.0	-10.0	-10.0	-10.0	-45.5	-172.5	-224.0
2	-7024.	-4161.	-2174.	-1484.	-1272.	-1060.	-846.	-630.	-424.	-212.	0.
SHEAR	215.7	165.4	40.1	14.1	14.1	14.1	14.1	14.1	14.1	14.1	0.0

HORIZONTAL MEMBER STRESSES LL MAX NEG BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	13.	25.	30.	51.	63.	76.	68.	146.	298.	460.
2	437.	289.	160.	109.	93.	78.	62.	47.	31.	16.	0.

HORIZONTAL MEMBER STRESSES LL MAX NEG TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-10.	-20.	-30.	-40.	-50.	-60.	-70.	-115.	-244.	-421.
2	-396.	-239.	-126.	-86.	-74.	-61.	-49.	-37.	-25.	-12.	0.

IDENT 141 07 03		FRAME SYSTEM									MAY, 02, 1975		PAGE 19
LL NO. 1.		DEAD LOAD PLUS NEGATIVE LIVE LOAD MOMENT ENVELOPE											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.	7062.	11938.	14627.	15130.	13447.	9350.	3066.	-6016.	-18751.	-54706.		
2	-32395.	-18404.	-7217.	795.	6455.	10241.	11941.	11766.	9719.	5797.	0.		
MEM NO		LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
HORIZONTAL MEMBER STRESSES FOR DL+LL MAX NEG BOTTOM FIBRE													
1	0.	-518.	-876.	-1073.	-1110.	-987.	-686.	-225.	441.	1316.	2157.		
2	2013.	1280.	530.	-58.	-474.	-751.	-876.	-863.	-713.	-425.	0.		
MEM NO		LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
HORIZONTAL MEMBER STRESSES FOR DL+LL MAX NEG TOP FIBRE													
1	0.	409.	692.	848.	877.	780.	542.	178.	-349.	-1078.	-1954.		
2	-1824.	-1057.	-418.	46.	374.	594.	692.	682.	564.	536.	0.		

IDENT 141 07 03		FRAME SYSTEM									MAY, 02, 1975		PAGE 20
LL NO. 1.		POSITIVE LIVE LOAD MOMENT ENVELOPE AND ASSOCIATED SHEARS											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.	2612.	4341.	5284.	5539.	5239.	4416.	3186.	1745.	478.	0.		
SHEAR	0.0	161.2	134.0	92.5	67.6	-102.2	-124.0	-143.2	-159.3	-104.7	0.0		
2	0.	445.	1601.	3008.	4142.	4889.	5152.	4903.	4025.	2420.	0.		
SHEAR	0.0	109.2	159.2	142.9	123.5	101.5	-68.3	-93.1	-134.2	-161.3	0.0		
MEM NO		LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
HORIZONTAL MEMBER STRESSES LL MAX POS BOTTOM FIBRE													
1	0.	-192.	-319.	-384.	-406.	-384.	-324.	-234.	-126.	-34.	0.		
2	0.	-31.	-122.	-221.	-304.	-359.	-376.	-360.	-295.	-176.	0.		
MEM NO		LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
HORIZONTAL MEMBER STRESSES LL MAX POS TOP FIBRE													
1	0.	151.	252.	306.	321.	304.	256.	185.	101.	27.	0.		
2	0.	26.	96.	174.	240.	283.	299.	284.	233.	140.	0.		

IDENT 141 07 03		FRAME SYSTEM									MAY, 02, 1975		PAGE 21
LL NO. 1.		DEAD LOAD PLUS POSITIVE LIVE LOAD MOMENT ENVELOPE											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.	9046.	16623.	20428.	21358.	19547.	14799.	7454.	-2262.	-14034.	-27235.		
2	-25366.	-13798.	-3363.	5287.	11869.	16190.	17942.	17306.	14166.	8429.	0.		
MEM NO		LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
HORIZONTAL MEMBER STRESSES FOR DL+LL MAX POS BOTTOM FIBRE													
1	0.	-722.	-1220.	-1499.	-1567.	-1434.	-1086.	-547.	167.	965.	1693.		
2	1577.	960.	248.	-368.	-671.	-1186.	-1316.	-1270.	-1040.	-616.	0.		
MEM NO		LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
HORIZONTAL MEMBER STRESSES FOR DL+LL MAX POS TOP FIBRE													
1	0.	571.	964.	1184.	1236.	1153.	858.	433.	-132.	-807.	-1553.		
2	-1426.	-792.	-196.	307.	688.	939.	1040.	1003.	622.	489.	0.		

OUTPUT

Sample Problem 3

IDENT 141 07 03 FRAME SYSTEM MAY, 02, 1975 PAGE 22
 LL NO. 1. LIVE LOAD ENVELOPES AND ASSOCIATED MOMENTS

MEMBER	1	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
PUS. V			194.1	161.2	134.0	108.0	83.0	61.4	41.8	23.5	12.3	3.2	0.0
MOMENT			0.0	2611.7	4341.1	5246.9	5414.0	4974.0	4064.3	2864.2	1547.4	467.7	0.0
NEG. V			-11.7	-20.5	-40.0	-67.4	-93.6	-118.3	-140.8	-163.4	-194.7	-226.6	-254.4
MOMENT			556.5	1560.6	3442.2	4741.7	5327.9	5143.4	4363.3	3245.5	1020.5	-2041.0	-5674.6
RANGE			205.8	161.7	174.0	175.4	177.2	174.7	162.0	144.7	207.1	224.8	254.4

LL NO. 1. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS

MEMBER	2	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
PUS. V			249.1	219.2	189.2	160.2	139.4	117.1	92.4	66.1	38.4	23.2	15.6
MOMENT			-5484.1	-2060.1	681.6	2965.0	4090.4	4742.6	4933.2	4401.0	2644.1	1367.5	645.2
NEG. V			0.0	-3.3	-12.5	-25.5	-42.1	-61.7	-83.9	-108.2	-134.2	-161.3	-189.2
MOMENT			0.0	440.5	1496.4	2682.5	3789.6	4626.2	5033.4	4868.7	4024.7	2419.9	0.0
RANGE			249.1	222.4	201.6	185.7	182.0	176.6	176.3	174.3	173.1	164.0	204.7

IDENT 141 07 03 FRAME SYSTEM MAY, 02, 1975 PAGE 23
 LL NO. 1. DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE

MEMBER	1	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
PUS. V			708.1	549.3	378.1	217.1	57.8	-99.4	-268.0	-419.4	-567.4	-712.0	-856.8
NEG. V			502.4	359.6	204.1	41.8	-119.4	-279.0	-450.6	-606.2	-774.4	-941.6	-1115.2

LL NO. 1. DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE

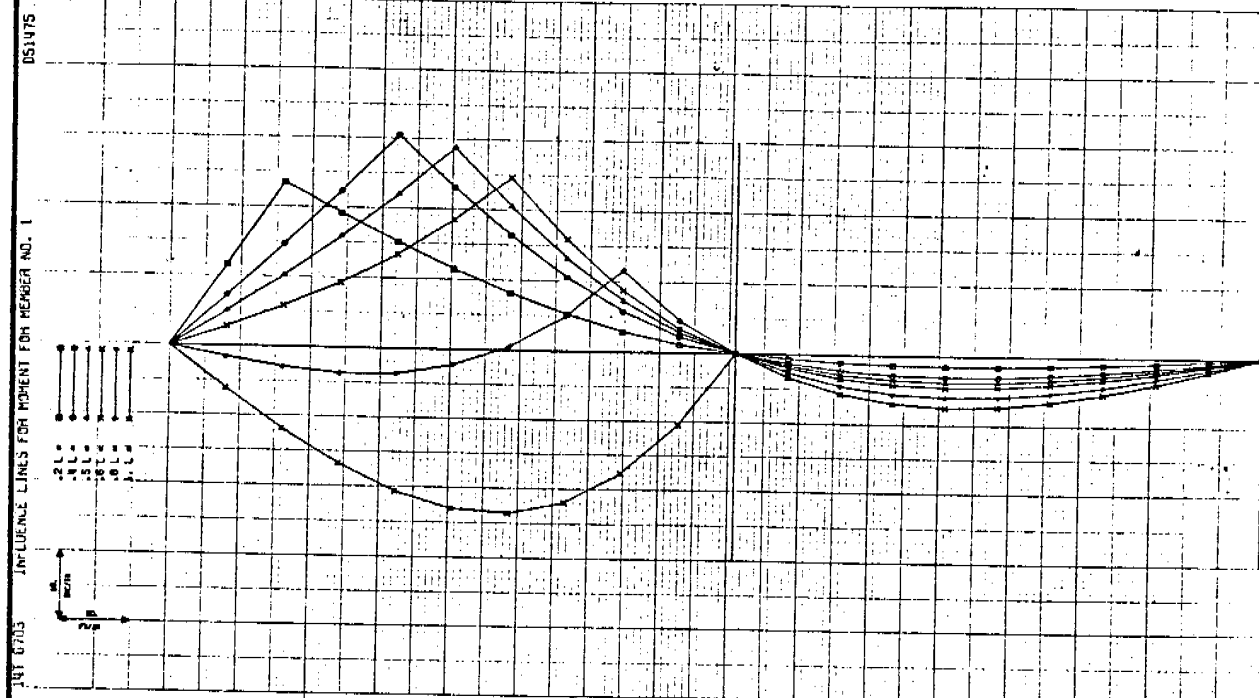
MEMBER	2	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
PUS. V			1061.6	895.6	739.8	585.4	440.6	292.4	149.1	-22.1	-174.3	-314.4	-447.6
NEG. V			432.7	673.1	536.2	400.1	258.6	114.1	-47.1	-196.4	-347.3	-494.5	-652.3

IDENT 141 07 03 FRAME SYSTEM MAY, 02, 1975 PAGE 24
 LL NO. 1. LIVE LOAD SUPPORT RESULTS

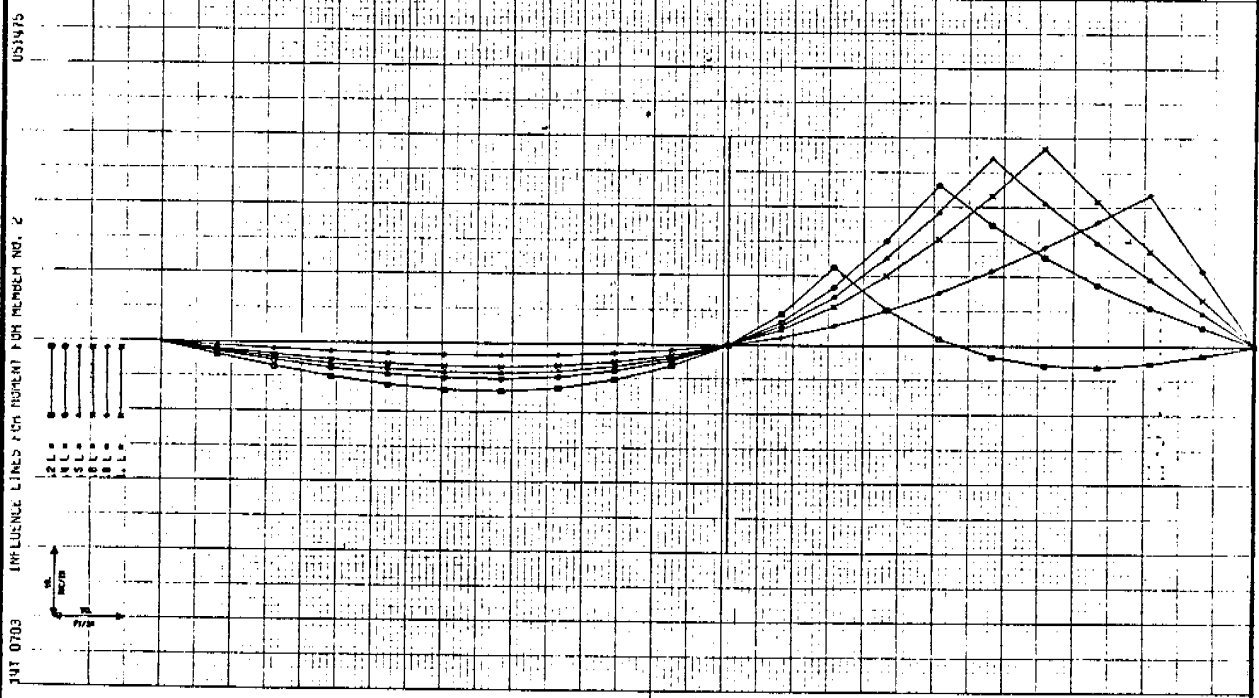
		MAX. AXIAL LOAD			MAX. LONGITUDINAL MOMENT		
		AXIAL LOAD	TUP	BOT.	AXIAL LOAD	TUP	BOT.
SUPPORT JT. 1	POSITIVE	79.4	0.	0.	0.0	0.	0.
	NEGATIVE	-4.8	0.	0.	0.0	0.	0.
MEMBER 3	POSITIVE	176.3	161.	-80.	94.0	1493.	-746.
	NEGATIVE	0.0	0.	0.	87.3	-1311.	656.
SUPPORT JT. 3	POSITIVE	77.4	0.	0.	0.0	0.	0.
	NEGATIVE	-6.4	0.	0.	0.0	0.	0.

THE RATIO OF SUBSTRUCTURE / SUPERSTRUCTURE LOADING IS 0.412

**** BATCH TOTALS 15 FRAME UNITS 2 L.L. UNITS 8 PLOT UNITS 0 PRESTRESS UNITS COST= \$ 5.60

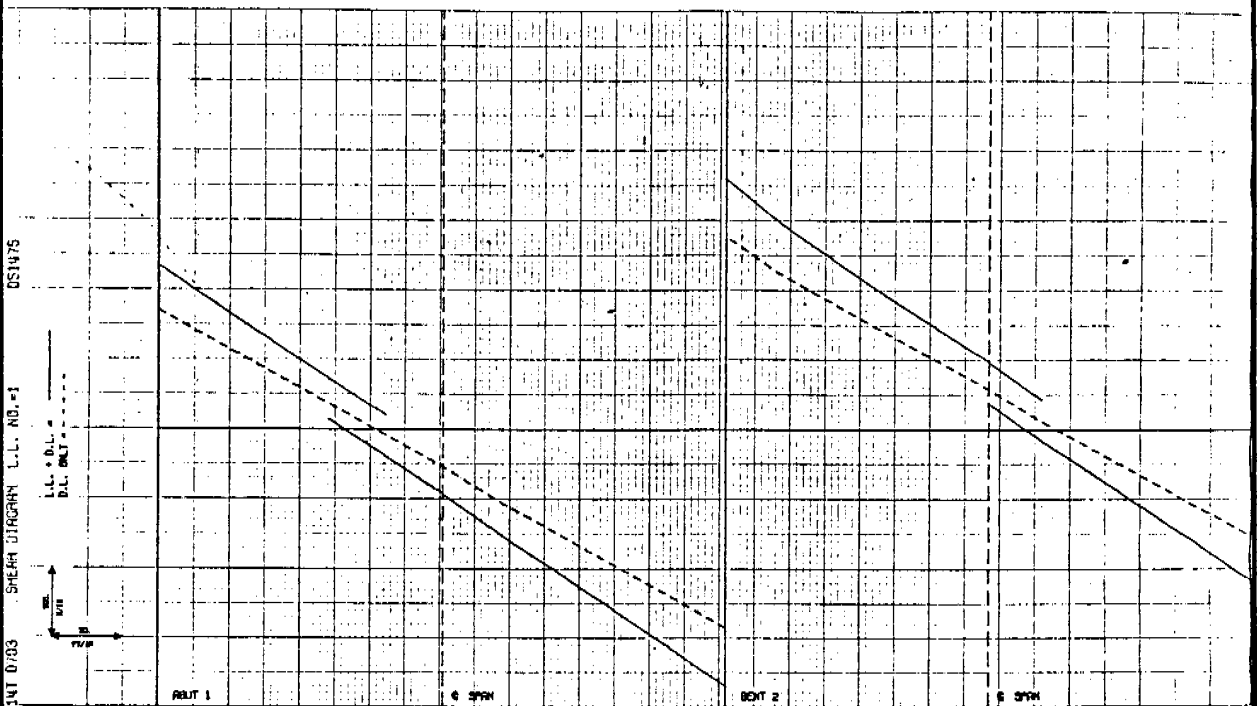


CALIFORNIA COMPUTER PRODUCTS, INC. ANAHEIM, CALIFORNIA CHART NO. 401 10 DIV. INCH



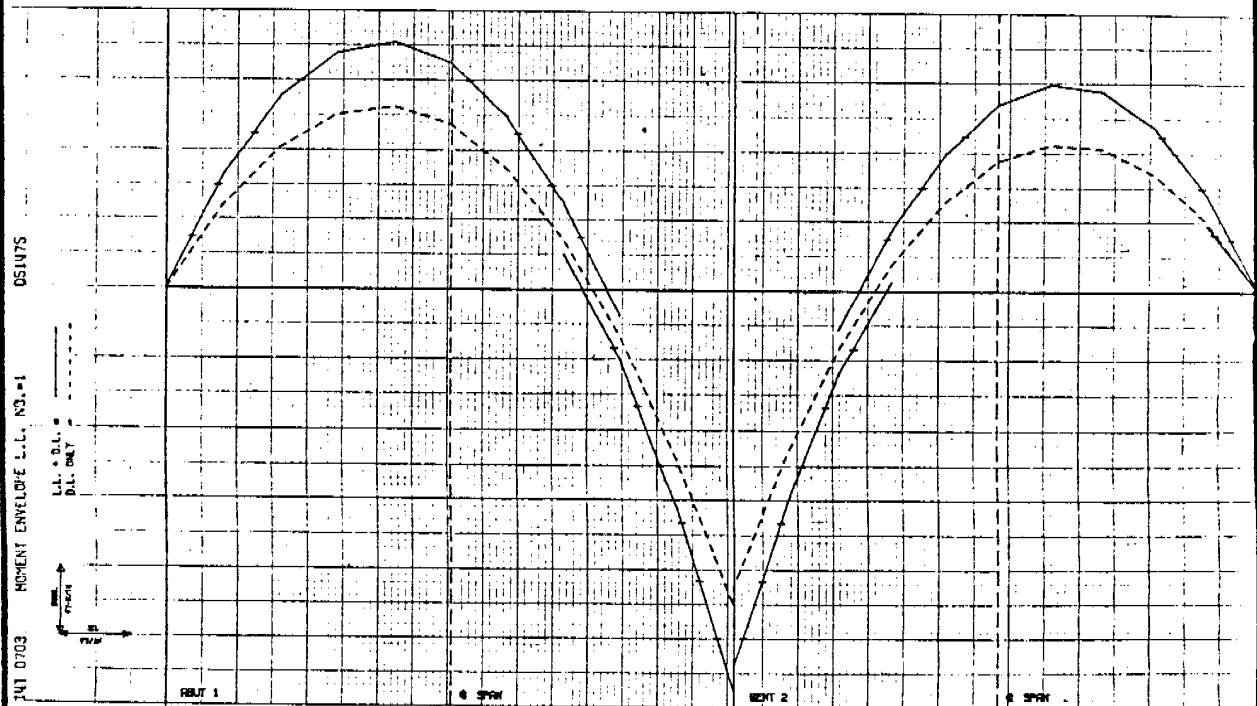
CALIFORNIA COMPUTER PRODUCTS, INC. ANAHEIM, CALIFORNIA CHART NO. 401 10 DIV. INCH

CALIFORNIA COMPUTER PRODUCTS, INC. ANAHEIM, CALIFORNIA CHART NO. 401 10 DIV. INCH



18 DIV INCH

CALIFORNIA COMPUTER PRODUCTS, INC. ANAHEIM, CALIFORNIA CHART NO. 401 18 DIV INCH



CALIFORNIA COMPUTER PRODUCTS, INC. ANAHEIM, CALIFORNIA CHART NO. 401 18 DIV INCH

CALIFORNIA COMPUTER PRODUCTS, INC.

SAMPLE PROBLEM 4

PROBLEM

A. General

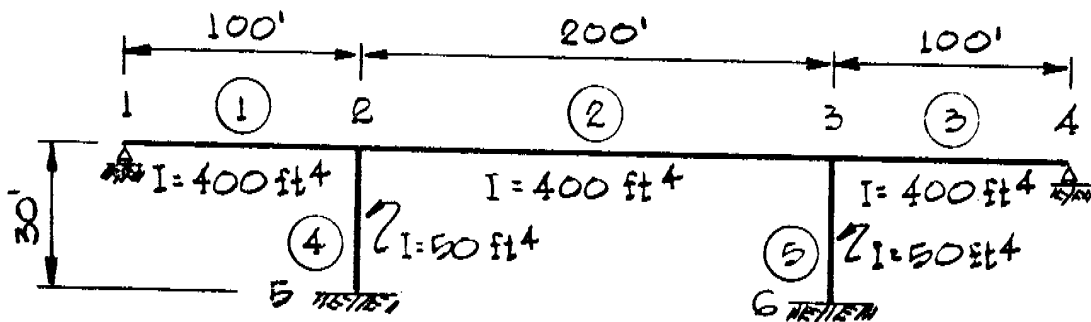
Three-span bridge with no expansion joints. Special maintenance overload truck to be automatically generated and moment and shear envelopes to be plotted.

B. Section Properties

All members prismatic as coded on Frame Description form. (See figure 8)

C. Loading

Dead loads coded on Frame Description as a uniform load. Live load as coded on Live Load Generator form.



DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - FRAME DESCRIPTION
DS-D93 (REV. 2-75)

BDE0AA

Page 1 of 2

IDENT: 14T 0704 SOURCE CHARGE: 1403314033910002
DIST. GR. BATCH PROB. DIST. UNIT DIST. UNIT AUTHORIZATION WHEN APPLICABLE
S/C 7301, 7310 S/C 2081

PROGRAM NUMBER: BDE035

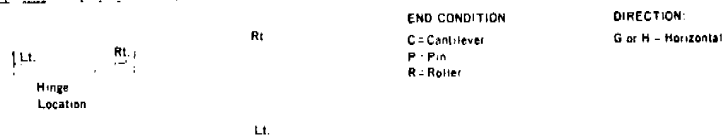
Name Example #4

Phone

Update

CODE	Line No.	Member No.	End Joint No.		End Condition Direction	Length	Min. I		Hinge Location or Support Width	Dead Load	Uniform Unit Wt.	Member Properties		Recall	D.L.			
			Lt.	Rt.			Stiffness Factor	Carry Over Factor				Member	Reverse			Deflections	Sideway	
								Lt.										Rt.
	1	1	2	P	G	100	40	0		3500					20			
	2	2	3		G	200												
	3	3	4	P	G	100												
	4	5	2			300	50	0										
	5	6	3			300	50	0										

S/C 7310



FRAME SYSTEM - Live Load Generator
DS-D124 (REV. 78)

BDE0AA

Page 2 of 2

Name Example #4

Phone

IDENT: 14T 0704
DIST. GR. BATCH PROB.
S/C 7322, 7323

MEMBER DATA

Update	CODE	Line No.	Member No.	Number of Live Lanes				Plot Date	COMMENTS
				Superstructure		Substructure			
L.L. End	Rt. End	Remaining Moment of Unit Steel		Moment & Shear Scale	Influence Lines				
		Positive	Negative						
		1	13	15				Frame Description data with the horizontal members numbered consecutively starting with 01 must accompany this data. Member Data - When the Number of L. L. Lanes is given, it must be given for the left end of Superstructure Member 01. (Substructure Member 01 defaults to 1.0 when left blank.) Thereafter, it is assumed to be constant until another entry is made. Live Load Data - Leave L. L. No. 4 blank for Standard P13 truck or check P13 box on Form DS-D125 if only one live load lane desired.	
		2	15	17					
		3	17	19					

S/C 7322

LIVE LOAD DATA

Update	CODE	Line No.	Multi-Axle Live Loading														OVER LOAD	No of Axles	Danger Loading	IMPACT	COMBINE CARD CONTROL								
			P _N	D ₁	P _{N+1}	D ₂	P _{N+2}	D ₃	P _{N+3}	D ₄	P _{N+4}	D ₅	P _{N+5}	D ₆	P _{N+6}	Kips						FL	Kips	FL	Kips	FL	Kips	FL	
		4																									1	1	
		4																										2	2
		5																										1	1
		5																										2	2
		6																										1	1
		6																										2	2

S/C 7323

IDENT 141 07 04

FRAME SYSTEM

MAY, 02, 1975

PAGE 1

FRAME DESCRIPTION

LINE NO.	MEM NO	JOINT		END COND		DIR	SPAN	SUPPORT OR HINGE		DEAD LOAD		CARRY OVER FACTORS		RECALL MEM		
		LT	RT	LT	RT			I	E	UNIFORM	SEC	LT	RT			
0010	1	1	2	P		G	100.0	400.00	0.0	0.	3.500	0.	0.0	0.0	0.0	0.0
0020	2	2	3			G	200.0	400.00	0.0	0.	3.500	0.	0.0	0.0	0.0	0.0
0030	3	3	4	P		G	200.0	400.00	0.0	0.	3.500	0.	0.0	0.0	0.0	0.0
0040	4	5	2				30.0	50.00	0.0	0.	0.0	0.	0.0	0.0	0.0	0.0
0050	5	6	3				30.0	50.00	0.0	0.	0.0	0.	0.0	0.0	0.0	0.0

IDENT 141 07 04

FRAME SYSTEM

MAY, 02, 1975

PAGE 2

FRAME DIAGNOSTICS

NO ERRORS FOUND

FRAME PROPERTIES

MEM NO	JT LT	JT RT	END COND		DIR	SPAN	SUPPORT OR HINGE		E	CARRY OVER FACTORS		DISTRIBUTION FACTORS	
			LT	RT			I			LT	RT	LT	RT
1	1	2	P		G	100.0	400.00	0.0	750.	0.500	0.0	0.0	0.450
2	2	3			G	200.0	400.00	0.0	750.	0.500	0.500	0.300	0.387
3	3	4	P		G	200.0	400.00	0.0	750.	0.0	0.500	0.290	0.0
4	5	2				30.0	50.00	0.0	750.	0.500	0.500	0.0	0.250
5	6	3				30.0	50.00	0.0	750.	0.500	0.500	0.0	0.323

IDENT 141 07 04

FRAME SYSTEM

MAY, 02, 1975

PAGE 3

FIXED END MOMENTS TRIAL 0

MEM NO	FIXED END MOMENTS		MEM NO	FIXED END MOMENTS		MEM NO	FIXED END MOMENTS	
	LT	RT		LT	RT		LT	RT
1	0.	+4375.	2	-11667.	-11667.	3	-17500.	0.
4	0.	0.	5	0.	0.			

*** SIDESWAY NOT CONSIDERED. ***

HORIZONTAL MEMBER MOMENTS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	852.	1354.	1506.	1308.	754.	-134.	-1387.	-2485.	-4933.	-7231.
2	-8814.	-3087.	1244.	4175.	5706.	5837.	4566.	1899.	-2170.	-7639.	-14506.
3	-16063.	-8175.	-1666.	3442.	7150.	9459.	10367.	4875.	7483.	4692.	0.

WARNING - MEMBER DEPTHS WERE NOT USED FOR ALL MEMBERS SO STRESSES WERE NOT CALC.

VERTICAL MEMBER MOMENTS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
4	793.	555.	317.	79.	-159.	-347.	-635.	-873.	-1111.	-1349.	-1587.
5	787.	551.	315.	79.	-157.	-344.	-630.	-866.	-1102.	-1336.	-1575.

HORIZONTAL MEMBER SHEARS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	102.7	67.7	32.7	-2.3	-37.3	-72.3	-107.3	-142.3	-177.3	-212.3	-247.3
2	321.5	251.5	181.5	111.5	41.5	-28.5	-98.5	-168.5	-238.5	-308.5	-378.5
3	430.4	360.4	290.4	220.4	150.4	80.4	10.4	-59.6	-129.6	-199.6	-269.6

VERTICAL MEMBER SHEARS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
4	-79.3	-79.3	-79.3	-79.3	-79.3	-79.3	-79.3	-79.3	-79.3	-79.3	-79.3

Page 4 of the output produces a warning indicating that member stresses could not be calculated from the available input data. As a result of this situation the program omits calculation of the horizontal member stresses. To obtain member stresses the structural depth must be given by a depth entry on the Super-structure Sections input form or a part code 27 on the section properties by parts input form. Member depths using part code 27 and an arbitrary part code 26 requires and entry for the Y coordinate of the center of gravity of the arbitrary section.

*** SIDESWAY NOT CONSIDERED. ***

VERTICAL MEMBER SHEARS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
5	-78.7	-78.7	-78.7	-78.7	-78.7	-78.7	-78.7	-78.7	-78.7	-78.7	-78.7

VERTICAL MEMBER REACTIONS TRIAL 0

MEM NO	LI REACTION	RI REACTION	MEMBER WEIGHT
4	508.9	508.9	0.0
5	808.9	808.9	0.0

IDENT 141 07 04 FRAME SYSTEM MAY. 02, 1975 PAGE 6

TRIAL 0

TANGENTIAL ROTATIONS - RADIAN - COUNTERCLOCKWISE POSITIVE

SPAN	LT. END	RT. END	SPAN	LT. END	RT. END	SPAN	LT. END	RT. END
1	0.000566	0.002204	2	0.002204	0.002187	3	0.002187	-0.014597
4	-0.000000	0.002204	5	-0.000000	0.002187			

HORIZONTAL MEMBER DEFLECTIONS IN FEET AT 1/20 POINTS FROM LEFT END - DOWNWARD POSITIVE

MEMBER	E	750.	0.0	0.063	0.005	0.008	0.009	0.010
MEMBER 1	E=	750.	0.010	0.009	0.007	0.004	0.001	-0.003
			-0.007	-0.010	-0.014	-0.016	-0.014	-0.017
			-0.015	-0.009	0.0			
MEMBER 2	E=	750.	0.0	0.031	0.076	0.127	0.181	0.231
			0.275	0.310	0.333	0.342	0.338	0.320
			0.290	0.250	0.202	0.149	0.096	0.049
			0.012	-0.007	0.0			
MEMBER 3	E=	750.	0.0	0.039	0.105	0.191	0.288	0.388
			0.486	0.577	0.654	0.716	0.757	0.777
			0.773	0.746	0.695	0.621	0.526	0.413
			0.284	0.145	0.0			

VERTICAL MEMBER DEFLECTIONS IN FEET AT 1/20 POINTS FROM LEFT END.

Page 6 reports tangential rotations at the ends of each member. Deflections at the 1/20 points were requested on the Frame Description form and printed for each horizontal member.

IDENT 141 07 04 FRAME SYSTEM MAY. 02, 1975 PAGE 7

TRIAL 0

MEMBER 4	E=	750.	0.0	-0.000	-0.001	-0.001	-0.002	-0.003
			-0.004	-0.005	-0.006	-0.007	-0.004	-0.009
			-0.010	-0.010	-0.010	-0.009	-0.008	-0.007
			-0.005	-0.003	0.0			
MEMBER 5	E=	750.	0.0	-0.000	-0.001	-0.001	-0.002	-0.003
			-0.004	-0.005	-0.006	-0.007	-0.006	-0.009
			-0.009	-0.010	-0.010	-0.009	-0.008	-0.007
			-0.005	-0.003	0.0			

LIVE LOAD DIAGNOSTICS

NO ERRORS FOUND

LIVE LOAD GENERATOR

LINE NO.	MEM NO.	NUMBER OF LIVE LOAD LANES				RESISTING MOMENT OF UNIT STEEL		PL-11 M & S SCALE ENV.	PL-11	INFLUENCE LINES	PL-13
		SUPERSTRUCTURE LT,END	SUPERSTRUCTURE RT,END	SUBSTRUCTURE LT,END	SUBSTRUCTURE RT,END	POSITIVE	NEGATIVE				
0010	1	1,300	1,500	1,0	1,0	0,	0,	1	0	NO	YES
0020	2	1,500	1,700	1,0	1,0	0,	0,				
0030	3	1,700	1,900	1,0	1,0	0,	0,				

LIVE LOAD

LINE NO.	LOAD NO.	P1	D2	P3	D4	P5	D6	P7	D8	P9	D10	P11	D12	P13	D14	P15	D16	P17	D18	P19	D20	P21	D22	P23	D24	P25	OVERLOAD	HWL	IMPACT	LUMB	LAND CONTROL	
4.	4.	20,0	18,0	48,0	18,0	48,0	18,0	48,0	18,0	48,0	18,0	48,0	18,0	48,0	18,0	48,0	18,0	48,0	18,0	48,0	18,0	48,0	18,0	48,0	18,0	48,0	18,0	0.	YES	00		
		48,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0	0,0					

Page 8 reports the input data as coded on the Live Load Generator input sheet. In this example a standard P-13 family of trucks is assumed to be the liveload vehicles. The axle spacing and loads are generated and printed for the maximum length truck that is used in the live load analysis. Live load numbers 4 through 6 output values are similar to superstructure live load results. If a particular truck is to be moved across the superstructure, then an entry must be made in the overload field to indicate a match between the "P" loads given and the axle loads of the particular truck. Output for this option is labeled with appropriate titles to indicate that a special truck was used for the generation of moment and shear envelopes.

LL NO. 4. NEGATIVE LIVE LOAD MOMENT ENVELOPE AND ASSOCIATED SHEARS

MEM NO.	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-734.	-1469.	-2203.	-2937.	-3671.	-4406.	-5140.	-5874.	-6608.	-7343.
SHEAR	0,0	-46,5	-46,5	-46,5	-46,5	-46,5	-46,5	-46,5	-46,5	-46,5	-46,5
2	-11422.	-5097.	-1181.	-965.	-1388.	-2494.	-3600.	-4707.	-5813.	-6919.	-9960.
SHEAR	224,2	164,8	7,7	7,7	-30,9	-30,9	-30,9	-30,9	-30,9	-30,9	-222,3
3	-15255.	-7324.	-3778.	-3305.	-2833.	-2361.	-1889.	-1417.	-944.	-472.	0.
SHEAR	237,9	194,2	14,6	14,6	14,6	14,6	14,6	14,6	14,6	14,6	0,0

OUTPUT

Sample Problem 4

IDENT 141 07 04 FRAME SYSTEM MAY, 02, 1975 PAGE 10

LL NO. 4, DEAD LOAD PLUS NEGATIVE LIVE LOAD MOMENT ENVELOPE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	118.	-115.	-897.	-1629.	-2912.	-4544.	-6526.	-8859.	-11541.	-14574.
2	-26240.	-8184.	63.	3210.	4310.	3345.	968.	-2806.	-7963.	-14555.	-24477.
3	-31330.	-15499.	-5444.	137.	4317.	7098.	8478.	8459.	7039.	4220.	0.

IDENT 141 07 04 FRAME SYSTEM MAY, 02, 1975 PAGE 11

LL NO. 4, POSITIVE LIVE LOAD MOMENT ENVELOPE AND ASSOCIATED SHEARS

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	1865.	3072.	3960.	4350.	4294.	3790.	2022.	1502.	1757.	1952.
SHEAR	0.0	130.9	165.9	72.1	40.1	-51.2	-84.2	-115.8	10.9	10.9	10.9
2	3037.	1930.	2910.	6706.	9313.	10397.	9854.	7719.	5971.	677.	547.
SHEAR	-30.9	-30.9	140.4	129.8	88.2	37.5	-69.5	-119.8	-159.5	-98.8	7.7
3	259.	670.	3400.	8670.	12957.	15626.	16514.	15524.	12534.	7369.	0.
SHEAR	0.9	80.2	154.9	158.4	123.4	75.1	-30.5	-80.8	-140.3	-200.0	0.0

IDENT 141 07 04 FRAME SYSTEM MAY, 02, 1975 PAGE 12

LL NO. 4, DEAD LOAD PLUS POSITIVE LIVE LOAD MOMENT ENVELOPE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	2717.	4426.	5666.	5658.	5054.	3651.	1435.	-1423.	-3170.	-5279.
2	-2781.	-1156.	4154.	10881.	15019.	16234.	14423.	9618.	1801.	-6762.	-13961.
3	-15824.	-7505.	1814.	12112.	20100.	25085.	26881.	25399.	20517.	12060.	0.

IDENT 141 07 04 FRAME SYSTEM MAY, 02, 1975 PAGE 13

LL NO. 4, LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS

MEMBER	1	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
PJS. V		231.7	180.5	146.8	112.3	82.2	57.6	37.5	21.8	19.5	19.5	19.5
MOMENT		0.0	1865.0	3019.4	3364.4	3286.1	2679.6	2248.3	1528.4	1561.7	1750.9	1952.1
NEG. V		-73.4	-73.4	-73.4	-73.4	-73.4	-94.9	-129.8	-168.4	-214.7	-264.4	-313.0
MOMENT		0.0	-734.3	-1466.5	-2202.8	-2937.0	-3014.1	-2976.3	-2384.2	-1115.1	-1146.1	-3534.3
RANGE		305.1	259.9	220.3	185.7	155.6	126.5	107.3	190.3	234.3	264.3	332.5

LL NO. 4, LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS

MEMBER	2	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
PJS. V		440.4	387.8	327.4	262.7	197.8	136.4	86.1	48.1	21.9	10.9	10.9
MOMENT		-4411.0	-3385.2	1756.0	5413.0	7275.7	7338.6	6135.1	4264.5	2345.2	331.3	547.4
NEG. V		-55.3	-55.3	-55.3	-55.3	-73.3	-120.3	-180.0	-247.6	-319.5	-391.7	-460.4
MOMENT		3030.0	1930.4	824.2	-282.0	5552.4	7010.5	7421.0	6154.8	2993.6	-2606.2	-6442.5
RANGE		495.7	443.1	382.7	318.1	271.1	256.7	266.1	295.7	341.3	402.5	471.2

LL NO. 4, LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS

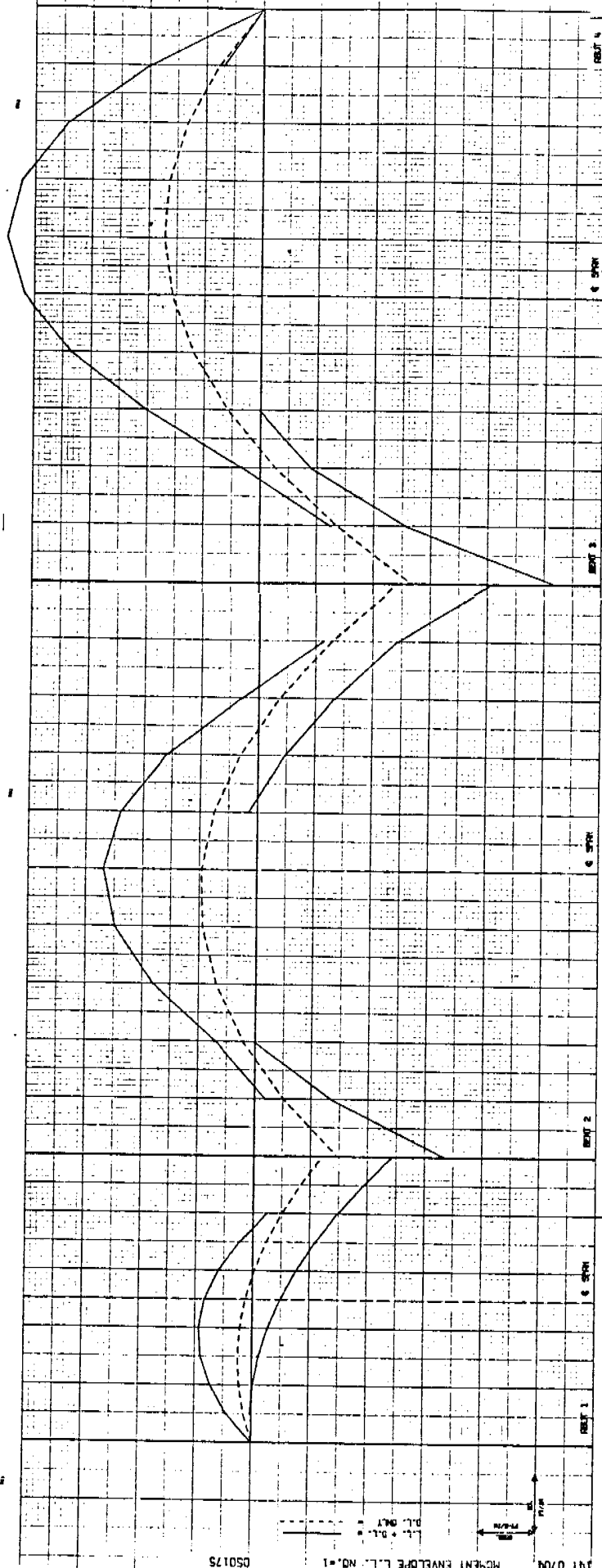
MEMBER	3	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
PJS. V		531.9	486.0	430.2	365.5	293.0	217.1	147.7	90.2	45.8	23.0	23.0
MOMENT		-11820.1	-4669.5	1952.6	7296.3	10690.9	11699.9	10618.9	8147.0	4998.0	-472.2	0.0
NEG. V		-1.3	-3.1	-14.2	-32.0	-61.0	-101.5	-154.2	-217.1	-288.9	-368.4	-454.6
MOMENT		259.3	553.9	2269.0	4561.5	7319.8	10125.1	12334.4	13023.6	11554.3	7368.5	0.0
RANGE		533.2	489.1	444.4	398.0	354.0	318.3	301.9	307.3	334.0	392.0	478.2

OUTPUT

Sample Problem 4

IDENT 141 07 04		FRAME SYSTEM										MAY, 02, 1975		PAGE 14	
LL NO. 4.		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE													
MEMBER	1	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT			
POS. V			334.4	254.2	179.5	110.0	44.8	-14.7	-69.8	-120.5	-157.8	-192.8	-227.8		
NEG. V			29.3	-5.7	-40.7	-75.7	-110.7	-167.2	-237.1	-310.6	-392.1	-477.1	-560.3		
LL NO. 4.		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE													
MEMBER	2	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT			
POS. V			762.0	639.4	508.9	374.3	239.3	108.0	-12.3	-120.3	-210.0	-297.6	-367.6		
NEG. V			266.2	196.2	126.2	56.2	-31.8	-148.7	-278.5	-416.0	-557.9	-700.2	-836.8		
LL NO. 4.		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE													
MEMBER	3	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT			
POS. V			962.3	846.4	720.6	585.9	443.4	297.5	158.1	30.6	-63.8	-176.0	-276.0		
NEG. V			429.1	357.3	276.2	187.8	89.4	-20.6	-143.8	-276.6	-418.4	-568.0	-724.2		

IDENT 141 07 04		FRAME SYSTEM						MAY, 02, 1975		PAGE 15	
LL NO. 4.		LIVE LOAD SUPPORT RESULTS									
		MAX. AXIAL LOAD	MAX. AXIAL LOAD		MAX. LONGITUDINAL MOMENT						
		AXIAL LOAD	TOP	BOT.	AXIAL LOAD	TOP	BOT.				
SUPPORT JT. 1	POSITIVE	171.6	0.	0.	0.0	0.	0.				
	NEGATIVE	-46.5	0.	0.	0.0	0.	0.				
MEMBER 4	POSITIVE	347.6	-1125.	562.	202.2	1058.	-529.				
	NEGATIVE	-41.8	606.	-303.	270.7	-2581.	1290.				
MEMBER 5	POSITIVE	346.6	-1048.	524.	232.6	3236.	-1618.				
	NEGATIVE	-8.6	-205.	102.	272.4	-4041.	2620.				
SUPPORT JT. 4	POSITIVE	244.3	0.	0.	0.0	0.	0.				
	NEGATIVE	-14.6	0.	0.	0.0	0.	0.				
**** BATCH TOTALS		15 FRAME UNITS		6 L.L. UNITS		6 PLUT UNITS		0 PRESTRESS UNITS		LOSTS = 7.20	

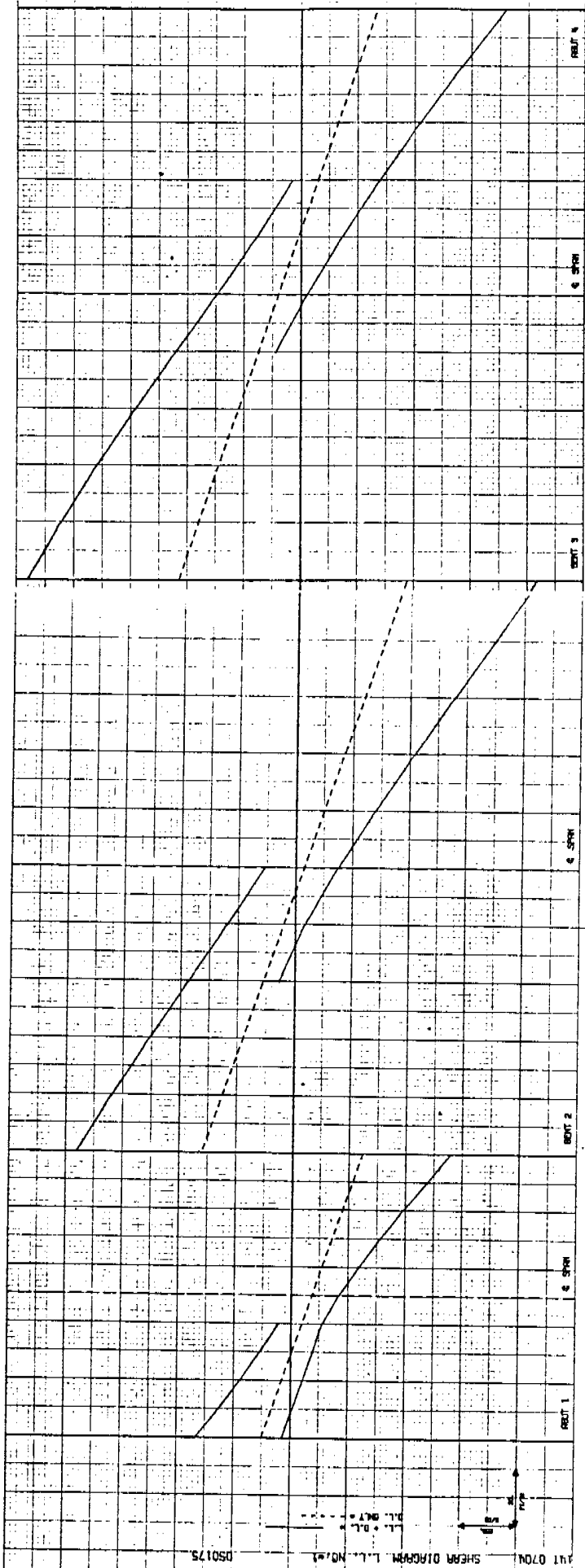


44T 0704 MOCHENT ENVELOPE E.L. NO. #1 050175

CALIFORNIA COMPUTER PRODUCTS, INC. ANAHEIM, CALIFORNIA CHART NO. 401 10 BY 10 IN

CALIFORNIA COMPUTER PRODUCTS, INC. ANAHEIM, CALIFORNIA CHART NO. 401 10 BY 10 IN

CALIFORNIA COMPUTER PRODUCTS, INC. ANAHEIM, CALIFORNIA CHART NO. 401 10 BY 10 IN



CALCOMP COMPUTER PRODUCTS INC. ANALYSIS CALCOMP, PRINTED BY CALCOMP, INC. IN BOSTON, MASS. 02114
 MAPS NO. 601 10 3/4" X 14" 1/4"

SAMPLE PROBLEM 5

PROBLEM

A. General

Six-span, two frames, prestressed bridge with one expansion joint. Prestress analysis to be computed by program.

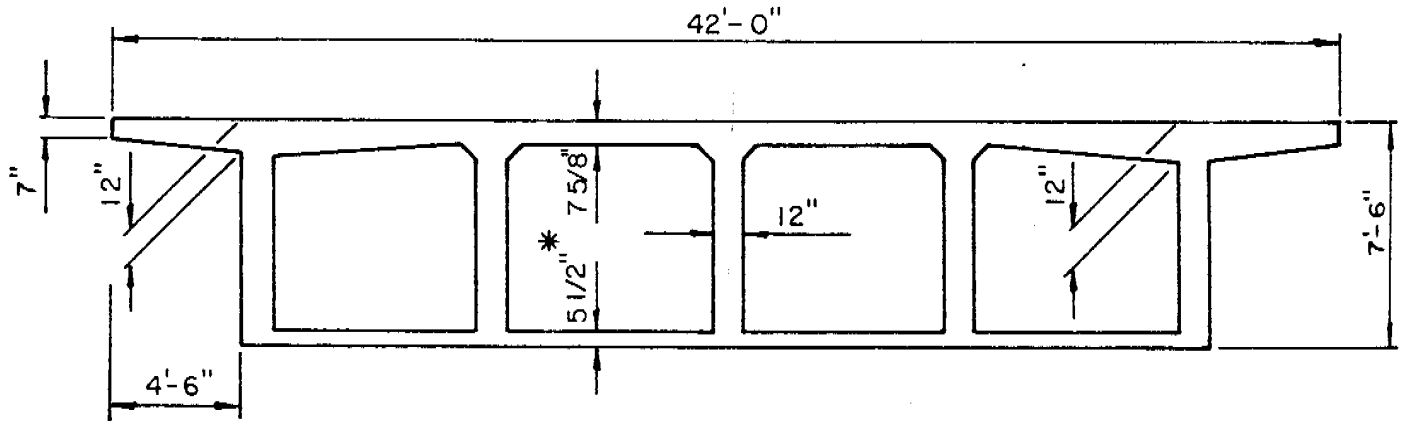
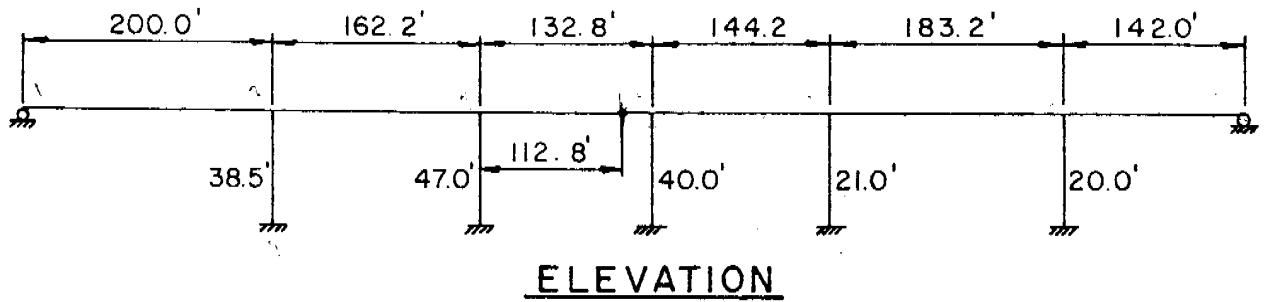
B. Section Properties

The columns are nonprismatic as shown in figure 9 and 10. The superstructure cross-section varies as shown on figure 9.

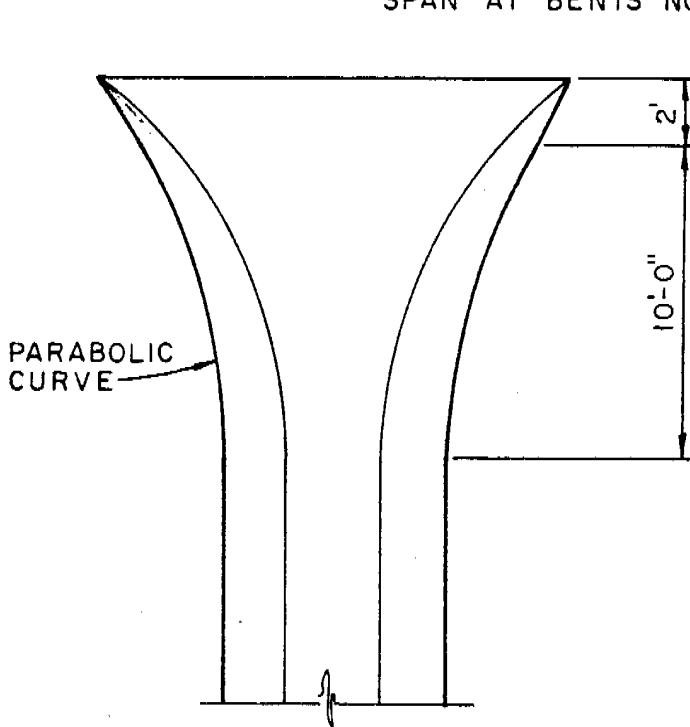
C. Loading

The dead loads are calculated from the unit weight of concrete times the cross-sectional areas generated by the program plus additional loads described on Load data form trial 00. Additional dead loads to be applied after prestressing are described on Load Data form under trial 01. Live loading to be applied to superstructure is 2.75 lanes of AASHTO HS20-44 loading without alternative.

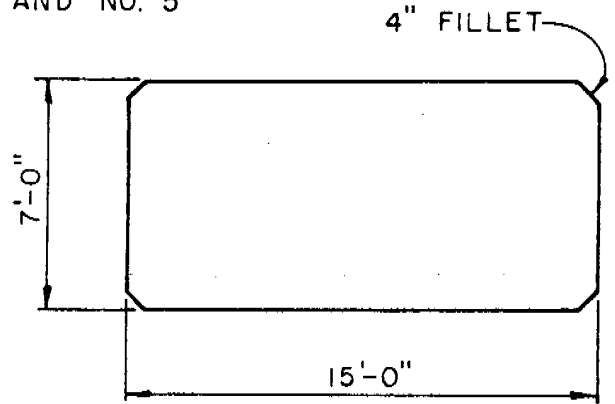
EXAMPLE: TWO FRAME PRESTRESSED BRIDGE



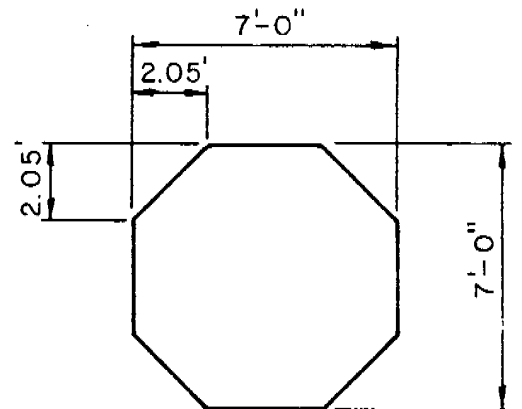
* 9" BOTTOM SLAB FLARE TO 0.1 PT. OF THE SPAN AT BENTS NO. 2 AND NO. 5



COLUMN ELEVATION

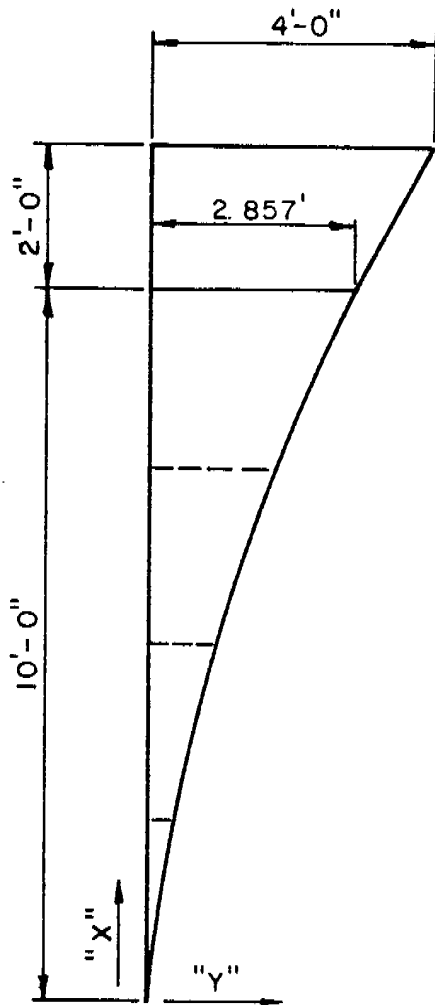


COLUMN AT TOP



COLUMN AT BASE

BENT COLUMNS



PARABOLIC CALCULATIONS

$$Y = mx^2 \quad X = \sqrt{y/m}$$

$$\text{SLOPE} = dy/dx = 2mx$$

Horizontal distance = Parabolic distance + Slope X Run

$$4' = mx^2 + (2mx) \times (2)$$

$$4' = 100m + 40m \quad \text{at } x = 10'$$

$$4' = 140m \quad m = 1/35$$

$$Y = (1/35) \times 10^2 = 2.857'$$

DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - FRAME DESCRIPTION

BDE0AA

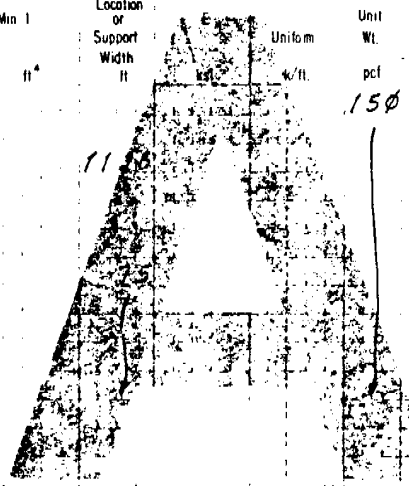
Page 1 of 9

IDENT. SOURCE CHARGE EXPENDITURE SPECIAL DESIGNATION PROGRAM
DIST. GR. BATCH PROR. DIST. UNIT DIST. UNIT AUTHORIZATION WHEN APPLICABLE NUMBER
14T 2001 1403314033910002 BDE035
S.C. 2091, 7310 S.C. 2091

Name EXAMPLE #5

Phone 2091

Update	Line No.	Member No.	End Joint No.		Length	Min I	Hinge Location or Support Width	Dead Load	Member Properties				Recall	D.L.
			Lt.	Rt.					Stiffness Factor	Carry Over Factor	Member	Reverse		
	1	1	22	0000				150						
	2	2	3	1622										
	3	3	4	1328										
	4	4	5	1442										
	5	5	6	1832										
	6	6	7	1420										
	7	8	2	385										
	8	9	3	470										
	9	10	4	400										
	10	11	5	210										
	11	12	6	200										



S/C 7310

END CONDITION

DIRECTION

Lt. Rt.
Hinge Location

C - Cantilever
P - Pin
R - Roller

G or H - Horizontal

DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - SUPERSTRUCTURE SECTIONS

BDE0AA

Page 2 of 9

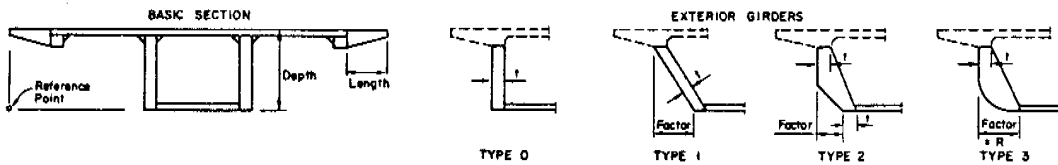
IDENT. SOURCE CHARGE EXPENDITURE SPECIAL DESIGNATION PROGRAM
DIST. GROUP BATCH PROR. DIST. UNIT DIST. UNIT AUTHORIZATION WHEN APPLICABLE NUMBER
14T 2001 BDE035
S.C. 2091, 7311 S.C. 2091

Name Example #5

Phone

UPDATE	LINE NO.	MEMBER NO.	CROSS SECTION LOCATION	REF. PT. COORD	S.S. DATA	EXTERIOR GIRDERS		OVERHANGS				STORE	
						LEFT	RIGHT	LEFT	RIGHT	LEFT	RIGHT		
	1	00	1		420	2012	012		45	7	1245	7	1202
	1	1800	2										
	1	2000	01		420	2012	012						03
	2	00	03										
	2	162	02										
	2	142	02										
	2	162	03										
	3	00	03										
	3	200	02										
	3	1328	02										
	4	00	02										
	4	1442	03										

S/C 7311



TYPE 9 MEANS NO EXTERIOR GIRDER

DEPARTMENT OF TRANSPORTATION
 FRAME SYSTEM - SUPERSTRUCTURE SECTIONS
 DS D112 (REV 4/75)

BDE0AA

Page 3 of 9

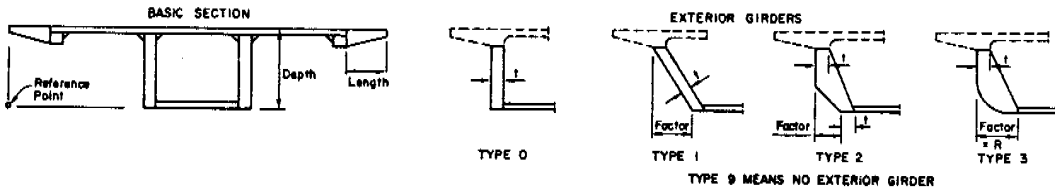
Name Example #5

Phone

IDENT		SOURCE		CHARGE	EXPENDITURE AUTHORIZATION	SPECIAL DESIGNATION WHEN APPLICABLE	PROGRAM NUMBER
DIST.	GROUP BATCH	DIST.	UNIT	DIST.	UNIT		
14T 2001		S/C 2001					

UPDATE	LINE NO.	MEMBER NO.	CROSS SECTION LOCATION	REF. PT. COORD	S.S. DATA	INT. AIRSPACES	EXTERIOR GIRDERS				OVERHANGS				STORE				
							LEFT	RIGHT	LEFT	RIGHT	LEFT	RIGHT	LEFT	RIGHT					
REC'D	NO.	NO.	(FT)	X	Y	WIDTH	DEPTH	WEB THICK	FACTOR	TYPE	WEB THICK	FACTOR	LENGTH	EXT. THICK	INT. THICK	LENGTH	EXT. THICK	INT. THICK	
		5	00.03																
		5	183.02																
		5	164.902																
		5	183.203																
		6	00.03																
		6	142.002																
		7	00.04																
		7	285.04																
		7	335.07																
		7	385.06																
		7	405.05																
		8	00.04																

S/C 7311



DEPARTMENT OF TRANSPORTATION
 FRAME SYSTEM - SUPERSTRUCTURE SECTIONS
 DS D112 (REV 4/75)

BDE0AA

Page 4 of 9

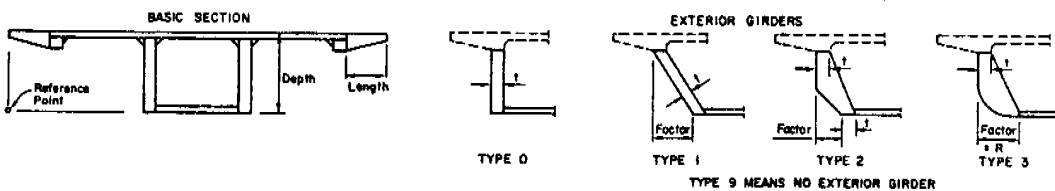
Name Example #5

Phone

IDENT		SOURCE		CHARGE	EXPENDITURE AUTHORIZATION	SPECIAL DESIGNATION WHEN APPLICABLE	PROGRAM NUMBER
DIST.	GROUP BATCH	DIST.	UNIT	DIST.	UNIT		
14T 2001		S/C 2001					

UPDATE	LINE NO.	MEMBER NO.	CROSS SECTION LOCATION	REF. PT. COORD	S.S. DATA	INT. AIRSPACES	EXTERIOR GIRDERS				OVERHANGS				STORE				
							LEFT	RIGHT	LEFT	RIGHT	LEFT	RIGHT	LEFT	RIGHT					
REC'D	NO.	NO.	(FT)	X	Y	WIDTH	DEPTH	WEB THICK	FACTOR	TYPE	WEB THICK	FACTOR	LENGTH	EXT. THICK	INT. THICK	LENGTH	EXT. THICK	INT. THICK	
		8	35.004																
		8	400.07																
		8	450.06																
		8	470.05																
		9	00.04																
		9	280.04																
		9	330.04																
		9	380.06																
		9	400.05																
		10	00.04																
		10	90.04																
		10	140.07																

S/C 7311



DEPARTMENT OF TRANSPORTATION
 FRAME SYSTEM - SUPERSTRUCTURE SECTIONS

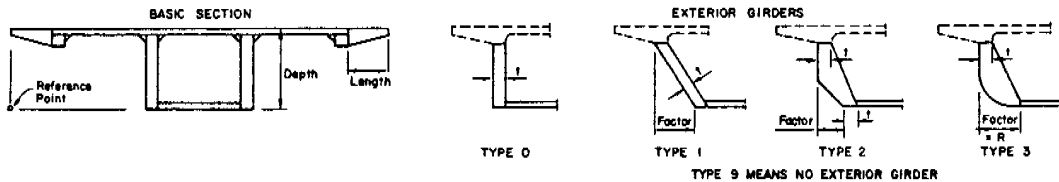
BDE0AA

Page 5 of 9
 Name Example #5
 Phone

IDENT				SOURCE		CHARGE		EXPENDITURE		SPECIAL DESIGNATION		PROGRAM	
DIST.	GROUP	BATCH	PROB.	DIST.	UNIT	DIST.	UNIT	AUTHORIZATION		WHEN APPLICABLE		NUMBER	
IAT 2001				S/C 2081								B D E 0 3 5	
S/C 2091, 7311				S/C 2081									

UPDATE	LINE NO.	MEMBER NO.	CROSS SECTION LOCATION	RECALL	REF. PT. COORD.		S.S. DATA		EXTERIOR GIRDERS				OVERHANGS				STORE					
					X	Y	WIDTH	DEPTH	LEFT		RIGHT		LEFT		RIGHT							
CROSS SECTION			(FT.)		(FT.)	(FT.)	(FT.)	(FT.)	(IN.)	WEB THICK (IN.)	FACTOR (FT.)	TYPE	WEB THICK (IN.)	FACTOR (FT.)	LENGTH (FT.)	EXT. THICK (IN.)	INT. THICK (IN.)	LENGTH (FT.)	EXT. THICK (IN.)	INT. THICK (IN.)		
	0		19006																			
	10		21005																			
	11		0004																			
	11		8004																			
	11		13007																			
	11		18006																			
	11		20005																			

S/C 7311



DEPARTMENT OF TRANSPORTATION
 FRAME SYSTEM - SECTION PROPERTIES BY PARTS

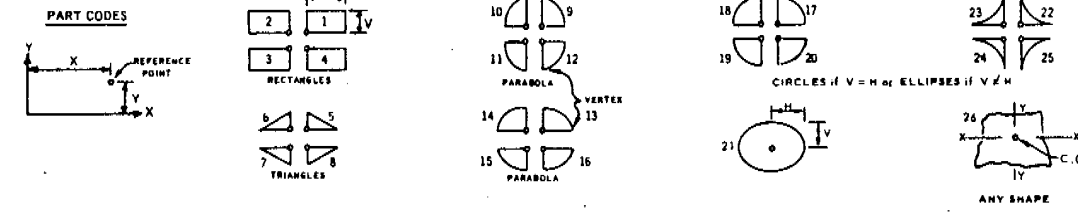
BDE0AA

Page 6 of 9
 Name Example #5
 Phone

IDENT				SOURCE		CHARGE		EXPENDITURE		SPECIAL DESIGNATION		PROGRAM	
DIST.	GROUP	BATCH	PROB.	DIST.	UNIT	DIST.	UNIT	AUTHORIZATION		WHEN APPLICABLE		NUMBER	
IAT 2001				S/C 2091, 7312		S/C 2081						B D E 0 3 5	
S/C 2091, 7312				S/C 2081									

UPDATE	LINE NO.	MEMBER NO.	CROSS SECTION LOCATION	RECALL	SIGN	PART CODE	PART DIMENSIONS		REF. PT. COORD.		ANY SHAPE			STORE
							Vertical or Depth D	Horizontal H	X	Y	n ⁴	lxx	lyy	
	0		00			8	0.37	14.50		6.87				01
			00			8	0.37	0.67						
			10			1	7.00	0.50						
			10			5	2.05	0.50						
			10			6								
			10			7								
			10			8								
			20			1	7.00	1.00						04
			20			5	0.33	0.33						
			20			6								
			20			7								
			20			8								05

S/C 7312



DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - SECTION PROPERTIES BY PARTS

BDE0AA

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DS-094 (REV 2 75)

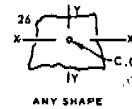
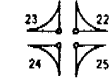
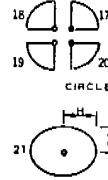
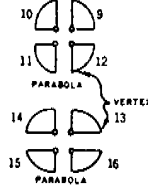
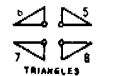
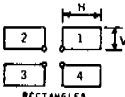
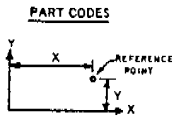
IDENT.			
DIST.	GROUP	BATCH	PROG.
14T	2001		
S/C 2081, 7312			

SOURCE	CHARGE	EXPENDITURE	SPECIAL DESIGNATION	PROGRAM
DIST. UNIT	DIST. UNIT	AUTHORIZATION	WHEN APPLICABLE	NUMBER
B D E P 3 5				

Phone

Update	CODE	Line No.	Member No.	Cross Section Location	Recall	Sign or	Part Code	Part Dimensions		Ref. Pt. Coord.		Area	Ixx	Iyy	Store
								Vertical Y or Depth D	Horizontal H	X	Y				
				3φ			1	700	1271						
							5	082	082						
							6								
							7								
				4φ			8	700	842						06
							1								
							5	174	174						07
							6								
							7								
							8								

S/C 7312



DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - SUPERSTRUCTURE LIVE LOAD

BDE0AA

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DS-0125 (REV 2 75)

IDENT.			
DIST.	GR.	BATCH	PROG.
14T	2001		
S/C 7320, 7321			

Name Example #5

Phone

MEMBER DATA

Update	CODE	Line No.	Member No.	Number of Live Load Lanes				Plot Data				COMMENTS
				Superstructure		Substructure		Resisting Moment of Unit Steel		Influence Lines	P-13	
				Lt. End	Rt. End	Lt.	Rt.	Positive	Negative			
			1	27.50		27	27					

Frame Description data with the horizontal members numbered consecutively starting with 01 must accompany this data.

Member Data - When the Number of L.L. Lanes is given, it must be given for the left end of Superstructure Member 01. (Substructure Member 01 defaults to 1.0 when left blank.) Thereafter, it is assumed to be constant until another entry is made.

Live Load Data - For AASHTO HS20-44 loading, leave Truck and Lane data blank for L.L. No. 1. When this data is given, it replaces the HS20-44 loading. An entry for the Number of Live Load Lanes, overrides that given as Member Data. Data entries for L.L. No.'s 2 and 3 produce separate results in addition to L.L. No. 1.

Influence Lines - When checked a plot of the influence lines will be produced along with the printed results.

S/C 7320

LIVE LOAD DATA

Update	CODE	Line No.	L.L. No.	Truck - (1 Lane)					Uniform Moment Rider	Shear Rider	No. Impact	Number of Live Load Lanes	COMMENTS
				P ₁	D ₁	P ₂	D ₂	P ₃					
			1										
			2										
			3										

S/C 7321

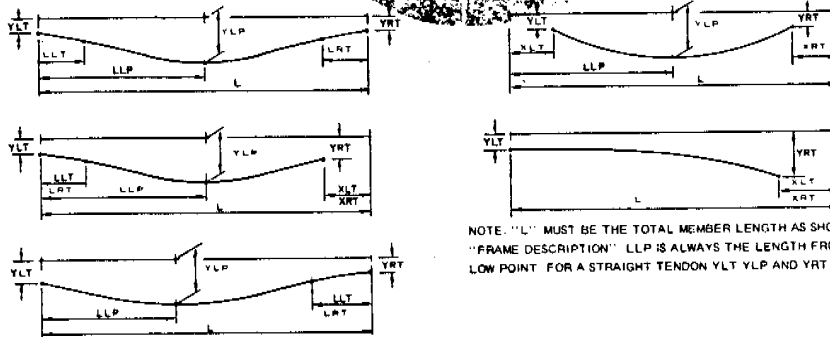
DEPARTMENT OF TRANSPORTATION
FRAME SYSTEM - PRESTRESSED DATA
DS-D150 Rev 3/75

IDENT
DIST GROUP BATCH PROB
14T 2001
S/C 7315

BDE0AA Page 9 of 9
Name Example #5
Phone

Update	Cable Path	Specifications	Anchor Set		Allow Tension	P-Jock	f _c	% Shortening Losses																		
			LT	RT																						
CODE	Line No	Trial No	Frame No	Path No	Member No	LLT	LLP	LRT	YLT	YLP	YRT	XLT	XRT	u	k	f _s	% Jack	End	LT	RT	Sec	%	KIPS	KSI	%	
	111	1				40	10		300	650																
	111	2	1050	10		125	500		150																	
	111	3	1060			150	500		300																	
	121	3				275			150																	
	121	4	1050	10		150	500		125	1128																
	121	5	1050	10		125	650		125																	
	121	6	1060			125	500		300																	

8/2 7316



NOTE: "L" MUST BE THE TOTAL MEMBER LENGTH AS SHOWN ON "FRAME DESCRIPTION". LLP IS ALWAYS THE LENGTH FROM THE LEFT END TO THE LOW POINT. FOR A STRAIGHT TENDON YLT, YLP AND YRT ARE REQUIRED INPUT.

IDENT		14T 20 01		FRAME SYSTEM		MAY. 15, 1975		PAGE 1			
FRAME DESCRIPTION											
LINE NO.	MEM NO.	JOINT NO.	END COND	DIR	SPAN	SUPPRT OR HINGE	DEAD LOAD UNIFORM	SEC	K	CARRY OVER FACTORS	RECALL MEM
		LT RT	LT RT			I	E		LT RT	LT RT	
0010	1	1	2	R	G	200.0	0.0	0.0	0.0	0.0	0.0
0020	2	2	3		G	162.2	0.0	0.0	0.0	0.0	0.0
0030	3	3	4		G	132.8	0.0	112.8	0.0	0.0	0.0
0040	4	4	5		G	144.2	0.0	0.0	0.0	0.0	0.0
0050	5	5	6		G	183.2	0.0	0.0	0.0	0.0	0.0
0060	6	6	7	R	G	142.0	0.0	0.0	0.0	0.0	0.0
0070	7	8	2			32.5	0.0	7.5	0.0	0.0	0.0
0080	8	9	2			47.0	0.0	7.5	0.0	0.0	0.0
0090	9	10	4			40.0	0.0	7.5	0.0	0.0	0.0
0100	10	11	5			21.0	0.0	7.5	0.0	0.0	0.0
0110	11	12	6			20.0	0.0	7.5	0.0	0.0	0.0

Page 1 thru Page 55 - This is the output from Frame System which defines the frame, member and frame properties, dead load, added dead loads and live load results. Since a prestress design will utilize all of this information, users should carefully review it for accuracy and completeness.

IDENT		14T 20 01		FRAME SYSTEM		MAY. 15, 1975		PAGE 2					
SECTION PROPERTIES													
LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	INERTIAS OF PARTS	IYY	STORE
				-							IXX		
0020	C	0.0		-	8	0.37	14.50	0.0	6.87	0.0	0.0	0.0	01
0010	C	0.0		-	8	0.37	0.67	0.0	0.0	0.0	0.0	0.0	
AREA		CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID									
2.56		X Y		X-X Y-Y									
		5.06 7.08		-6.11 28.57									
0040	C	1.0		-	1	7.00	7.00	0.0	0.0	0.0	0.0	0.0	STORE
0030	C	1.0		-	5	2.05	2.05	0.0	0.0	0.0	0.0	0.0	
0070	C	1.0		-	6	2.05	2.05	0.0	7.00	0.0	0.0	0.0	
0060	C	1.0		-	7	2.05	2.05	7.00	7.00	0.0	0.0	0.0	
0050	C	1.0		-	8	2.05	2.05	7.00	0.0	0.0	0.0	0.0	04
AREA		CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID									
40.59		X Y		X-X Y-Y									
		3.50 3.50		91.23 91.23									
0080	C	2.0		-	1	7.00	15.00	0.0	0.0	0.0	0.0	0.0	
0120	C	2.0		-	5	0.33	0.33	0.0	0.0	0.0	0.0	0.0	
0110	C	2.0		-	6	0.33	0.33	0.0	7.00	0.0	0.0	0.0	
0100	C	2.0		-	7	0.33	0.33	15.00	7.00	0.0	0.0	0.0	
0090	C	2.0		-	8	0.33	0.33	15.00	0.0	0.0	0.0	0.0	05
AREA		CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID									
104.78		X Y		X-X Y-Y									
		7.50 3.50		426.08 1956.49									

IDENT 147 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 3

SECTION PROPERTIES

LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	INERTIAS OF PARTS	IXX	IYY	STORE
0170	0	3.0		-	1	7.00	12.71	0.0	0.0	0.0	0.0	0.0	0.0	
0160	0	3.0		-	5	0.82	0.82	0.0	0.0	0.0	0.0	0.0	0.0	
0150	0	3.0		-	6	0.82	0.82	0.0	0.0	0.0	0.0	0.0	0.0	
0140	0	3.0		-	7	0.82	0.82	0.0	0.0	0.0	0.0	0.0	0.0	
0130	0	3.0		-	8	0.82	0.82	0.0	0.0	0.0	0.0	0.0	0.0	C6

AREA	CENTROID LOCATION	MOMENT OF INERTIA ABOUT CENTROID
	X Y	X-X Y-Y
87.63	6.45 3.55	346.42 1142.42

LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	INERTIAS OF PARTS	IXX	IYY	STORE
0200	0	4.0		-	1	7.00	1.42	0.0	0.0	0.0	0.0	0.0	0.0	
0190	0	4.0		-	5	1.74	1.74	0.0	0.0	0.0	0.0	0.0	0.0	
0180	0	4.0		-	6	1.74	1.74	0.0	0.0	0.0	0.0	0.0	0.0	
0220	0	4.0		-	7	1.74	1.74	0.0	0.0	0.0	0.0	0.0	0.0	
0210	0	4.0		-	8	1.74	1.74	0.0	0.0	0.0	0.0	0.0	0.0	07

AREA	CENTROID LOCATION	MOMENT OF INERTIA ABOUT CENTROID
	X Y	X-X Y-Y
52.88	4.69 3.90	154.95 225.55

IDENT 147 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 4

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE	SLAB THICKNESS	INT. GIRDER	STORE
					WIDTH DEPTH	TOP BOTTOM	NO. WEB	
0010	1	0.0	C1	0.0	42.0 7.50	7.62 5.50	3 12.	02

LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG	RT. OVERHANG
TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH EXT. INT.	LENGTH EXT. INT.
0 12. 0.0	0 12. 0.0	4.5 7. 12.	4.5 7. 12.

LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	INERTIAS OF PARTS	IXX	IYY	STORE
				-				5.06	7.08	2.56		-6.11	28.57	

AREA	CENTROID LOCATION	MOMENT OF INERTIA ABOUT CENTROID
	X Y	X-X Y-Y
78.24	20.48 4.38	620.23 10539.61

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE	SLAB THICKNESS	INT. GIRDER	STORE
					WIDTH DEPTH	TOP BOTTOM	NO. WEB	
0020	1	180.0	G2	0.0	0.0 0.0	0.0 0.0	0 0.	

LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG	RT. OVERHANG
TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH EXT. INT.	LENGTH EXT. INT.
0 0. 0.0	0 0. 0.0	0.0 0. 0.	0.0 0. 0.

LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	INERTIAS OF PARTS	IXX	IYY	STORE
				-				20.48	4.38	78.24		620.23	10539.61	

AREA	CENTROID LOCATION	MOMENT OF INERTIA ABOUT CENTROID
	X Y	X-X Y-Y
78.24	20.48 4.38	620.23 10539.61

OUTPUT

Sample Problem 5

IDENT 14T 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 5

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE		
					WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB			
0030	1	200.0	01	0.0	0.0	42.0	7.50	7.62	9.06	3	12.	03	
					LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG		
					TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.
					0	12.	0.0	0	12.	0.0	0.0	0.0	0.0
					INERTIAS OF PARTS								
LINE NO. MEM	LOC	RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
			1				5.06	7.08	2.56	-6.11	28.57		
					CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID						
					X	Y	X-X	Y-Y					
					91.75	20.56	3.72	796.94	15706.22				

MEMBER 1 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
		LT	RT	LT	RT
200.0	620.23	4.041	4.181	0.516	0.499

IDENT 14T 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 6

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE		
					WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB			
0040	2	0.0	03	0.0	0.0	0.0	0.0	0.0	0.0	0	0.		
					LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG		
					TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.
					0	0.	0.0	0	0.	0.0	0.0	0.0	0.
					INERTIAS OF PARTS								
LINE NO. MEM	LOC	RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
			3				20.56	3.72	91.75	796.94	15706.22		
					CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID						
					X	Y	X-X	Y-Y					
					91.75	20.56	3.72	796.94	15706.22				

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE		
					WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB			
0050	2	16.2	02	0.0	0.0	0.0	0.0	0.0	0.0	0	0.		
					LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG		
					TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.
					0	0.	0.0	0	0.	0.0	0.0	0.0	0.
					INERTIAS OF PARTS								
LINE NO. MEM	LOC	RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
			2				20.48	4.38	78.24	620.23	10539.61		
					CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID						
					X	Y	X-X	Y-Y					
					78.24	20.48	4.38	620.23	10539.66				

OUTPUT

Sample Problem 5

IDENT 14T 20 C1 FRAME SYSTEM MAY. 15, 1975 PAGE 7

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
					WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB		
0060	2	142.2	02	0.0	0.0	0.0	0.0	0.0	0.0	0	0.	
			LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG					
			TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.				
			0 0. 0.0	0 0. 0.0	0.0	0. 0.	0.0	0. 0.				
			INERTIAS OF PARTS									
LINE NO. MEM	LOC	RECALL	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
	RECALL	2				20.48	4.38	78.24	620.23	10539.61		
			CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
			AREA	X	Y	X-X	Y-Y					
			78.24	20.48	4.38	620.23	10539.66					

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
					WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB		
0070	2	162.2	03	0.0	0.0	0.0	0.0	0.0	0.0	0	0.	
			LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG					
			TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.				
			0 0. 0.0	0 0. 0.0	0.0	0. 0.	0.0	0. 0.				
			INERTIAS OF PARTS									
LINE NO. MEM	LOC	RECALL	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
	RECALL	3				20.56	3.72	91.75	796.94	15706.22		
			CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
			AREA	X	Y	X-X	Y-Y					
			91.75	20.56	3.72	796.94	15706.29					

IDENT 14T 20 C1 FRAME SYSTEM MAY. 15, 1975 PAGE 8

MEMBER 2 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
		LT	RT	LT	RT
162.2	620.23	4.232	4.262	0.518	0.514

IDENT 14T 20 C1 FRAME SYSTEM MAY. 15, 1975 PAGE 9

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
					WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB		
0080	3	0.0	03	0.0	0.0	0.0	0.0	0.0	0	0.		
			LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG					
			TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.				
			0 0. 0.0	0 0. 0.0	0.0	0. 0.	0.0	0. 0.				
			INERTIAS OF PARTS									
LINE NO. MEM	LOC	RECALL	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
	RECALL	3				20.56	3.72	91.75	796.94	15706.22		
			CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
			AREA	X	Y	X-X	Y-Y					
			91.75	20.56	3.72	796.94	15706.29					

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
					WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB		
0090	3	20.0	02	0.0	0.0	0.0	0.0	0.0	0.0	0	0.	
			LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG					
			TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.				
			0 0. 0.0	0 0. 0.0	0.0	0. 0.	0.0	0. 0.				
			INERTIAS OF PARTS									
LINE NO. MEM	LOC	RECALL	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
	RECALL	2				20.48	4.38	78.24	620.23	10539.61		
			CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
			AREA	X	Y	X-X	Y-Y					
			78.24	20.48	4.38	620.23	10539.66					

OUTPUT

Sample Problem 5

IDENT 14T 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 10

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
0100	3	132.P	02	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB	
					C.C.	0.0	0.0	0.0	0.0	0	0.	
					LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG			
					TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.		
					0 0. 0.0	0 0. 0.0	0.0	0. 0.	0.0	0. 0.		
LINE					INERTIAS OF PARTS							
NO. MEM	LOC	RECALL	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
	RECALL	2				20.48	4.38	78.24	620.23	10539.61		
	AREA	CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
			X	Y	X-X		Y-Y					
	78.24		20.48	4.38	620.23		10539.66					

MEMBER 3 PROPERTIES

HINGE AT LOCATION 112.8		MIN INERTIA	STIFFNESS		CARRY OVER	
LENGTH			LT	RT	LT	RT
132.8		620.23	3.721	0.117	0.177	5.640

IDENT 14T 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 11

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
0110	4	0.0	02	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB	
					0.0	0.0	0.0	0.0	0.0	0	0.	
					LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG			
					TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.		
					0 0. 0.0	0 0. 0.0	0.0	0. 0.	0.0	0. 0.		
LINE					INERTIAS OF PARTS							
NO. MEM	LOC	RECALL	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
	RECALL	2				20.48	4.38	78.24	620.23	10539.61		
	AREA	CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
			X	Y	X-X		Y-Y					
	78.24		20.48	4.38	620.23		10539.66					

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
0120	4	144.2	02	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB	
					0.0	0.0	0.0	0.0	0.0	0	0.	
					LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG			
					TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.		
					0 0. 0.0	0 0. 0.0	0.0	0. 0.	0.0	0. 0.		
LINE					INERTIAS OF PARTS							
NO. MEM	LOC	RECALL	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
	RECALL	3				20.56	3.72	91.75	796.94	15706.22		
	AREA	CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
			X	Y	X-X		Y-Y					
	91.75		20.56	3.72	796.94		15706.29					

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MEMBER 4 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
		LT	RT	LT	RT
144.2	620.23	4.271	4.840	0.532	0.469

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE WIDTH	DEPTH	SLAB THICKNESS TOP	BOTTOM	INT. GIRDER NO.	WEB	STORE	
0130	5	0.0	03	0.0	0.0	0.0	0.0	0.0	0	0.		
					LT. EXT. GIRDER TYPE	WEB FACTOR	RT. EXT. GIRDER TYPE	WEB FACTOR	LT. OVERHANG LENGTH	EXT. INT.	RT. OVERHANG LENGTH	EXT. INT.
					0	0.0	0	0.0	0.0	0.	0.0	0.
LINE NO. MEM	LOC RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
	RECALL 3					20.56	3.72	91.75	756.94	15706.22		
	AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID								
	91.75	X	Y	X-X	Y-Y							
		20.56	3.72	796.94	15706.24							

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE WIDTH	DEPTH	SLAB THICKNESS TOP	BOTTOM	INT. GIRDER NO.	WEB	STORE	
0140	5	18.3	02	0.0	0.0	0.0	0.0	0.0	0	0.		
					LT. EXT. GIRDER TYPE	WEB FACTOR	RT. EXT. GIRDER TYPE	WEB FACTOR	LT. OVERHANG LENGTH	EXT. INT.	RT. OVERHANG LENGTH	EXT. INT.
					0	0.0	0	0.0	0.0	0.	0.0	0.
LINE NO. MEM	LOC RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
	RECALL 2					20.48	4.38	78.24	620.23	10539.61		
	AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID								
	78.24	X	Y	X-X	Y-Y							
		20.48	4.38	620.23	10539.66							

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE WIDTH	DEPTH	SLAB THICKNESS TOP	BOTTOM	INT. GIRDER NO.	WEB	STORE	
0150	5	164.9	02	0.0	0.0	0.0	0.0	0.0	0	0.		
					LT. EXT. GIRDER TYPE	WEB FACTOR	RT. EXT. GIRDER TYPE	WEB FACTOR	LT. OVERHANG LENGTH	EXT. INT.	RT. OVERHANG LENGTH	EXT. INT.
					0	0.0	0	0.0	0.0	0.	0.0	0.
LINE NO. MEM	LOC RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
	RECALL 2					20.48	4.38	78.24	620.23	10539.61		
	AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID								
	78.24	X	Y	X-X	Y-Y							
		20.48	4.38	620.23	10539.66							

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE WIDTH	DEPTH	SLAB THICKNESS TOP	BOTTOM	INT. GIRDER NO.	WEB	STORE	
G160	5	183.2	03	0.0	0.0	0.0	0.0	0.0	0	0.		
					LT. EXT. GIRDER TYPE	WEB FACTOR	RT. EXT. GIRDER TYPE	WEB FACTOR	LT. OVERHANG LENGTH	EXT. INT.	RT. OVERHANG LENGTH	EXT. INT.
					0	0.0	0	0.0	0.0	0.	0.0	0.
LINE NO. MEM	LOC RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
	RECALL 3					20.56	3.72	91.75	796.94	15706.22		
	AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID								
	91.75	X	Y	X-X	Y-Y							
		20.56	3.72	796.94	15706.29							

MEMBER 5 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS LT	RT	CARRY OVER LT	RT
183.2	620.23	4.225	4.225	0.515	0.515

OUTPUT

Sample Problem 5

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SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE	
0170	6	0.0	03	0.0	0.0	WIDTH 0.0	DEPTH 0.0	TOP 0.0	BOTTOM 0.0	NO. WEB 0	G. WEB 0	
			LT. EXT. GIRDER TYPE WEB FACTOR 0 0.0 0.0			RT. EXT. GIRDER TYPE WEB FACTOR 0 0.0 0.0			LT. OVERHANG LENGTH EXT. INT. 0.0 0.0 0.0		RT. OVERHANG LENGTH EXT. INT. 0.0 0.0 0.0	
LINE NO. MEM	LOC RECALL	- CODE	V	H	X	Y	INERTIAS OF PARTS					
	RECALL 3				20.56	3.72	AREA	IXX	IYY	STORE		
AREA			CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID						
91.75			X	Y			X-X	Y-Y				
			20.56	3.72			796.94	15706.22				

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE	
0180	6	142.0	02	0.0	0.0	WIDTH 0.0	DEPTH 0.0	TOP 0.0	BOTTOM 0.0	NO. WEB 0	G. WEB 0	
			LT. EXT. GIRDER TYPE WEB FACTOR 0 0.0 0.0			RT. EXT. GIRDER TYPE WEB FACTOR 0 0.0 0.0			LT. OVERHANG LENGTH EXT. INT. 0.0 0.0 0.0		RT. OVERHANG LENGTH EXT. INT. 0.0 0.0 0.0	
LINE NO. MEM	LOC RECALL	- CODE	V	H	X	Y	INERTIAS OF PARTS					
	RECALL 2				20.48	4.38	AREA	IXX	IYY	STORE		
AREA			CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID						
78.24			X	Y			X-X	Y-Y				
			20.48	4.38			620.23	10539.66				

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MEMBER 6 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
142.0	620.23	LT	RT	LT	RT
		4.840	4.271	0.469	0.532

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SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE	
0190	7	0.0	04	0.0	0.0	WIDTH 0.0	DEPTH 0.0	TOP 0.0	BOTTOM 0.0	NO. WEB 0	G. WEB 0	
			LT. EXT. GIRDER TYPE WEB FACTOR 0 0.0 0.0			RT. EXT. GIRDER TYPE WEB FACTOR 0 0.0 0.0			LT. OVERHANG LENGTH EXT. INT. 0.0 0.0 0.0		RT. OVERHANG LENGTH EXT. INT. 0.0 0.0 0.0	
LINE NO. MEM	LOC RECALL	- CODE	V	H	X	Y	INERTIAS OF PARTS					
	RECALL 4				3.50	3.50	AREA	IXX	IYY	STORE		
AREA			CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID						
40.59			X	Y			X-X	Y-Y				
			3.50	3.50			91.23	91.23				

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE	
0200	7	28.5	04	0.0	0.0	WIDTH 0.0	DEPTH 0.0	TOP 0.0	BOTTOM 0.0	NO. WEB 0	G. WEB 0	
			LT. EXT. GIRDER TYPE WEB FACTOR 0 0.0 0.0			RT. EXT. GIRDER TYPE WEB FACTOR 0 0.0 0.0			LT. OVERHANG LENGTH EXT. INT. 0.0 0.0 0.0		RT. OVERHANG LENGTH EXT. INT. 0.0 0.0 0.0	
LINE NO. MEM	LOC RECALL	- CODE	V	H	X	Y	INERTIAS OF PARTS					
	RECALL 4				3.50	3.50	AREA	IXX	IYY	STORE		
AREA			CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID						
40.59			X	Y			X-X	Y-Y				
			3.50	3.50			91.23	91.23				

OUTPUT

Sample Problem 5

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SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE		
					WIDTH	DEPTH		TOP	BOTTOM	NO.	WEB			
0210	7	33.5	07	0.0	0.0	0.0	0.0	0.0	0.0	0	0.			
			LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG		
			TYPE WEB FACTOR			TYPE WEB FACTOR			LENGTH EXT. INT.			LENGTH EXT. INT.		
			0 0. 0.0			0 0. 0.0			0.0 0. 0.			0.0 0. 0.		
LINE	NO.	MEM	LOC	RECALL	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
				7				4.69	3.90	52.88	154.95	225.55		
		AREA			CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID						
					X	Y	X-X			Y-Y				
		52.88			4.69	3.90	154.95			225.55				

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE		
					WIDTH	DEPTH		TOP	BOTTOM	NO.	WEB			
0220	7	38.5	06	0.0	0.0	0.0	0.0	0.0	0.0	0	0.			
			LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG		
			TYPE WEB FACTOR			TYPE WEB FACTOR			LENGTH EXT. INT.			LENGTH EXT. INT.		
			0 0. 0.0			0 0. 0.0			0.0 0. 0.			0.0 0. 0.		
LINE	NO.	MEM	LOC	RECALL	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
				6				6.45	3.55	87.63	346.42	1142.42		
		AREA			CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID						
					X	Y	X-X			Y-Y				
		87.63			6.45	3.55	346.42			1142.42				

IDENT 14T 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 20

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE		
					WIDTH	DEPTH		TOP	BOTTOM	NO.	WEB			
0230	7	40.5	C5	0.0	0.0	0.0	0.0	0.0	0.0	0	0.			
			LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG		
			TYPE WEB FACTOR			TYPE WEB FACTOR			LENGTH EXT. INT.			LENGTH EXT. INT.		
			0 0. 0.0			0 0. 0.0			0.0 0. 0.			0.0 0. 0.		
LINE	NO.	MEM	LOC	RECALL	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
				5				7.50	3.50	104.78	426.08	1956.49		
		AREA			CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID						
					X	Y	X-X			Y-Y				
		104.78			7.50	3.50	426.08			1956.50				

MEMBER 7 PROPERTIES

WARNING - MEMBER LENGTHS DISAGREE. THAT GIVEN IN FRAME DESCRIPTION IS USED.	LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
			LT	RT	LT	RT
	38.5	91.23	4.487	6.800	0.703	0.464

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SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
					WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB		
0240	B	0.0	04	0.0	0.0	0.0	0.0	0.0	0	0.		
					LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG			
					TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH EXT. INT.	LENGTH EXT. INT.	LENGTH EXT. INT.	LENGTH EXT. INT.		
					0	0.	0.0	0.0	0.	0.	0.	
LINE					INERTIAS OF PARTS							
NO. MEM	LOC	RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE
	RECALL	4					3.50	3.50	40.59	91.23	91.23	
	AREA	CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
			X	Y	X-X	Y-Y						
	40.59		3.50	3.50	91.23	91.23						

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
					WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB		
0250	B	35.0	04	0.0	0.0	0.0	0.0	0.0	0	0.		
					LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG			
					TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH EXT. INT.	LENGTH EXT. INT.	LENGTH EXT. INT.	LENGTH EXT. INT.		
					0	0.	0.0	0.0	0.	0.	0.	
LINE					INERTIAS OF PARTS							
NO. MEM	LOC	RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE
	RECALL	4					3.50	3.50	40.59	91.23	91.23	
	AREA	CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
			X	Y	X-X	Y-Y						
	40.59		3.50	3.50	91.23	91.23						

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SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
					WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB		
0260	E	40.0	07	0.0	0.0	0.0	0.0	0.0	0	0.		
					LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG			
					TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH EXT. INT.	LENGTH EXT. INT.	LENGTH EXT. INT.	LENGTH EXT. INT.		
					0	0.	0.0	0.0	0.	0.	0.	
LINE					INERTIAS OF PARTS							
NO. MEM	LOC	RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE
	RECALL	7					4.69	3.90	52.88	154.95	225.55	
	AREA	CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
			X	Y	X-X	Y-Y						
	52.88		4.69	3.90	154.95	225.55						

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
					WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB		
0270	E	45.0	06	0.0	0.0	0.0	0.0	0.0	0	0.		
					LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG			
					TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH EXT. INT.	LENGTH EXT. INT.	LENGTH EXT. INT.	LENGTH EXT. INT.		
					0	0.	0.0	0.0	0.	0.	0.	
LINE					INERTIAS OF PARTS							
NO. MEM	LOC	RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE
	RECALL	6					6.45	3.55	87.63	346.42	1142.42	
	AREA	CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
			X	Y	X-X	Y-Y						
	87.63		6.45	3.55	346.42	1142.42						

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SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
0280	8	47.0	05	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB	
					0.0	0.0	0.0	0.0	0	0.		
					LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG			RT. OVERHANG		
					TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.
					0	0.	0.0	0.	0.	0.0	0.	0.
LINE					INERTIAS OF PARTS							
NO. MEM	LOC	RECALL	-	CODE	V	H	X	Y	AREA	Ixx	Iyy	STORE
	RECALL	5					7.50	3.50	104.78	426.08	1956.49	
	AREA	CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
			X	Y	X-X	Y-Y						
	104.78		7.50	3.50	426.08	1956.50						

MEMBER 8 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
		LT	RT	LT	RT
47.0	91.23	4.436	6.374	0.679	0.472

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SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
0290	9	0.0	04	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB	
					0.0	0.0	0.0	0.0	0.0	0	0.	
					LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG			RT. OVERHANG		
					TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.
					0	0.	0.0	0.	0.	0.0	0.	0.
LINE					INERTIAS OF PARTS							
NO. MEM	LOC	RECALL	-	CODE	V	H	X	Y	AREA	Ixx	Iyy	STORE
	RECALL	4					3.50	3.50	40.59	91.23	91.23	
	AREA	CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
			X	Y	X-X	Y-Y						
	40.59		3.50	3.50	91.23	91.23						

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE			SLAB THICKNESS		INT. GIRDER		STORE
0300	9	28.0	04	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB	
					0.0	0.0	0.0	0.0	0.0	0	0.	
					LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG			RT. OVERHANG		
					TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.
					0	0.	0.0	0.	0.	0.0	0.	0.
LINE					INERTIAS OF PARTS							
NO. MEM	LOC	RECALL	-	CODE	V	H	X	Y	AREA	Ixx	Iyy	STORE
	RECALL	4					3.50	3.50	40.59	91.23	91.23	
	AREA	CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
			X	Y	X-X	Y-Y						
	40.59		3.50	3.50	91.23	91.23						

OUTPUT

Sample Problem 5

SECTION PROPERTIES

LINE NO.	MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE				
						WIDTH	DEPTH	TOP	BOTTOM	NO.	WER					
0310	9	35.0	C4	0.0	0.0	0.0	0.0	0.0	0.0	0	0.					
				LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG			
				TYPE	WER	FACTOR	TYPE	WER	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.	
				0	0.	0.0	0	0.	0.0	0.0	0.	0.	0.0	0.	0.	
				INERTIAS OF PARTS												
				AREA		IXX		IYY		STORE						
				40.54	3.50		3.50		40.54		91.23		91.23			
				CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID										
				X	Y	X-X		Y-Y								
				3.50	3.50	91.23		91.23								

LINE NO.	MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE				
						WIDTH	DEPTH	TOP	BOTTOM	NO.	WER					
0320	9	38.0	C6	0.0	0.0	0.0	0.0	0.0	0.0	0	0.					
				LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG			
				TYPE	WER	FACTOR	TYPE	WER	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.	
				0	0.	0.0	0	0.	0.0	0.0	0.	0.	0.0	0.	0.	
				INERTIAS OF PARTS												
				AREA		IXX		IYY		STORE						
				87.63	6.45		3.55		87.63		346.42		1142.42			
				CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID										
				X	Y	X-X		Y-Y								
				6.45	3.55	346.42		1142.42								

SECTION PROPERTIES

LINE NO.	MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE				
						WIDTH	DEPTH	TOP	BOTTOM	NO.	WER					
0330	9	40.0	C5	0.0	0.0	0.0	0.0	0.0	0.0	0	0.					
				LT. EXT. GIRDER			RT. EXT. GIRDER			LT. OVERHANG			RT. OVERHANG			
				TYPE	WER	FACTOR	TYPE	WER	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.	
				0	0.	0.0	0	0.	0.0	0.0	0.	0.	0.0	0.	0.	
				INERTIAS OF PARTS												
				AREA		IXX		IYY		STORE						
				104.78	7.50		3.50		104.78		426.08		1956.49			
				CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID										
				X	Y	X-X		Y-Y								
				7.50	3.50	426.08		1956.50								

MEMBER 9 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
		LT	RT	LT	RT
40.0	91.23	4.365	5.940	0.653	0.482

OUTPUT

Sample Problem 5

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SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE
0340	10	0.0	C4	0.0	0.0	0.0	0.0	0.0	0.0	0	0.
					LT. EXT. GIRDER TYPE WFB FACTOR	RT. EXT. GIRDER TYPE WFB FACTOR	LT. OVERHANG LENGTH EXT. INT.	RT. OVERHANG LENGTH EXT. INT.			
					0 0. 0.0	0 0. 0.0	0.0 0. 0.	0.0 0. 0.			
LINE NO. MEM					+		INERTIAS OF PARTS				
	LOC RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE
	RECALL 4					3.50	3.50	40.59	91.23	91.23	
	AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
		X	Y	X-X	Y-Y						
	40.59	3.50	3.50	91.23	91.23						

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE
0350	10	9.0	C4	0.0	0.0	0.0	0.0	0.0	0.0	0	0.
					LT. EXT. GIRDER TYPE WFB FACTOR	RT. EXT. GIRDER TYPE WFB FACTOR	LT. OVERHANG LENGTH EXT. INT.	RT. OVERHANG LENGTH EXT. INT.			
					0 0. 0.0	0 0. 0.0	0.0 0. 0.	0.0 0. 0.			
LINE NO. MEM					+		INERTIAS OF PARTS				
	LOC RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE
	RECALL 4					3.50	3.50	40.59	91.23	91.23	
	AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
		X	Y	X-X	Y-Y						
	40.59	3.50	3.50	91.23	91.23						

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SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE
0360	10	14.0	07	0.0	0.0	0.0	0.0	0.0	0.0	0	0.
					LT. EXT. GIRDER TYPE WFB FACTOR	RT. EXT. GIRDER TYPE WFB FACTOR	LT. OVERHANG LENGTH EXT. INT.	RT. OVERHANG LENGTH EXT. INT.			
					0 0. 0.0	0 0. 0.0	0.0 0. 0.	0.0 0. 0.			
LINE NO. MEM					+		INERTIAS OF PARTS				
	LOC RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE
	RECALL 7					4.69	3.90	52.86	154.95	225.55	
	AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
		X	Y	X-X	Y-Y						
	52.86	4.69	3.90	154.95	225.55						

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE
0370	10	19.0	C6	0.0	0.0	0.0	0.0	0.0	0.0	0	0.
					LT. EXT. GIRDER TYPE WFB FACTOR	RT. EXT. GIRDER TYPE WFB FACTOR	LT. OVERHANG LENGTH EXT. INT.	RT. OVERHANG LENGTH EXT. INT.			
					0 0. 0.0	0 0. 0.0	0.0 0. 0.	0.0 0. 0.			
LINE NO. MEM					+		INERTIAS OF PARTS				
	LOC RECALL	-	CODE	V	H	X	Y	AREA	IXX	IYY	STORE
	RECALL 6					6.45	3.55	87.63	346.42	1142.42	
	AREA	CENTROID LOCATION		MOMENT OF INERTIA ABOUT CENTROID							
		X	Y	X-X	Y-Y						
	87.63	6.45	3.55	346.42	1142.42						

IDENT 14T 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 29

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE					
0380 10	21.0	05	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB						
					0.0	0.0	0.0	0.0	0	0.						
					LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG					
					TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.
					0	0.	0.0	0	0.	0.0	0.0	0.	0.	0.0	0.	0.
LINE NO. MEM	LOC	RECALL	- CODE		V	H	X	Y	INERTIAS OF PARTS			STORE				
									AREA	IXX	IYY					
									104.78	426.08	1956.49					
									MOMENT OF INERTIA ABOUT CENTROID							
									X-X	Y-Y						
									426.08	1956.49						

MEMBER 10 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
21.0	91.23	LT	RT	LT	RT
		4.710	9.655	0.820	0.400

IDENT 14T 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 30

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE					
0390 11	0.0	04	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB						
					0.0	0.0	0.0	0.0	0	0.						
					LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG					
					TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.
					0	0.	0.0	0	0.	0.0	0.0	0.	0.	0.0	0.	0.
LINE NO. MEM	LOC	RECALL	- CODE		V	H	X	Y	INERTIAS OF PARTS			STORE				
									AREA	IXX	IYY					
									40.59	91.23	91.23					
									MOMENT OF INERTIA ABOUT CENTROID							
									X-X	Y-Y						
									91.23	91.23						

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE					
0400 11	8.0	04	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB						
					0.0	0.0	0.0	0.0	0	0.						
					LT. EXT. GIRDER		RT. EXT. GIRDER		LT. OVERHANG		RT. OVERHANG					
					TYPE	WEB	FACTOR	TYPE	WEB	FACTOR	LENGTH	EXT.	INT.	LENGTH	EXT.	INT.
					0	0.	0.0	0	0.	0.0	0.0	0.	0.	0.0	0.	0.
LINE NO. MEM	LOC	RECALL	- CODE		V	H	X	Y	INERTIAS OF PARTS			STORE				
									AREA	IXX	IYY					
									40.59	91.23	91.23					
									MOMENT OF INERTIA ABOUT CENTROID							
									X-X	Y-Y						
									91.23	91.23						

OUTPUT

Sample Problem 5

IDENT 14T 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 31

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE			
0410	11	13.0	07	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB			
				LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG						
				TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.					
				0 0 0.0	0 0 0.0	0.0	0. 0.	0.0	0. 0.					
LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
								4.69	3.90	52.88	154.95	225.55		
				CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
				X	Y	X-X	Y-Y							
				52.88	4.64	3.90	154.95	225.55						

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE			
0420	11	12.0	06	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB			
				LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG						
				TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.					
				0 0 0.0	0 0 0.0	0.0	0. 0.	0.0	0. 0.					
LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
								6.45	3.55	87.63	346.42	1142.42		
				CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
				X	Y	X-X	Y-Y							
				87.63	6.45	3.55	346.42	1142.42						

IDENT 14T 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 32

SECTION PROPERTIES

LINE MEM	LOC	RECALL	X	Y	SUPERSTRUCTURE		SLAB THICKNESS		INT. GIRDER		STORE			
0430	11	20.0	05	0.0	0.0	WIDTH	DEPTH	TOP	BOTTOM	NO.	WEB			
				LT. EXT. GIRDER	RT. EXT. GIRDER	LT. OVERHANG		RT. OVERHANG						
				TYPE WEB FACTOR	TYPE WEB FACTOR	LENGTH	EXT. INT.	LENGTH	EXT. INT.					
				0 0 0.0	0 0 0.0	0.0	0. 0.	0.0	0. 0.					
LINE NO.	MEM	LOC	RECALL	+	CODE	V	H	X	Y	AREA	IXX	IYY	STORE	
								7.50	3.50	104.78	426.08	1956.49		
				CENTROID LOCATION			MOMENT OF INERTIA ABOUT CENTROID							
				X	Y	X-X	Y-Y							
				104.78	7.50	3.50	426.08	1956.50						

MEMBER 11 PROPERTIES

LENGTH	MIN INERTIA	STIFFNESS		CARRY OVER	
		LT	RT	LT	RT
20.0	91.23	4.727	9.913	0.825	0.393

IDENT 14T 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 33

FRAME DIAGNOSTICS

NO ERRORS FOUND

FRAME PROPERTIES

MEM NO	JT LT	JT RT	END COND		DIR	SPAN	I	SUPPORT OR HINGE	E	CARRY OVER FACTORS		DISTRIBUTION FACTORS	
			LT	RT						LT	RT		
1	1	2	R	G	200.0	620.23	0.0	750.	0.516	0.0	0.0	0.230	
2	2	3		G	162.2	620.23	0.0	750.	0.518	0.514	0.386	0.354	
3	3	4		G	132.8	620.23	112.8	750.	0.177	0.640	0.377	0.017	
4	4	5		G	144.2	620.23	0.0	750.	0.532	0.469	0.566	0.270	
5	5	6		G	183.2	620.23	0.0	750.	0.515	0.515	0.186	0.190	
6	6	7	R	G	142.0	620.23	0.0	750.	0.0	0.532	0.210	0.0	
7	8	2			38.5	91.23	7.5	750.	0.703	0.464	0.0	0.384	
8	9	3			47.0	91.23	7.5	750.	0.679	0.472	0.0	0.269	
9	10	4			40.0	91.23	7.5	750.	0.653	0.482	0.0	0.417	
10	11	5			21.0	91.23	7.5	750.	0.820	0.400	0.0	0.544	
11	12	6			20.0	91.23	7.5	750.	0.825	0.393	0.0	0.600	

IDENT 14T 20 01	FRAME SYSTEM	MAY. 15, 1975	PAGE 34
FIXED END MOMENTS TRIAL 0			
MEM NO	FIXED END MOMENTS LT RT	MEM NO	FIXED END MOMENTS LT RT
1	0. -60576.	2	-26746. -26524.
4	-20635. -23548.	5	-33583. -33583.
7	0. 0.	8	0. 0.
10	0. 0.	11	0. 0.
		3	-20028. -12058.
		6	-33474. 0.
		9	0. 0.

IDENT 14T 20 01
 SIDESWAY DIAGNOSTICS
 NO ERRORS FOUND
 MAY. 15, 1975
 PAGE 35

RESULTS OF 1 INCH SWAY TO THE RIGHT

VERTICAL MEMBER	SHEAR (KIPS)	MOMENTS (FT-KIPS) LT	RT	BASED ON E = 3000 KSI
7	717.0	-13325.	14280.	
8	448.5	-9806.	11274.	
9	716.6	-13484.	15180.	
10	4629.0	-44611.	52598.	
11	4826.0	-46064.	50456.	

IDENT 14T 20 01
 FRAME SYSTEM
 MAY. 15, 1975
 PAGE 36

*** SIDESWAY INCLUDED. ***

HORIZONTAL MEMBER MOMENTS TRIAL 0

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	16068.	27443.	34122.	36107.	33398.	25995.	13897.	-2895.	-24381.	-50702.
2	-43713.	-26977.	-13420.	-2951.	4430.	8724.	9930.	8049.	3080.	-4978.	(-45707.)
3	(-34781.)	-10682.	-2531.	3544.	7550.	9486.	9352.	7148.	2875.	-3468.	(-13820.)
4	(-21028.)	-4388.	3374.	6611.	11281.	11343.	8753.	3471.	-4546.	-15341.	(-11880.)
5	(-18071.)	-13817.	-423.	9032.	14548.	16126.	13764.	7464.	-2775.	-16953.	(-10098.)
6	(-14633.)	-17755.	-5391.	4281.	11299.	15707.	17543.	16850.	13668.	8038.	(-25423.)
7	(-12437.)										(-28955.)
8	(-31067.)										(-35187.)
9	(-27646.)										(-31403.)
10	(-32654.)										0.
11	(-28875.)										

HORIZONTAL MEMBER STRESSES TRIAL 0 BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-789.	-1347.	-1675.	-1772.	-1639.	-1276.	-682.	142.	1197.	1480.
2	1288.	1324.	659.	145.	-217.	-428.	-487.	-395.	-151.	225.	447.
3	585.	454.	124.	-174.	-371.	-466.	-459.	-351.	-141.	170.	496.
4	610.	206.	-152.	-372.	-467.	-450.	-333.	-127.	160.	517.	823.
5	895.	678.	21.	-443.	-714.	-791.	-675.	-366.	136.	832.	1017.
6	935.	598.	189.	-156.	-430.	-623.	-726.	-727.	-615.	-378.	-0.

OUTPUT

Sample Problem 5

IDENT 141 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 37

HORIZONTAL MEMBER STRESSES TRIAL 0

MEM NO LEFT .1 PT .2 PT .3 PT .4 PT .5 PT .6 PT .7 PT .8 PT .9 PT RIGHT

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	561.	458.	1191.	1260.	1166.	907.	485.	-101.	-851.	-1107.
2	-1312.	-941.	-468.	-103.	155.	304.	347.	281.	107.	-172.	-456.
3	-596.	-365.	-88.	124.	263.	331.	326.	249.	100.	-121.	-352.
4	-434.	-152.	116.	245.	384.	384.	294.	116.	-151.	-508.	-838.
5	-912.	-482.	-15.	315.	508.	563.	460.	260.	-97.	-592.	-1036.
6	-952.	-588.	-179.	143.	380.	531.	597.	577.	471.	279.	0.

VERTICAL MEMBER MOMENTS TRIAL 0

MEM NO LEFT .1 PT .2 PT .3 PT .4 PT .5 PT .6 PT .7 PT .8 PT .9 PT RIGHT

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
7	-349.	385.	1118.	1852.	2586.	3320.	4054.	4788.	5521.	6255.	6989.
8	4190.	3294.	2398.	1502.	606.	-290.	-1185.	-2081.	-2977.	-3873.	-4769.
9	1103.	717.	332.	-54.	-439.	-825.	-1210.	-1596.	-1981.	-2367.	-2752.
10	73.	-165.	-404.	-642.	-881.	-1119.	-1357.	-1596.	-1834.	-2073.	-2311.
11	-1865.	-1445.	-1026.	-606.	-186.	234.	654.	1073.	1493.	1913.	2333.

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*** SIDESWAY INCLUDED. ***

HORIZONTAL MEMBER SHEARS TRIAL 0

MEM NO LEFT .1 PT .2 PT .3 PT .4 PT .5 PT .6 PT .7 PT .8 PT .9 PT RIGHT

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	920.8	686.1	451.3	216.6	-18.1	-252.8	-487.5	-722.3	-957.0	-1191.7	-1446.7
2	1137.7	931.0	740.6	550.3	359.9	164.5	-20.8	-211.2	-401.5	-592.7	-802.6
3	867.4	693.6	525.4	379.6	223.7	67.8	-88.0	-243.9	-399.7	-555.6	-711.4
4	795.5	624.8	451.2	274.7	95.2	-87.1	-272.4	-460.7	-651.8	-845.9	-1042.9
5	1072.2	838.6	623.6	408.6	193.6	-21.4	-236.4	-451.4	-666.4	-861.4	-1115.0
6	1160.5	966.5	775.4	587.2	401.8	219.4	39.8	-137.0	-310.8	-481.8	-649.9

VERTICAL MEMBER SHEARS TRIAL 0

MEM NO LEFT .1 PT .2 PT .3 PT .4 PT .5 PT .6 PT .7 PT .8 PT .9 PT RIGHT

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
7	190.6	190.6	190.6	190.6	190.6	190.6	190.6	190.6	190.6	190.6	190.6
8	-190.6	-190.6	-190.6	-190.6	-190.6	-190.6	-190.6	-190.6	-190.6	-190.6	-190.6
9	-96.4	-96.4	-96.4	-96.4	-96.4	-96.4	-96.4	-96.4	-96.4	-96.4	-96.4
10	-113.5	-113.5	-113.5	-113.5	-113.5	-113.5	-113.5	-113.5	-113.5	-113.5	-113.5
11	209.9	209.9	209.9	209.9	209.9	209.9	209.9	209.9	209.9	209.9	209.9

IDENT 141 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 39

VERTICAL MEMBER REACTIONS TRIAL 0

MEM NO	LT REACTION	RT REACTION	MEMBER WEIGHT
7	2860.3	2584.4	275.9
8	1999.8	1670.0	329.8
9	1784.0	1507.0	277.9
10	2286.5	2115.0	171.4
11	2440.8	2275.5	165.3

OUTPUT

Sample Problem 5

IDENT 14T 20 G1 FRAME SYSTEM MAY. 14, 1975 PAGE 40

TRIAL 0

TANGENTIAL SPAN	ROTATIONS - RADIANS - COUNTERCLOCKWISE POSITIVE	ROTATIONS - RADIANS - COUNTERCLOCKWISE POSITIVE	SPAN	ROTATIONS - RADIANS - COUNTERCLOCKWISE POSITIVE	ROTATIONS - RADIANS - COUNTERCLOCKWISE POSITIVE	SPAN	ROTATIONS - RADIANS - COUNTERCLOCKWISE POSITIVE	ROTATIONS - RADIANS - COUNTERCLOCKWISE POSITIVE
	LT. END	RT. END		LT. END	RT. END		LT. END	RT. END
1	0.03285	-0.00448	2	-0.00447	-0.00046	3	-0.00046	0.002327
4	0.002327	0.001313	5	0.001314	0.000362	6	0.000362	-0.010125
7	0.000000	-0.00447	8	-0.000000	-0.00046	9	-0.000000	0.002327
10	0.000000	0.001313	11	0.000000	0.000362			

HORIZONTAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END - DOWNWARD POSITIVE

MEMBER	E=	LT	1/4	1/2	3/4	RT	
		0.0	0.043	0.111	0.091	-0.024	
MEMBER 1	E= 750.	0.0		1.424	1.768	0.956	0.0
MEMBER 2	E= 750.	0.0		-0.054	0.118	0.115	0.0
MEMBER 3	E= 750.	0.0		0.057	0.117	0.036	0.0
MEMBER 4	E= 750.	0.0		0.145	0.202	0.090	0.0
MEMBER 5	E= 750.	0.0		0.296	0.502	0.267	0.0
MEMBER 6	E= 750.	0.0		0.165	0.352	0.301	0.0

VERTICAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END.

IDENT 14T 20 G1 FRAME SYSTEM MAY. 15, 1975 PAGE 41

TRIAL 0

MEMBER 7	E= 750.	0.0	-0.001	-0.016	-0.063	-0.144
MEMBER 8	E= 750.	0.0	-0.024	-0.076	-0.123	-0.144
MEMBER 9	E= 750.	0.0	-0.004	-0.009	-0.006	0.012
MEMBER 10	E= 750.	0.0	0.000	0.002	0.005	0.012
MEMBER 11	E= 750.	0.0	0.002	0.006	0.010	0.012

IDENT 14T 20 G1 FRAME SYSTEM MAY. 15, 1975 PAGE 42

LIVE LOAD DIAGNOSTICS

NO ERRORS FOUND

SUPERSTRUCTURE LIVE LOAD

LINE NO.	MEM NO.	NUMBER OF LIVE LOAD LANES				RESISTING MOMENT OF UNIT STEEL		PLOT M & S ENV.	PLOT SCALP	INFLU- ENCF LINES	P13
		LT. END	PT. END	LT. END	RT. END	POSITIVE	NEGATIVE				
0010	1	2.750	2.750	2.7	2.7	0.	0.	0	0	NO	NO
	2	2.750	2.750	2.7	2.7	0.	0.				
	3	2.750	2.750	2.7	2.7	0.	0.				
	4	2.750	2.750	2.7	2.7	0.	0.				
	5	2.750	2.750	2.7	2.7	0.	0.				
	6	2.750	2.750	2.7	2.7	0.	0.				

LIVE LINE LOAD NO.	TRUCK					UNIFORM	LANE MOM. RIDER	SHFAR RIDER	IMPACT	NO. LL LNS.	LIVE LOAD SIDESWAY	COMMENTS
	P1	D1	P2	D2	P3							
1.	8.0	14.0	32.0	14.0	32.0	0.640	18.0	26.0	YES	0.0	NO	H520-44 AASHI LOADING WITHOUT ALTERNATIVE

OUTPUT

Sample Problem 5

IDENT 14T 20 01		FRAME SYSTEM									MAY. 15, 1975		PAGE 43
NEGATIVE LIVE LOAD MOMENT ENVELOPE AND ASSOCIATED SHEARS													
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.	-169.	-378.	-507.	-676.	-845.	-1014.	-1183.	-2492.	-6152.	-11379.		
SHEAR	0.0	-8.5	-8.5	-8.5	-8.5	-8.5	-8.5	-8.5	-71.9	-225.7	-244.2		
2	(-5133.)	-5702.	-3568.	-2912.	-2416.	-2019.	-1623.	-1226.	-1556.	-3416.	-6517.		
SHEAR	(-8326.)	242.2	174.1	26.7	24.5	24.5	24.5	24.5	24.5	-9.9	-154.7		
3	(-5977.)	-3646.	-2325.	-1914.	-1562.	-1214.	-866.	-519.	-171.	-1396.	-4146.		
SHEAR	(-5310.)	202.8	142.6	-11.5	-32.6	-33.1	-33.2	-33.2	-33.3	-33.3	-207.8		
4	(-4414.)	-2244.	-1665.	-1451.	-1402.	-1353.	-1304.	-1255.	-1206.	-3995.	-6652.		
SHEAR	(-3833.)	198.2	39.1	22.8	2.9	2.9	2.9	2.9	2.9	-41.6	-168.2		
5	(-6977.)	-7768.	-3960.	-1505.	-679.	-685.	-699.	-713.	-737.	-1610.	-4113.		
SHEAR	(-6550.)	240.6	177.4	32.6	0.4	-0.8	-0.8	-0.8	-11.8	-35.1	-175.9		
6	(-7336.)	-4354.	-2181.	-1213.	-1040.	-866.	-693.	-520.	-347.	-173.	-242.9		
SHEAR	(-6550.)	225.3	184.5	119.1	12.2	12.2	12.2	12.2	12.2	12.2	0.0		

HORIZONTAL MEMBER STRESSES LL MAX NEG BOTTOM FIBRE											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	8.	17.	25.	33.	41.	50.	58.	122.	302.	330.
2	270.	280.	175.	138.	114.	99.	80.	60.	76.	155.	187.
3	172.	155.	114.	94.	77.	60.	43.	25.	8.	69.	173.
4	167.	105.	75.	63.	58.	54.	50.	46.	71.	135.	196.
5	226.	194.	74.	33.	34.	34.	35.	36.	79.	202.	232.
6	212.	147.	77.	44.	40.	34.	29.	22.	16.	8.	0.

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HORIZONTAL MEMBER STRESSES LL MAX NEG TOP FIBRE													
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT		
1	0.	-6.	-12.	-18.	-24.	-29.	-35.	-41.	-87.	-215.	-343.		
2	-275.	-199.	-125.	-98.	-84.	-70.	-57.	-43.	-54.	-118.	-191.		
3	-175.	-124.	-81.	-67.	-55.	-42.	-30.	-18.	-6.	-49.	-123.		
4	-133.	-78.	-57.	-50.	-48.	-46.	-44.	-42.	-68.	-132.	-201.		
5	-230.	-138.	-53.	-24.	-24.	-24.	-25.	-26.	-56.	-144.	-236.		
6	-216.	-144.	-73.	-41.	-35.	-29.	-24.	-18.	-12.	-6.	0.		

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LL NO. 1. DEAD LOAD PLUS NEGATIVE LIVE LOAD MOMENT ENVELOPE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	15899.	27109.	33615.	35431.	32553.	24981.	12714.	-5387.	-30534.	-62081.
2	-57645. (-48108.)	-32679.	-16988.	-5764.	2014.	6705.	8307.	6823.	1524.	-8394.	(-56094.) -22776.
3	(-27006.) (-23382.)	-14328.	-4854.	1630.	5988.	8272.	8486.	6630.	2704.	-4864.	(-19411.) -16036.
4	(-15047.) (-16189.)	-6653.	1710.	7160.	9879.	9990.	7445.	2216.	-6581.	-19336.	(-13630.) -35607.
5	(-39035.) (-34624.)	-17777.	-1429.	8353.	13863.	15427.	13052.	6727.	-4385.	-21066.	(-31533.) -43151.
6	(-40190.) (-35425.)	-22109.	-7572.	3068.	10260.	14640.	16850.	16330.	13321.	7864.	(-38588.) 0.

HORIZONTAL MEMBER STRESSES FOR DL+LL MAX NEG BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-780.	-1330.	-1650.	-1739.	-1596.	-1220.	-624.	264.	1498.	1816.
2	1558.	1604.	824.	283.	-99.	-324.	-408.	-335.	-75.	380.	628.
3	757.	609.	238.	-60.	-204.	-406.	-416.	-325.	-133.	239.	669.
4	794.	312.	-77.	-309.	-404.	-396.	-284.	-81.	231.	652.	1021.
5	1121.	872.	95.	-410.	-680.	-757.	-641.	-330.	215.	1034.	1249.
6	1147.	745.	266.	-112.	-391.	-489.	-657.	-705.	-600.	-370.	-0.

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HORIZONTAL MEMBER STRESSES FOR DL+LL MAX NEG TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	555.	946.	1173.	1237.	1136.	872.	444.	-188.	-1066.	-1850.
2	-1586.	-1140.	-593.	-201.	70.	234.	290.	238.	53.	-289.	-640.
3	-771.	-489.	-169.	57.	209.	289.	296.	231.	94.	-170.	-476.
4	-565.	-230.	59.	245.	336.	338.	251.	74.	-219.	-641.	-1040.
5	-1142.	-620.	-67.	291.	484.	538.	455.	235.	-153.	-735.	-1272.
6	-1168.	-732.	-252.	103.	345.	502.	573.	559.	459.	273.	0.

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LL NO. 1. POSITIVE LIVE LOAD MOMENT ENVELOPE AND ASSOCIATED SHEARS

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	3859.	6594.	8221.	8767.	8269.	6777.	4372.	2402.	716.	234.
SHEAR	0.0	172.7	124.2	76.1	-28.8	-76.0	-122.5	-161.7	-174.2	-121.0	1.2
2	627.	846.	2360.	3724.	4589.	4836.	4528.	3612.	2227.	1517.	1830.
SHEAR	-14.8	70.9	164.1	136.2	109.8	-83.5	-112.8	-140.9	-166.2	-46.4	33.1
3	1227.	1402.	2213.	3259.	4053.	4341.	4044.	3080.	1247.	169.	500.
SHEAR	-9.3	70.9	107.6	90.5	117.6	-75.2	-107.1	-155.2	-190.2	19.6	19.6
4	675.	1180.	2779.	3411.	4468.	4463.	3458.	2966.	1650.	869.	984.
SHEAR	-15.4	197.1	153.0	124.6	95.3	-97.5	-125.7	-151.7	-174.3	-58.8	14.9
5	709.	823.	1964.	3507.	4547.	4879.	4541.	3495.	1949.	675.	525.
SHEAR	-8.9	64.4	166.9	142.7	112.8	-81.5	-113.1	-143.0	-169.1	-65.9	7.2
6	136.	419.	1487.	2897.	4126.	4971.	5305.	5106.	4228.	2564.	0.
SHEAR	-0.7	71.3	114.3	165.1	143.4	118.3	-73.7	-102.3	-148.9	-180.6	0.0

HORIZONTAL MEMBER STRESSES LL MAX POS BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-189.	-324.	-403.	-430.	-406.	-333.	-215.	-118.	-35.	-8.
2	-20.	-42.	-116.	-183.	-225.	-237.	-222.	-177.	-109.	-69.	-59.
3	-40.	-60.	-109.	-160.	-199.	-213.	-199.	-151.	-61.	-8.	-25.
4	-33.	-55.	-125.	-169.	-185.	-177.	-151.	-108.	-56.	-29.	-32.
5	-23.	-40.	-96.	-172.	-223.	-239.	-223.	-171.	-96.	-33.	-17.
6	-4.	-14.	-52.	-106.	-157.	-197.	-219.	-220.	-190.	-120.	0.

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HORIZONTAL MEMBER STRESSES LL MAX POS TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	135.	230.	287.	306.	289.	237.	153.	84.	25.	8.
2	21.	30.	82.	130.	160.	169.	158.	126.	78.	52.	60.
3	40.	48.	77.	114.	141.	151.	141.	107.	44.	6.	17.
4	24.	41.	96.	134.	152.	151.	133.	99.	55.	29.	32.
5	23.	29.	69.	122.	159.	170.	158.	122.	66.	24.	17.
6	5.	14.	50.	97.	139.	168.	180.	175.	146.	89.	0.

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LL NO. 1. DEAD LOAD PLUS POSITIVE LIVE LOAD MOMENT ENVELOPE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	19928.	34037.	42343.	44874.	41668.	32772.	18270.	-493.	-23665.	-50468. (-45381.)
2	-43086. (-39103.)	-26131.	-11060.	773.	9019.	13559.	14458.	11661.	5307.	-3462.	-14429. (-12264.)
3	-19802. (-16831.)	-9280.	-318.	6802.	11603.	13827.	13401.	10228.	4123.	-3299.	-11380. (-9672.)
4	-13957. (-11663.)	-3208.	6153.	12522.	15749.	15806.	12711.	6437.	-2896.	-14473.	-27471. (-24466.)
5	-30557. (-26412.)	-12994.	1541.	12539.	19095.	21004.	18305.	10959.	-826.	-16278.	-34661. (-30846.)
6	-32717. (-28664.)	-17336.	-3904.	7177.	15426.	20678.	22848.	21956.	17895.	10601.	0.

HORIZONTAL MEMBER STRESSES FOR DL+LL MAX POS BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-978.	-1670.	-2078.	-2202.	-2045.	-1608.	-897.	24.	1161.	1464.
2	1266.	1282.	543.	-38.	-443.	-665.	-710.	-572.	-260.	157.	397.
3	545.	394.	16.	-334.	-569.	-679.	-658.	-502.	-202.	162.	475.
4	582.	151.	-277.	-540.	-652.	-627.	-484.	-235.	102.	488.	792.
5	871.	638.	-76.	-615.	-937.	-1031.	-898.	-538.	41.	799.	999.
6	928.	584.	137.	-262.	-587.	-821.	-945.	-947.	-806.	-498.	-0.

OUTPUT

Sample Problem 5

IDENT	14T 20 01	FRAME SYSTEM									MAY. 15, 1975	PAGE 50
HORIZONTAL MEMBER STRESSES FOR DE*LL MAX POS TOP FIBRE												
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT	
1	0.	695.	1188.	1478.	1566.	1454.	1144.	638.	-17.	-826.	-1497.	
2	-1140.	-912.	-386.	27.	315.	473.	505.	407.	145.	-119.	-404.	
3	-555.	-317.	-11.	237.	405.	483.	468.	357.	144.	-115.	-338.	
4	-414.	-111.	212.	428.	534.	535.	428.	215.	-96.	-479.	-807.	
5	-887.	-453.	54.	438.	666.	733.	639.	382.	-29.	-568.	-1617.	
6	-945.	-574.	-130.	240.	519.	699.	777.	751.	616.	367.	0.	

IDENT	14T 20 01	FRAME SYSTEM									MAY. 15, 1975	PAGE 51
LL NO. 1. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS												
MEMBER	1	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		246.6	147.3	153.4	122.1	94.6	69.5	47.4	28.7	14.1	4.2	1.3
MOMENT		0.0	3304.6	4410.0	7325.0	7566.9	6950.2	5664.4	4022.4	2259.9	-339.1	255.3
NEG. V		-4.3	-20.9	-46.4	-79.0	-106.3	-135.6	-165.2	-204.9	-246.6	-289.2	-332.0
MOMENT		537.1	2280.8	5070.4	6834.0	7481.8	7150.1	7186.0	5074.1	1603.4	-3216.3	-9284.7
RANGE		255.9	218.2	202.3	201.1	202.9	205.1	212.6	233.6	260.7	293.5	333.3

LL NO. 1. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS												
MEMBER	2	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		243.1	245.3	207.9	172.2	135.2	106.8	84.8	64.5	49.2	44.0	43.1
MOMENT		-7318.4	-3410.2	-546.4	1285.6	2204.2	2391.8	2087.2	1564.3	1114.7	2544.1	3149.2
NEG. V		-16.2	-17.1	-27.8	-48.9	-72.2	-100.9	-130.3	-158.9	-188.9	-226.2	-263.7
MOMENT		1341.2	1179.4	2139.4	3372.4	4310.9	4694.1	4435.3	3550.0	1705.9	-1169.0	-5001.3
RANGE		299.3	262.5	235.8	218.1	211.4	210.7	215.1	223.5	238.1	270.2	306.8

LL NO. 1. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS												
MEMBER	3	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		244.0	212.0	186.2	162.5	133.3	101.2	67.2	45.8	28.4	27.6	27.4
MOMENT		-4520.9	-1658.4	1951.0	3186.6	3964.3	4066.6	3397.8	533.0	746.7	1072.6	1436.2
NEG. V		-11.6	-14.8	-2.0	-39.0	-63.1	-91.0	-121.9	-155.2	-190.2	-218.4	-234.7
MOMENT		1349.5	1571.9	2298.0	2844.6	3763.9	4220.4	4038.1	3079.9	1247.5	-761.5	-2566.8
RANGE		255.5	226.8	212.2	201.5	196.3	192.2	189.1	201.0	218.6	245.9	262.2

IDENT	14T 20 01	FRAME SYSTEM									MAY. 15, 1975	PAGE 52
LL NO. 1. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS												
MEMBER	4	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		237.0	200.6	170.1	141.3	112.1	83.8	57.7	40.1	27.6	24.8	24.2
MOMENT		-3195.1	-535.0	2773.3	3861.8	4361.3	4268.2	3654.3	842.7	372.5	1756.1	2043.7
NEG. V		-20.5	-24.3	-37.8	-56.5	-85.0	-114.2	-142.9	-169.8	-196.9	-230.6	-263.9
MOMENT		1301.1	1456.7	2479.2	3488.4	4207.1	4327.2	3877.8	2903.0	894.5	-1834.6	-5307.3
RANGE		257.4	224.9	207.9	197.8	197.0	198.0	200.6	209.9	224.5	255.4	288.1

LL NO. 1. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS												
MEMBER	5	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		277.5	257.0	195.9	161.0	130.4	98.8	68.4	41.2	21.4	11.6	10.4
MOMENT		-6134.6	-1748.9	1370.0	3430.0	4457.6	4737.2	4271.9	3197.9	334.3	-84.0	982.7
NEG. V		-12.3	-13.4	-23.2	-41.4	-68.6	-99.1	-130.7	-161.3	-198.0	-239.1	-279.5
MOMENT		1702.7	1112.3	2142.1	3209.1	4279.2	4738.1	4446.5	3423.9	1832.0	-1672.3	-6303.2
RANGE		289.8	250.4	219.1	202.4	199.1	198.0	199.1	202.4	219.4	250.7	289.9

LL NO. 1. LIVE LOAD SHEAR ENVELOPES AND ASSOCIATED MOMENTS												
MEMBER	6	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		275.2	241.3	208.8	184.5	161.6	135.6	107.1	76.4	44.3	23.8	13.3
MOMENT		-5679.3	-2102.7	754.6	2834.3	4065.0	4866.4	5077.9	4564.4	3222.9	1576.9	510.4
NEG. V		-1.1	-3.9	-12.3	-26.1	-44.1	-65.9	-91.0	-118.8	-148.9	-180.6	-213.3
MOMENT		150.6	496.5	1395.3	2594.3	3760.5	4611.2	5168.6	5061.7	4227.6	2563.6	0.0
RANGE		274.3	245.2	221.1	210.6	205.8	201.6	198.0	195.2	193.2	204.4	226.6

IDENT 14T 20 01		FRAME SYSTEM								MAY. 15, 1975		PAGE 53
LL NO. 1.		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE										
MEMBER	1	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		1167.4	882.4	605.2	328.7	76.5	-183.3	-440.2	-693.5	-942.9	-1187.5	-1445.4
NEG. V		911.6	665.2	403.0	137.6	-126.4	-388.5	-652.7	-927.2	-1203.5	-1480.9	-1778.7

LL NO. 1.		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE										
MEMBER	2	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		1420.9	1176.3	948.5	722.4	499.1	279.4	64.0	-146.6	-352.3	-548.7	-759.5
NEG. V		1121.6	913.8	712.8	504.3	287.7	68.7	-151.1	-370.1	-590.4	-818.9	-1066.3

LL NO. 1.		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE										
MEMBER	3	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		1111.4	905.6	723.6	542.0	357.0	169.1	-20.8	-198.1	-371.3	-528.0	-684.0
NEG. V		855.8	678.7	511.4	340.6	160.6	-23.1	-209.9	-399.1	-589.9	-774.0	-946.1

LL NO. 1.		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE										
MEMBER	4	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		1032.5	825.4	621.3	416.0	207.3	-3.4	-214.8	-420.6	-624.2	-821.1	-1016.7
NEG. V		775.1	600.5	413.5	218.2	10.3	-201.3	-415.3	-630.4	-848.7	-1076.5	-1306.8

IDENT 14T 20 01		FRAME SYSTEM								MAY. 15, 1975		PAGE 54
LL NO. 1.		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE										
MEMBER	5	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		1349.7	1075.6	815.5	568.6	324.0	77.4	-168.1	-410.3	-645.0	-869.8	-1104.6
NEG. V		1059.8	825.2	600.4	367.2	125.0	-120.5	-367.1	-612.7	-864.4	-1120.5	-1394.5

LL NO. 1.		DEAD LOAD PLUS LIVE LOAD SHEAR ENVELOPE										
MEMBER	6	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
POS. V		1433.7	1207.8	964.2	771.7	563.4	355.0	146.8	-60.5	-266.5	-458.0	-636.6
NEG. V		1159.4	962.6	763.1	561.1	357.7	153.4	-51.2	-255.8	-459.7	-662.3	-863.2

IDENT 14T 20 01		FRAME SYSTEM						MAY. 15, 1975		PAGE 55
LL NO. 1.		LIVE LOAD SUPPORT RESULTS								
		MAX. AXIAL LOAD	MAX. AXIAL LOAD		MAX. LONGITUDINAL MOMENT		MAX. AXIAL LOAD	MAX. LONGITUDINAL MOMENT		
			TOP	BOT.	TOP	BOT.		TOP	BOT.	
SUPPORT	JT. 1									
	POSITIVE	246.6	0.	0.	0.0	0.	0.	0.	0.	
	NEGATIVE	-9.3	0.	0.	0.0	0.	0.	0.	0.	
MEMBER	7									
	POSITIVE	552.8	254.1	-1180.	313.2	5357.	-2487.			
	NEGATIVE	-17.4	427.	-198.	211.7	-2829.	1313.			
MEMBER	8									
	POSITIVE	423.7	480.	-227.	227.2	2119.	-1001.			
	NEGATIVE	-54.7	-660.	312.	153.5	-2056.	971.			
MEMBER	9									
	POSITIVE	394.9	115.	-55.	211.9	1988.	-958.			
	NEGATIVE	-43.7	119.	-58.	160.0	-2468.	1189.			
MEMBER	10									
	POSITIVE	458.3	-828.	331.	206.5	3498.	-1600.			
	NEGATIVE	-23.8	-431.	173.	233.1	-5051.	2021.			
MEMBER	11									
	POSITIVE	469.7	624.	-245.	244.9	4938.	-1943.			
	NEGATIVE	-11.4	-429.	169.	225.3	-4608.	1813.			
SUPPORT	JT. 7									
	POSITIVE	213.3	0.	0.	0.0	0.	0.	0.	0.	
	NEGATIVE	-13.3	0.	0.	0.0	0.	0.	0.	0.	

THE RATIO OF SUBSTRUCTURE / SUPERSTRUCTURE LOADING IS 1.000

OUTPUT

Sample Problem 5

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FRAME SYSTEM

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PAGE 56

INPUT PRESTRESS DATA

TRIAL 1 FRAME 1 PATH 1

LINE NO.	MEM NO.	LLT	LLP	LPT	YLT	YLP	YRT	U	K
0010	1	0.0	0.40	0.10	3.00	6.50	1.25	0.25	0.0002
0020	2	0.10	0.50	0.10	1.25	5.00	1.50	0.25	0.0002
0030	3	0.10	0.60	0.0	1.50	4.00	3.00	0.25	0.0002

XLT(FT) = 0.0 XRT(FT) = 20.0 STEEL STRESS(KSI) = 270. JACKING τ = .75 JACKING ENDS = L
 ANCHOR SET(IN): LEFT = 0.625 RIGHT = 0.0 CONC. STRENGTH(Psi) = 3500. ALLOW. TENSION(Psi) = -355.
 P-JACK(KIPS) = 0. SHORTENING PERCENT = 100 TOTAL LOSSES(KSI) = 32

 ***** THE ANSWERS ARE UNCHECKED AND THE USER IS RESPONSIBLE FOR CHECKING THEM. *****

Page 56 - The input prestress data has been printed with any program default values shown. Note the warning! The prestress routines are very complex and unwary users may be able to force a wrong solution from the program.

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CABLE PATH OFFSETS

TRIAL 1 FRAME 1 PATH 1

MEMBER	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	3.00	4.53	5.63	6.28	6.50	6.32	5.80	4.92	3.70	2.12	1.25
2	1.25	2.00	3.31	4.25	4.81	5.00	4.83	4.30	3.43	2.20	1.50
3	1.50	1.92	2.67	3.25	3.67	3.92	4.00	3.84	3.36	0.0	0.0

Page 57 - The input cable path points of inflection have been analyzed, and converted to cable path offsets (in feet from the top of deck) at 10th points of the full span. If no cable path exists at a 10th point, the offset is printed as zero. (see 0.9 point of Span 3).

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CABLE PATH ECCENTRICITIES

TRIAL 1	FRAME 1	PATH 1									
MEMBER	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	-0.117	1.414	2.508	3.164	3.383	3.204	2.683	1.808	0.583	-0.992	-2.534
2	-2.534	-1.117	0.196	1.133	1.696	1.883	1.708	1.183	0.308	-1.043	-2.284
3	-2.284	-1.425	-0.450	0.133	0.550	0.800	0.883	0.722	0.240	0.0	0.0

Page 58 - Locations of the neutral axis and structure depth have been calculated from the section properties input. These values are now combined with the cable path offsets to obtain the eccentricities. A minus sign indicates the cable path is above the neutral axis.

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FORCE COEFFICIENTS

TRIAL 1	FRAME 1	PATH 1									
MEMBER	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.728	0.738	0.747	0.756	0.765	0.772	0.780	0.782	0.774	0.766	0.746
2	0.746	0.727	0.718	0.711	0.703	0.695	0.689	0.682	0.674	0.667	0.650
3	0.650	0.637	0.632	0.628	0.623	0.619	0.614	0.608	0.602	0.0	0.0

THE POINT OF NO MOVEMENT IS IN SPAN 3, 112.80 FEET FROM THE LEFT END OF THE SPAN

THE LEFT ANCHOR SET LENGTH IS 111.

THE RIGHT ANCHOR SET LENGTH IS 0.

THE FORCE COEF. AT THE LEFT END IS 0.728

THE FORCE COEF. AT THE RIGHT END IS 0.598

Page 59 - Friction and wobble losses have been obtained from the cable path offsets and used to calculate the force coefficients. If no cable exists at a 10th point, a value of zero is printed. Since the cable path may not begin or end on an even 10th point, the force coefficients at the cable ends are also shown. Anchor set lengths in feet and the location of the point of no movement of the prestress tendon in its duct are also printed. Error or warning messages may be printed if losses or anchor sets are excessive.

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FRAME SYSTEM

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PAGE 60

SECONDARY MOMENTS

TRIAL 1 FRAME 1 PATH 1

FLM'S DUE TO SECONDARY EFFECTS BEFORE BALANCING

MEMBER	LEFT END	RIGHT END
1	0.0	1.444
2	0.188	0.390
3	-0.316	0.056

DEM'S DUE TO SECONDARY EFFECTS

MEMBER	LEFT END	RIGHT END
1	0.0	1.175
2	0.725	-0.010
3	-0.136	0.024
4	0.013	-0.006
5	-0.001	0.001
6	0.000	0.0

Page 60 - The secondary prestress fixed-end moments and the secondary prestress distributed end moments are printed out mainly to assist users in checking their answers.

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FRAME SYSTEM

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PAGE 61

P/S MOMENT COEF.

TRIAL 1 FRAME 1 PATH 1

*** SIDESWAY INCLUDED. DEAD LOAD WAS SWAYED. ***
ADJUSTED FOR LOSSES & SECONDARY MOMENTS BUT NO SHORTENING

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.0852	-0.9341	-1.6552	-2.0655	-2.1528	-1.9326	-1.4394	-0.6498	0.4216	1.7420	2.9806
2	2.7886	1.6067	0.5495	-0.2197	-0.7108	-0.9327	-0.9050	-0.6394	-0.1455	0.6534	1.3369
3	1.4144	0.8467	0.2315	-0.1285	-0.3793	-0.5233	-0.5627	-0.4516	-0.1484	0.0041	0.0123
4	0.0070	0.0060	0.0050	0.0040	0.0030	0.0020	0.0010	-0.0000	-0.0010	-0.0020	-0.0030
5	-0.0005	-0.0004	-0.0004	-0.0003	-0.0003	-0.0002	-0.0001	-0.0001	-0.0000	0.0000	0.0001
6	0.0002	0.0002	0.0002	0.0002	0.0001	0.0001	0.0001	0.0001	0.0000	0.0000	0.0000

Page 61 - Moment coefficients are obtained by combining the P_e moments with the distributed secondary moments. Losses and sidesway will be included, but prestressed elastic shortening is not included. Note that the effects of prestressing carry over to other frames.

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FEM'S & DELTAS IN COLUMNS DUE TO SHORTENING - PJACK = 1

TRIAL 1 FRAME 1 PATH 1

MEM NO	FEM LT. END	FEM RT. END	DELTA TOP OF COL. (POSITIVE TO RIGHT)
7	-0.258312285	0.336459100	0.000005084
8	0.267569959	-0.337226868	-0.000006056

***** POINT OF NO MOVEMENT IS 62.42 FEET FROM THE LEFT END OF SPAN 2 *****

Page 62 - Deflections and Fixed-end moments due to prestress elastic shortening are printed here. The values shown are always for 100% of the elastic shortening, even if a lesser value was requested. The reduction to less than 100% elastic shortening does not occur until the final prestress moment coefficients are calculated.

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PAGE 63

P/S MOMENT COEF.

TRIAL 1 FRAME 1 PATH 1

ADJUSTED FOR LOSSES & SECONDARY MOMENTS & SHORTENING

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.0052	-0.9436	-1.6741	-2.0939	-2.1907	-1.9799	-1.4961	-0.7160	0.3459	1.6569	2.8860
2	2.8707	1.6871	0.6285	-0.1422	-0.6347	-0.8580	-0.8318	-0.5676	-0.0751	0.7224	1.4045
3	1.2574	0.7082	0.1115	-0.2301	-0.4624	-0.5879	-0.6088	-0.4792	-0.1575	0.0135	0.0402
4	0.0228	0.0195	0.0162	0.0130	0.0097	0.0064	0.0032	-0.0001	-0.0034	-0.0066	-0.0095
5	-0.0016	-0.0014	-0.0013	-0.0011	-0.0009	-0.0007	-0.0005	-0.0003	-0.0001	0.0001	0.0003
6	0.0008	0.0007	0.0006	0.0005	0.0005	0.0004	0.0003	0.0002	0.0002	0.0001	0.0000

Page 63 - These prestressed moment coefficients are the final coefficients with all losses, including the input percent of elastic shortening. These are the values used to determine the prestress force and the prestress moments, shears, stresses, and reactions.

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FRAME SYSTEM

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TRIAL 1 FRAME 1 PATH 1

HORIZONTAL MEMBER STRESSES PRESTRESS ONLY BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	637.	1177.	1563.	1789.	1847.	1745.	1502.	1101.	545.	-140.	-390.
2	-384.	-152.	247.	738.	985.	1093.	1073.	930.	669.	260.	39.
3	89.	246.	533.	705.	821.	882.	889.	816.	644.	-7.	-21.
4	-12.	-10.	-8.	-6.	-4.	-3.	-1.	0.	1.	2.	3.
5	1.	1.	1.	1.	0.	0.	0.	0.	0.	-0.	-0.
6	-0.	-0.	-0.	-0.	-0.	-0.	-0.	-0.	-0.	-0.	-0.

HORIZONTAL MEMBER STRESSES PRESTRESS ONLY TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	712.	343.	63.	-63.	-90.	-6.	180.	468.	850.	1325.	1596.
2	1591.	1259.	902.	612.	424.	334.	338.	428.	603.	866.	1005.
3	954.	818.	632.	502.	412.	362.	350.	392.	504.	5.	15.
4	6.	7.	6.	5.	3.	2.	1.	-0.	-1.	-2.	-3.
5	-1.	-1.	-0.	-0.	-0.	-0.	-0.	-0.	-0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

Page 64 - All information is now available to obtain the prestress jacking force. This force is calculated and stressed are obtained and printed here.

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TRIAL 1 FRAME 1 PATH 1

HORIZONTAL MEMBER STRESSES DL + P/S FOR BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	637.	388.	216.	114.	75.	106.	227.	419.	687.	1056.	1090.
2	404.	1132.	1005.	882.	767.	665.	586.	535.	518.	485.	486.
3	674.	700.	657.	532.	451.	416.	430.	465.	503.	163.	475.
4	599.	147.	-160.	-377.	-471.	-453.	-335.	-127.	161.	519.	827.
5	896.	679.	21.	-443.	-714.	-791.	-675.	-366.	136.	832.	1017.
6	435.	598.	189.	-157.	-430.	-623.	-726.	-727.	-615.	-378.	-0.

HORIZONTAL MEMBER STRESSES DL + P/S FOR TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	712.	903.	1041.	1128.	1170.	1160.	1087.	953.	749.	474.	89.
2	279.	358.	434.	509.	578.	639.	685.	709.	710.	694.	550.
3	358.	453.	543.	626.	676.	693.	677.	642.	605.	-116.	-338.
4	-426.	-145.	122.	299.	387.	386.	296.	116.	-153.	-511.	-842.
5	-412.	-483.	-15.	315.	507.	563.	480.	260.	-97.	-592.	-1035.
6	-452.	-568.	-179.	143.	380.	531.	597.	577.	471.	279.	0.

Pages 65, 66, 67, and 68 - Stresses due to the various load combinations are calculated and printed. The MIN PJACK is designed so that the combined DL + ADDED DL + LL + I + P/S stresses sum up to the allowable tension. Then the DL + P/S stresses and the DL + ADDED DL + P/S stresses are checked to see that zero tension is not exceeded. The critical location of PJACK design is found on Page 67 at the 0.4 point of Span 1, bottom fiber stress. The stress here is at the maximum tension allowable of -355 KSI.

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TRIAL 1 FRAME 1 PATH 1

HORIZONTAL MEMBER STRESSES DL + ADDED DL + P/S FOR BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	637.	388.	216.	114.	75.	106.	227.	419.	687.	1056.	1090.
2	404.	1132.	1005.	882.	767.	665.	586.	535.	518.	485.	486.
3	674.	700.	657.	532.	451.	416.	430.	465.	503.	163.	475.
4	599.	147.	-160.	-377.	-471.	-453.	-335.	-127.	161.	519.	827.
5	896.	679.	21.	-443.	-714.	-791.	-675.	-366.	136.	832.	1017.
6	435.	598.	189.	-157.	-430.	-623.	-726.	-727.	-615.	-378.	-0.

HORIZONTAL MEMBER STRESSES DL + ADDED DL + P/S FOR TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	712.	903.	1041.	1128.	1170.	1160.	1087.	953.	749.	474.	89.
2	279.	358.	434.	509.	578.	639.	685.	709.	710.	694.	550.
3	358.	453.	543.	626.	676.	693.	677.	642.	605.	-116.	-338.
4	-426.	-145.	122.	299.	387.	386.	296.	116.	-153.	-511.	-842.
5	-412.	-483.	-15.	315.	507.	563.	480.	260.	-97.	-592.	-1035.
6	-452.	-568.	-179.	143.	380.	531.	597.	577.	471.	279.	0.

OUTPUT

Sample Problem 5

IDENT 14T 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 67

TRIAL 1 FRAME 1 PATH 1

HORIZONTAL MEMBER STRESSES DL + ADDED DL + MAX POS LL + I + P/S BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	637.	199.	-107.	-289.	-385.	-300.	-106.	204.	564.	1021.	1080.
2	882.	1040.	889.	700.	542.	427.	364.	358.	404.	416.	436.
3	634.	641.	549.	372.	252.	203.	231.	314.	441.	155.	454.
4	570.	141.	-265.	-546.	-656.	-630.	-485.	-235.	103.	490.	796.
5	872.	638.	-75.	-615.	-937.	-1030.	-898.	-538.	41.	799.	999.
6	428.	584.	137.	-263.	-588.	-821.	-945.	-947.	-806.	-498.	-0.

HORIZONTAL MEMBER STRESSES DL + ADDED DL + MAX POS LL + I + P/S TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	712.	1038.	1271.	1415.	1476.	1449.	1323.	1105.	833.	499.	100.
2	301.	387.	516.	639.	738.	807.	843.	835.	788.	747.	601.
3	599.	501.	621.	739.	817.	845.	818.	749.	648.	-110.	-323.
4	-406.	-104.	218.	433.	539.	537.	429.	215.	-98.	-482.	-810.
5	-888.	-454.	53.	437.	666.	733.	639.	382.	-29.	-568.	-1017.
6	-945.	-574.	-130.	240.	519.	699.	777.	751.	616.	367.	0.

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TRIAL 1 FRAME 1 PATH 1

HORIZONTAL MEMBER STRESSES DL + ADDED DL + MAX NEG LL + I + P/S BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	637.	397.	233.	139.	108.	147.	276.	477.	809.	1358.	1426.
2	1173.	1411.	1160.	1020.	886.	764.	666.	595.	594.	639.	667.
3	846.	855.	771.	625.	527.	476.	472.	491.	511.	232.	648.
4	783.	302.	-85.	-315.	-413.	-394.	-285.	-81.	232.	654.	1024.
5	1122.	873.	95.	-409.	-680.	-757.	-640.	-330.	215.	1034.	1249.
6	1147.	745.	266.	-112.	-391.	-589.	-697.	-705.	-600.	-370.	-0.

HORIZONTAL MEMBER STRESSES DL + ADDED DL + MAX NEG LL + I + P/S FOR TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	712.	898.	1029.	1110.	1147.	1130.	1051.	911.	662.	259.	-254.
2	4.	159.	309.	411.	494.	566.	628.	666.	656.	577.	365.
3	183.	328.	462.	559.	621.	651.	646.	624.	599.	-165.	-461.
4	-557.	-123.	65.	250.	339.	340.	252.	74.	-220.	-643.	-1043.
5	-1142.	-621.	-68.	291.	484.	538.	455.	235.	-153.	-735.	-1272.
6	-1166.	-732.	-252.	103.	345.	502.	573.	559.	459.	273.	0.

**** MIN PJACK = 10529. KIPS CONC STRENGTH @ 28 DAYS = 3691. PSI @ STRESSING = 2128. PSI ****

Page 68 - The value of the required PJACK and the required concrete strength is shown here.

TRIAL 1 FRAME 1 PATH 1

HORIZONTAL MEMBER MOMENTS DUE TO P/S

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	197.	-9435.	-17627.	-22047.	-23066.	-20847.	-15753.	-7539.	3642.	17446.	30388.
2	50226.	17764.	6618.	-1497.	-6683.	-9034.	-8758.	-5976.	-791.	7606.	14788.
3	13240.	7457.	1174.	-2422.	-4869.	-6190.	-6411.	-5046.	-1659.	142.	423.
4	240.	205.	171.	137.	102.	68.	33.	-1.	-36.	-70.	-104.
5	-17.	-15.	-13.	-11.	-9.	-7.	-5.	-3.	-1.	1.	3.
6	8.	7.	7.	6.	5.	4.	3.	2.	2.	1.	0.

VERTICAL MEMBER MOMENTS DUE TO P/S

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
7	-2268.	-2057.	-1847.	-1636.	-1426.	-1215.	-1004.	-794.	-583.	-372.	-162.
8	1023.	766.	509.	252.	-5.	-263.	-520.	-777.	-1034.	-1291.	-1548.
9	87.	60.	33.	6.	-21.	-48.	-75.	-102.	-129.	-156.	-183.
10	-41.	-26.	-15.	-2.	10.	23.	36.	49.	62.	74.	87.
11	-8.	-7.	-6.	-4.	-3.	-2.	-1.	1.	2.	3.	5.

Page 69 - Moments in all members due to prestress are printed here. The prestressing effects in other frames is also shown.

TRIAL 1 FRAME 1 PATH 1

TANGENTIAL ROTATIONS - RADIANS - CLOCKWISE	SPAN	LT. END	RT. END	SPAN	LT. END	RT. END	SPAN	LT. END	RT. END
1	-0.00067	0.004579	2	0.004579	0.000478	3	0.000478	0.000128	
4	0.000128	-0.000014	5	-0.000014	0.000005	6	0.000005	-0.000003	
7	-0.000003	0.001454	8	0.000462	0.000940	9	-0.000002	0.000126	
10	-0.000004	-0.000018	11	-0.000004	0.000001				

HORIZONTAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END - DOWNWARD POSITIVE

MEMBER	E = 750.	0.0	-0.888	-1.085	-0.561	0.0
MEMBER 2	E = 750.	0.0	-0.042	-0.173	-0.116	0.0
MEMBER 3	E = 750.	0.0	-0.045	-0.090	-0.043	0.0
LONG HINGE	LT	1/4	1/2	3/4	RT	
	0.0	-0.034	-0.084	-0.076	-0.003	
MEMBER 4	E = 750.	0.0	0.003	0.002	0.001	0.0
MEMBER 5	E = 750.	0.0	-0.000	-0.000	-0.000	0.0
MEMBER 6	E = 750.	0.0	0.000	0.000	0.000	0.0

VERTICAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END.

Pages 70-71 - Deflections and rotations due to prestressing only are printed here. This completes the output for a given Trial, Frame, and Path.

OUTPUT

Sample Problem 5

IDENT	14T 20 01	FRAME SYSTEM						MAY. 15, 1975	PAGE 71
TRIAL	1	FRAME 1	PATH 1						
MEMBER	7	E=	750.	0.0	-0.010	-0.022	-0.014	0.0	
MEMBER	8	E=	750.	0.0	-0.000	-0.006	-0.008	0.0	
MEMBER	9	E=	750.	0.0	-0.000	-0.001	-0.001	0.0	
MEMBER	10	E=	750.	0.0	0.000	0.000	0.000	0.0	
MEMBER	11	E=	750.	0.0	-0.000	-0.000	-0.000	0.0	

IDENT	14T 20 01	FRAME SYSTEM						MAY. 15, 1975	PAGE 72
INPUT PRESTRESSED DATA									
TRIAL	1	FRAME 2	PATH 1						
LINE NO.	MEM NO.	LLT	LLP	LRT	YLT	YLP	YRT	U	K
0040	3	0.0	0.0	0.0	2.75	0.0	1.50	0.25	0.0002
0050	4	0.10	0.50	0.10	1.50	5.00	1.25	0.25	0.0002
0060	5	0.10	0.50	0.10	1.25	6.50	1.25	0.25	0.0002
0070	6	0.10	0.60	0.0	1.25	5.00	3.00	0.25	0.0002

XLT(FT) = 112.0 XRT(FT) = 0.0 STEEL STRESS(KSI) = 270. JACKING % = .75 JACKING ENDS = B
 ANCHOR SFT(IN); LEFT = 0.625 RIGHT = 0.625 CONC. STRENGTH(PST) = 3500. ALLOW. TENSION(PST) = -355.
 P-JACK(KIPS) = 0. SHORTENING PERCENT = 100 TOTAL LOSSES(KSI) = 32

 ***** THE ANSWERS ARE UNCHECKED AND THE USER IS RESPONSIBLE FOR CHECKING THEM. *****

Pages 72 thru 87 - The output for Frame 2 is basically the same as the output for Frame 1. Page 84 contains a note warning the user that the initial condition controlled design. This means that the maximum allowable tension stress of -355 KSI will not appear, but a value of zero will appear in the initial stresses. This zero stress shows on Page 81, top fiber stresses, left end of member six.

IDENT	14T 20 01	FRAME SYSTEM						MAY. 15, 1975	PAGE 73		
CABLE PATH OFFSETS											
TRIAL	1	FRAME 2	PATH 1								
MEMBER	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.05	1.50
4	1.50	2.20	3.42	4.30	4.82	5.00	4.81	4.25	3.31	2.00	1.25
5	1.25	2.30	4.14	5.45	6.24	6.50	6.24	5.45	4.14	2.30	1.25
6	1.25	1.88	3.00	3.87	4.50	4.87	5.00	4.88	4.50	3.88	3.00

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CABLE PATH ECCENTRICITIES

MEMBER	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-1.066	-1.617
4	-1.617	-0.984	0.175	0.983	1.441	1.549	1.295	0.666	-0.338	-1.718	-2.534
5	-2.534	-0.817	1.021	2.333	3.121	3.383	3.121	2.333	1.021	-0.817	-2.534
6	-2.534	-1.843	-0.651	0.291	0.983	1.424	1.616	1.558	1.250	0.691	-0.117

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FORCE COEFFICIENTS

MEMBER	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.661	0.684
4	0.684	0.714	0.713	0.722	0.730	0.738	0.741	0.733	0.725	0.716	0.695
5	0.695	0.673	0.672	0.681	0.690	0.698	0.707	0.716	0.726	0.736	0.760
6	0.760	0.780	0.778	0.771	0.764	0.757	0.751	0.744	0.737	0.730	0.722

THE POINT OF NO MOVEMENT IS IN SPAN 5, 28.30 FEET FROM THE LEFT END OF THE SPAN

THE LEFT ANCHOR SET LENGTH IS 152.

THE RIGHT ANCHOR SET LENGTH IS 93.

THE FORCE COEFF. AT THE LEFT END IS 0.644

THE FORCE COEFF. AT THE RIGHT END IS 0.722

IDENT 147 20 01 FRAME SYSTEM MAY. 15, 1975 PAGE 76

SECONDARY MOMENTS

MEMBER	LEFT END	RIGHT END
3	0.047	-0.008
4	0.311	-0.136
5	0.908	0.891
6	-0.049	0.0

FEM'S DUE TO SECONDARY EFFECTS BEFORE BALANCING

MEMBER	LEFT END	RIGHT END
1	0.0	-0.001
2	-0.004	0.010
3	0.018	-0.003
4	0.071	0.213
5	0.808	0.797
6	0.171	0.0

DFM'S DUE TO SECONDARY EFFECTS

OUTPUT

Sample Problem 5

IDENT 14T 20 C1

FRAME SYSTEM

MAY. 15, 1975

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P/S MOMENT COEF.

TRIAL 1 FRAME 2 PATH 1

*** SIDESWAY INCLUDED. DEAD LOAD WAS SWAYED. ***
ADJUSTED FOR LOSSES & SECONDARY MOMENTS BUT NO SHORTENING

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.0	-0.0001	-0.0001	-0.0002	-0.0002	-0.0003	-0.0004	-0.0004	-0.0005	-0.0005	-0.0006
2	-0.0050	-0.0034	-0.0018	-0.0002	0.0015	0.0031	0.0047	0.0063	0.0079	0.0095	0.0112
3	0.0179	0.0158	0.0137	0.0116	0.0095	0.0074	0.0052	0.0031	0.0010	0.7036	1.1026
4	1.1788	0.7795	-0.0242	-0.5954	-0.9243	-1.0023	-0.8051	-0.3195	0.4273	1.4261	1.9704
5	2.5718	1.3592	0.1218	-0.7828	-1.3491	-1.5580	-1.4056	-0.8725	0.0565	1.3972	2.7200
6	2.0496	1.5434	0.6457	-0.1026	-0.6464	-0.9913	-1.1442	-1.1068	-0.8860	-0.4871	0.0845

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FRAME SYSTEM

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FEMMS & DELTAS IN COLUMNS DUE TO SHORTENING - PJACK = 1

TRIAL 1 FRAME 2 PATH 1

MEM NO	FEM LT. END	FEM RT. END	DELTA TOP OF COL. (POSITIVE TO RIGHT)
9	-0.764239132	0.928301811	0.000017126
10	-1.106619835	1.744941711	0.000005777
11	1.954242821	-3.137096405	-0.000009219

***** POINT OF NO MOVEMENT IS 76.46 FEET FROM THE LEFT END OF SPAN 5 *****

IDENT 14T 20 C1

FRAME SYSTEM

MAY. 15, 1975

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P/S MOMENT COEF.

TRIAL 1 FRAME 2 PATH 1

ADJUSTED FOR LOSSES & SECONDARY MOMENTS & SHORTENING

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.0	-0.0002	-0.0004	-0.0006	-0.0008	-0.0010	-0.0011	-0.0013	-0.0015	-0.0017	-0.0019
2	-0.0161	-0.0109	-0.0057	-0.0005	0.0047	0.0099	0.0151	0.0203	0.0255	0.0307	0.0359
3	0.0575	0.0507	0.0440	0.0372	0.0304	0.0237	0.0169	0.0101	0.0033	0.7012	1.0950
4	1.1234	1.2933	0.3487	-0.3633	-0.8331	-1.0519	-0.9956	-0.6508	-0.0449	0.8130	1.2165
5	2.6360	1.4575	0.2542	-0.6162	-1.1484	-1.3232	-1.1366	-0.5694	0.3936	1.7685	3.1253
6	1.4376	0.9976	0.1156	-0.5660	-1.0436	-1.3223	-1.4090	-1.3054	-1.0184	-0.5533	0.0845

IDENT 14T 20 C1

FRAME SYSTEM

MAY. 15, 1975

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TRIAL 1 FRAME 2 PATH 1

HORIZONTAL MEMBER STRESSES PRESTRESS ONLY BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	0.	0.	0.	0.	0.	1.	1.	1.	1.	1.
2	5.	5.	3.	0.	-2.	-4.	-7.	-9.	-11.	-13.	-11.
3	-17.	-20.	-20.	-17.	-14.	-11.	-8.	-5.	-1.	220.	63.
4	-266.	6.	413.	695.	863.	926.	865.	743.	527.	251.	120.
5	-297.	-107.	428.	823.	1067.	1151.	1076.	831.	409.	-194.	-396.
6	100.	239.	514.	742.	918.	1037.	1095.	1081.	990.	814.	544.

HORIZONTAL MEMBER STRESSES PRESTRESS ONLY TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-0.	-0.	-0.	-0.	-0.	-0.	-0.	-0.	-1.	-1.
2	-6.	-3.	-2.	-0.	1.	3.	5.	6.	8.	10.	11.
3	17.	16.	14.	12.	10.	7.	5.	3.	1.	755.	898.
4	1131.	964.	664.	440.	293.	224.	237.	329.	499.	744.	841.
5	1266.	1004.	622.	353.	192.	143.	209.	397.	709.	1153.	1457.
6	952.	844.	585.	382.	239.	155.	131.	164.	255.	464.	609.

IDENT 14T 20 C1

FRAME SYSTEM

MAY. 15, 1975

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TRIAL 1 FRAME 2 PATH 1

HORIZONTAL MEMBER STRESSES DL + P/S FOR BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	637.	308.	217.	114.	76.	106.	227.	419.	687.	1057.	1091.
2	908.	1136.	1008.	883.	765.	660.	579.	526.	506.	472.	476.
3	657.	681.	638.	515.	437.	406.	422.	461.	501.	383.	538.
4	333.	203.	253.	318.	392.	473.	550.	616.	686.	770.	946.
5	598.	572.	449.	380.	354.	360.	400.	464.	546.	637.	620.
6	1034.	837.	703.	585.	488.	414.	369.	354.	374.	436.	544.

HORIZONTAL MEMBER STRESSES DL + P/S FOR TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	712.	903.	1041.	1128.	1170.	1160.	1086.	952.	749.	473.	88.
2	274.	354.	432.	509.	580.	642.	689.	716.	718.	704.	560.
3	376.	469.	557.	638.	686.	701.	682.	645.	606.	639.	560.
4	706.	819.	786.	739.	680.	610.	533.	445.	347.	233.	-0.
5	354.	521.	606.	668.	699.	705.	690.	657.	613.	562.	422.
6	0.	256.	406.	526.	619.	687.	728.	741.	726.	682.	609.

OUTPUT

Sample Problem 5

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TRIAL 1 FRAME 2 PATH 1

HORIZONTAL MEMBER STRESSES DL + ADDED DL + P/S FOR BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	637.	388.	217.	114.	76.	106.	227.	419.	687.	1057.	1091.
2	908.	1136.	1006.	883.	765.	660.	576.	526.	506.	472.	476.
3	657.	681.	638.	515.	437.	406.	422.	461.	501.	383.	538.
4	353.	203.	253.	318.	392.	473.	550.	616.	686.	770.	946.
5	598.	572.	449.	380.	354.	360.	400.	464.	546.	637.	620.
6	1034.	837.	703.	585.	468.	414.	369.	354.	374.	436.	544.

HORIZONTAL MEMBER STRESSES DL + ADDED DL + P/S FOR TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	712.	903.	1041.	1128.	1170.	1160.	1086.	952.	745.	473.	88.
2	274.	354.	432.	509.	580.	642.	689.	716.	718.	704.	560.
3	376.	469.	557.	638.	686.	701.	682.	645.	606.	639.	560.
4	706.	819.	786.	739.	680.	610.	533.	445.	347.	233.	-0.
5	354.	521.	606.	668.	699.	705.	690.	657.	613.	562.	422.
6	0.	256.	406.	526.	619.	687.	728.	741.	726.	682.	609.

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TRIAL 1 FRAME 2 PATH 1

HORIZONTAL MEMBER STRESSES DL + ADDED DL + MAX POS LL + I + P/S BOTTOM FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	637.	199.	-107.	-289.	-355.	-249.	-105.	205.	569.	1022.	1080.
2	886.	1095.	892.	700.	540.	423.	357.	349.	397.	404.	425.
3	617.	621.	624.	355.	238.	193.	223.	310.	440.	375.	517.
4	305.	147.	128.	149.	207.	296.	400.	507.	630.	741.	915.
5	575.	532.	353.	208.	131.	121.	178.	293.	450.	604.	602.
6	1027.	823.	650.	479.	331.	217.	149.	133.	184.	316.	544.

HORIZONTAL MEMBER STRESSES DL + ADDED DL + MAX POS LL + I + P/S TOP FIBRE

MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	712.	1038.	1271.	1415.	1476.	1448.	1323.	1105.	833.	498.	99.
2	297.	384.	515.	639.	740.	811.	847.	842.	796.	756.	612.
3	416.	517.	635.	751.	827.	852.	823.	753.	649.	644.	575.
4	726.	860.	882.	873.	832.	761.	666.	544.	402.	262.	31.
5	378.	550.	675.	790.	858.	876.	848.	779.	681.	585.	440.
6	7.	270.	456.	622.	758.	855.	908.	916.	872.	771.	609.

OUTPUT

Sample Problem 5

IDENT	14T 20 01	FRAME SYSTEM	MAY. 15, 1975	PAGE	64						
TRIAL	1	FRAME 1	PATH 1								
HORIZONTAL MEMBER STRESSES DL + ADDED DL + MAX NEG LL + I + P/S BOTTOM FIBRE											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	637.	347.	233.	139.	109.	148.	277.	477.	810.	1359.	1427.
2	1178.	1416.	1183.	1021.	884.	759.	659.	586.	583.	627.	657.
3	829.	835.	752.	609.	514.	465.	465.	486.	510.	452.	711.
4	517.	308.	328.	380.	450.	527.	600.	662.	759.	905.	1144.
5	824.	766.	523.	413.	387.	395.	435.	501.	625.	839.	852.
6	1246.	984.	774.	629.	527.	448.	398.	376.	390.	444.	544.
HORIZONTAL MEMBER STRESSES DL + ADDED DL + MAX NEG LL + I + P/S FOR TOP FIBRE											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	712.	897.	1029.	1110.	1147.	1130.	1051.	911.	662.	259.	-254.
2	-0.	155.	308.	410.	495.	571.	633.	673.	664.	586.	376.
3	200.	344.	476.	571.	631.	658.	652.	627.	600.	590.	437.
4	+75.	742.	729.	690.	632.	565.	489.	403.	279.	101.	-202.
5	124.	383.	554.	644.	676.	681.	665.	631.	556.	418.	186.
6	-216.	111.	333.	485.	584.	657.	704.	723.	714.	676.	609.

**** MIN P/JACK = 9075. KIPS CONC STRENGTH @ 28 DAYS = 3116. PSI @ STRESSING = 1880. PSI ****

**** REDSIGN HAS TAKEN PLACE FOR P/JACK TO ELIMINATE TENSION UNDER (DL + ADDED DL + P/S) CONDITION.
 **** POINT OF CONTROL CAN BE FOUND UNDER (DL + ADDED DL + P/S) STRESSES.

IDENT	14T 20 01	FRAME SYSTEM	MAY. 15, 1975	PAGE	85						
TRIAL	1	FRAME 2	PATH 1								
HORIZONTAL MEMBER MOMENTS DUE TO P/S											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
1	0.	-2.	-3.	-5.	-7.	-9.	-10.	-12.	-14.	-16.	-17.
2	-146.	-99.	-52.	-5.	43.	90.	137.	184.	232.	279.	326.
3	522.	460.	355.	338.	276.	215.	153.	92.	30.	6363.	9942.
4	16639.	11736.	3164.	-3297.	-7560.	-9546.	-9035.	-5906.	-407.	7378.	11039.
5	23421.	13227.	2307.	-5592.	-10422.	-12006.	-10315.	-5167.	3572.	16049.	28362.
6	13046.	9054.	1049.	-5136.	-9471.	-12000.	-12787.	-11847.	-9242.	-5021.	767.
VERTICAL MEMBER MOMENTS DUE TO P/S											
MEM NO	LEFT	.1 PT	.2 PT	.3 PT	.4 PT	.5 PT	.6 PT	.7 PT	.8 PT	.9 PT	RIGHT
7	50.	68.	46.	24.	3.	-19.	-41.	-63.	-85.	-107.	-129.
8	-77.	-45.	-15.	8.	35.	62.	89.	115.	142.	169.	196.
9	-6200.	-4910.	-3621.	-2331.	-1042.	248.	1538.	2627.	4117.	5406.	6696.
10	-6232.	-7020.	-4809.	-2598.	-386.	1825.	4036.	6248.	8459.	10670.	12882.
11	12192.	9441.	6691.	3940.	1189.	-1562.	-4313.	-7063.	-9814.	-12565.	-15316.

IDENT 14T 20 01			FRAME SYSTEM			MAY. 15, 1975			PAGE 86
TRIAL 1	FRAME 2	PATH 1							
TANGENTIAL SPAN	ROTATIONS LT. END	- RADIANS RT. END	- CLOCKWISE SPAN	POSITIVE LT. END	RT. END	SPAN	LT. END	RT. END	
1	-0.000069	0.000017	2	0.000017	-0.000194	3	-0.000194	0.001375	
4	0.001275	0.001002	5	0.001002	-0.002328	6	-0.002328	0.007394	
7	0.000039	0.000056	8	0.000032	-0.000162	9	-0.000162	-0.002641	
10	-0.002746	-0.001745	11	0.003921	0.001593				

HORIZONTAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END - DOWNWARD POSITIVE

MEMBER	E=	750.	C.C	0.0	-0.000	-0.001	-0.001	0.0
MEMBER 1	E=	750.	C.C	0.0	0.002	0.004	0.005	0.0
MEMBER 2	E=	750.	C.C	0.0	-0.010	-0.026	-0.045	0.0
LONG HINGE				LT C.C	1/4 -0.008	1/2 -0.020	3/4 -0.036	RT -0.053
MEMBER 4	E=	750.	C.C	0.0	-0.068	-0.151	-0.095	0.0
MEMBER 5	E=	750.	C.C	0.0	-0.170	-0.323	-0.154	0.0
MEMBER 6	E=	750.	C.C	0.0	-0.153	-0.282	-0.227	0.0

VERTICAL MEMBER DEFLECTIONS IN FEET AT 1/4 POINTS FROM LEFT END.

IDENT 14T 20 01			FRAME SYSTEM			MAY. 15, 1975			PAGE 87
TRIAL 1	FRAME 2	PATH 1							
MEMBER 7	E=	750.	C.C	0.000	-0.000	-0.000	0.0		
MEMBER 8	E=	750.	C.C	0.001	0.002	0.001	0.0		
MEMBER 9	E=	750.	C.C	-0.014	0.002	0.015	0.0		
MEMBER 10	E=	750.	C.C	-0.004	0.002	0.005	0.0		
MEMBER 11	E=	750.	C.C	0.007	0.001	-0.004	0.0		

***** BATCH TOTALS 103 FRAME UNITS 6 L.L. UNITS 0 PLOT UNITS 7 PRESTRESS UNITS COST= \$ 7.36

SYSTEM DOCUMENTATION

A complete package of system documentation may be obtained for the program Frame System by sending a request and a 9-track magnetic tape to:

California Department of Transportation
Division of Structures
Bridge Computer Services
Box 1499
Sacramento, California 95807